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In cooperation with the Pennsylvania Department of Conservation and Natural Resources

Pennsylvania Rural Development Council

Harrisburg, PA

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# **Standard Plans for Glulam Timber Pedestrian Bridges**

Patrick S. Powers, P.E. Perry D. Schram, P.E.



# Abstract

The development of standardized pedestrian timber bridge plans and specifications is a key element in improving design and construction practices. The bridge plans presented were developed as a cooperative effort between the USDA Forest Service, Wood In Transportation (WIT) program; The Pennsylvania Department of Conservation and Natural Resources (DCNR); the Pennsylvania Rural Development Council (PRDC); and Powers & Schram Inc., Consulting Engineers. This publication contains standardized designs and details for two timber bridge superstructure types, including longitudinal glued-laminated timber (glulam) stringer bridges with transverse timber decks, and longitudinal glulam panel bridges. The set of standards encompasses numerous span length and width combinations, design loads for an AASHTO H-10 vehicle, and pedestrian live loads.

Keywords: Timber, bridge, pedestrian, glulam, red maple, southern pine, Douglas-fir

Cover Photo: Jacobsburg Environmental Education Center Pedestrian Timber Bridge, Pennsylvania Department of Conservation aand Natural Resources, Belfast, Pennsylvania

These designs are intended for information purposes only and must be verified by a registered professional engineer.

February 2000

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### GENERAL INFORMATION

- 1. Use this series of standard drawings to provide a rapid means of producing design drawings for single span timber predestrian and blike/emergensy vehicle bridges in the 3.0 m to 18.0 m span range. By selecting the oppropriate standard format join sheets and inserting basic geometry and job specific information, the designer generates a complete set of contract drawings ready for construction.
- 2. All dimensions for this series are shown in millimeters unless otherwise noted.
- 3. The bridge types in this series utilize glulam timber components as basic elements of the superstructure. Standardized obutments are provided to assist the Engineer with the abutment design. With three types of superstructures and interchangeable obutments from which to choose, the designer should be oble to adopt the standards to fit most single span applications.
- 4. The lomination process utilized in glutom timber production enhances the structural efficiency of the timber bridge design. The process permits optimum use of higher grode lumber moteroid in the beam's highly stressed cross-sectional zones. Use of effective treatments maintains maximum service life or exposure durability by resisting and controling decay, insect utdack, and exposure of the process of the provides added treatments are considered to the provides added treatment on wet or rej deck surfaces.
- Use these glulam timber standards for pedestrian and bike/emergency vehicle stream crossings with the following general limitations.
- 1. Bridge curb to curb widths of 1220 mm, 1625 mm & 3600 mm.
- 2. Angle: of intersection (skew) not less than 45 degrees
- 3. Spans 3.0 m to 18.0 m.
- Select one of the two possible assembly types for the bridge superstructure: glulam beam with transverse glulam deck (102M), or glulam panel (103M),

Use the first bridge superstructure, gulum beam, for spons 3.0 m to 18.0 m. This superstructure composition consists of gulum timber beams and a transverse timber deck. The gulum beam system characteristically has a large depth—to—spon ratio due to the relative) low bending strength of wood compared to steel. In some cases, vertical clearance restrictions may rule out the use of this structure type because of the excessive superstructure depth. Where vertical clearance is a problem, consider the use of the gulum ponel superstructure.

For short spans of 3.0 m to 6.0 m, use the second type of bridge superstructure, a longitudinal hardwood glulam panel, to effectively reduce the depth of the timber superstructure. The longitudinal panel acts as a timber slob structure with a relatively shrillow profile.

- 7. Use the Bridge Rail Details which are shown on the drawings in series 104M.
- 8. The pile substructure details provided with these standard drawings assist in the design of safe, low cost bridge obtunnents in many cases. Unfortunetly, foundation conditions are not olways suitable for this obtunent type, therefore, consider on alternate substructure design. Be aware of required pile embedment length in selecting pile obtunent sites. Follower to attain the required pile embedment length due to bedrock or a very dense soil strotum close to the ground surface couses on unoccapitable lateral pile movement. To avoid such problems, verify the obtility to reach the minimum required embedment length as required by stream scour or soil conditions before selection a substructure type.
- 9. Consider the potential for pile damage during driving in determining suitability of timber pile abutters: Use timber pile sidely of sriction piles in oreas free of boulders or "ver such obstruct ans during driving. Employ timber piles with coultion where pile tips reach bedrock or a very dense stratum before ottoining the required friction embedment length. When such or contact occurs, driving resistance and the risk of pile damage increases ripidity. or minimize (MPOR) Do not drive beyond the MPOR.
- 10. Submit a completed set of drawings assembled from these standards to a registered professional engineer for review and approval to ensure adequate design, and perform a subsurface investigation prior to beginning the foundation design.

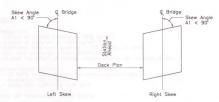
# INSTRUCTIONS FOR STANDARDS USE

Before using these standards, obtain basic survey, geometric data, and soils information for the proposed construction site. If the site is suitable for a timber bridge, choose one of the available timber superstructure types. If vertical clearance is a problem, use the longitudinal panel type, if feasible timber and the site of the site of

Design of substructure units is based on the material parameters and soil conditions shown on 100M, sheet 2. Compute sociur depth when substructure units are exposed to stream currents. Provide adequate embedment for substructure units to resist the effects of soour and frost.

Referring to the Index of Sheets (see this sheet), standards are separated into design sheets and construction sheets. In addition to informational and instructional material, the design sheets include data assembly sheets for the standardized types of substructures and superstructures. These sheets contain the basic data and the equations necessary to generate the information required for the fill—in type construction sheets. Select the appropriate data cossembly sheets and the appropriate construction sheets for the selected structure type.

Select the appropriate construction sheets for left, 90°, & right skewed structures. The skew angle for a left skewed structure is measured to the left of the bicycle path or wolkway centerline while a right skew angle is measured to the right of the centerline. See the following



After selecting the necessary data assembly and construction sheets, produce final contract drawings. Observe the following steps in the preparation process:

- A. Complete the data assembly sheets for the superstructure type selected.
- 1. Fill in the control stations and elevations table.
- Complete the control dimensions table. Reference supplemental tables. Work the table from tor to bottom.
- Choose a bridge rail type.
- 4. Complete the quantities table
- B. Complete the data assembly sheets for the substructure type selected.
- Enter the abutment number in the drawing title block (a separate data assembly sheet is required for each abutment).
- Complete the control dimensions table. Refer to geometric equations and supplemental tables and figures as required.
- 3. Complete the bar schedule table
- 4. Complete the substructure quantities table.
- C. Transfer the appropriate information from the data assembly sheets to the fill-in spaces on the standard construction sheets.
- Information from the superstructure data assembly sheet should be placed in the appropriate fill—in alots in the standard superstructure drawings 102M or 103M. Coded letters and numbers are provided to facilitate the correct placement of dimensions and other data.
- Information from the substructure and superstructure data assembly sheets must also be transferred to the standard substructure drawings, 105M, 106M, 107M, or 108M, through the use of codes provided.
- 3. If pile footings are required, the applicable driving method must be shown in the General Notes on the appropriate standard superstructure drawing. If pile load testing is required, pile load test "ato must be shown in a table near the General Notes. Estimated pile tip ..evations should be shown on core boring log plots when included as part of the design drawings.
- Completion of the appropriate stakeout & bridge rail details drawings (series 104M), is accomplished by reference to the substructure & superstructure data assembly sheets.
- D. Complete quantity estimates, add drawing titles and miscellaneous information.
  - Compute quantities for excavation, structure backfill, and other items not specifically provided for on the ~.to assembly sheets. Post all quantities in the approximate quantity table on the structure's quantities sheet.
- Customize the standard drawings by adding necessary location and route number information to the title block of each sheet. Number each sheet consecutively.
- 3. Add necessary information pertaining to utilities, hydraulic data, and alignments.
- 4. Add subsurface exploration information as required.

Include the completed data assembly sheets with the final set of contract plans produced from these standard drawings. The data assembly sheets follow the filled-in construction drawings and are numbered as part of the complete drawing set. Normally, no separate design calculations are required.

Determine and show the approximate location and type of the utility lines together with utility owner's names and address of all lines found within the construction area of the bridge. Show such lines on the structure General Plan sheet.

If the structure crosses a stream, the designer must obtain necessary permits from appropriate approval agencies. Show pertinent hydraulic data on the General Plan sheet.

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POWERS & SCHRAM INC.
CONSULTING ENGINEERS
STATE COLLEGE, PA

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GENERAL INFORMATION & INSTRUCTIONS

SHEET NO: SERIES TITLE: PEDESTRIAN GLULAN

1

ERIES NO:

100M

PEDESTRIAN GLULAM TIMBER BRIDGE DESIGN

## DESIGN CRITERIA

DESIGN SPECIFICATIONS - Design Division of 1994 AASHTO LRFD Bridge Design Specifications SUPERSTRUCTURE

- Io. Live Load (Typical Bike/Emergency Vehicle Bridge)
  - A. H Design Truck (Emergency Vehicle) load at strength 1 Load Combination (17.2kN front axle and 71.2kN rear axle spaced at 4.3m to 9.0m)
  - B. Pedestrian Load at Strength 1 Load Combination (4.1 x 10<sup>-3</sup> MPa)
- Ib. Live Load (Typical Pedestrian Bridge)
  - A. Pedestrian Load at Strength 1 Load Combination  $(4.1 \times 10^{-3} MPa)$
- IIo. Dead Loads (Typical Bike/Emergency Vehicle Bridge) —Bituminous surface of 90 kg/m²
  - -Future wearing surface 150 kg/m<sup>2</sup>
    -Timber bridge components 800 kg/m
- -Steel Bridge Components 7850 kg/m 3
- Ib. Dead Loads (Typical Pedestrian Bridge) -Optional select surface treatment (see note below) of 22.5 kg/m<sup>2</sup>
  -Future wearing surface 150 kg/m<sup>2</sup>
  -Timber bridge components 800 kg/m<sup>3</sup>
  - -Steel Bridge Components 7850 kg/m 3
  - Note: select surface treatment is Percol Elastic Cement (Microsurfacing) by E.J. Breneman, Inc. (610–678–9691) or an approved equal. 10 mm thick max.
- I Timber Design Criteria
  - A. Glulam Transverse Deck Design
  - 1. Design deck thickness in accordance with AASHTO 4.6.2.1
  - 2. Wet-Use Base Resistance & MOE (MPa)

	Douglas 3 Fir (DF)	Red 2 Maple (RM)	Southern Pine (SP)
Bending (Fby)	27.6	25.8	29.7
Shear (Fvy)	2.80	3.70	3.50
Modulus of Elasticity (Ey)	9650	8040	9650

- In-service moisture content > 16%
   Values generated from AIC's approved computer program
  "CI\_DesVal" \ Values reflect HB glulom combinations of No. 2 (N2) grade
  lumber for RM. (Reference: Pennsylvania D.O.T., BI\_G\_560M).
   Values from ASATIO Table 8.4.1.2.3—2 Value reflect 2 and 49
  Glulom Combinations for Douglos Fir and Southern Pine respectively.
- Nominal resistance and modulus of elasticity values obtained by adjusting wet-use base resistance values with applicable modification factors according to AASHTO 8.4.4.
- 4. Deflection less than or equal to span/425 and extreme relative deflection between adjacent deck panel edges less than or equal to 2.5 mm.
- B. Solid Sown Transverse Deck Design
- 1. Design deck thickness in accordance with AASHTO 4.6.2.1
- 2. Wet-Use Base Resistance & MOE (MPa) 1,2

	Douglas Fir (DF)	Red Maple (RM)	Southern Pine (SP)
Bending (Fby)	17	17	19
Shear (Fvy)	2.10	2.10	2.10
Modulus of Elasticity (Ey)	10000	9300	10000

- 1.) In-service moisture content > 16%
  2.) Values from AASHTO Table 8.4.1.2.3-2 Grade No. 2
- Nominal resistance and modulus of elasticity values obtained by adjusting wet—use base resistance values with applicable modification factors according to AASHTO 8.4.4.
- 4. Live load deflection less than or equal to span/425 and extreme relative deflection between adjacent deck panel edges less than or equal to 2.5 mm.
- - 1. Live load distribution for moment and shear in interior beams with wood decks. AASHTO table 4.6.2.2.2a-1
- 2. Live load distribution factor (deflection) = No. of lanes / No. of beams
- 3. Wet-Use Base Resistance & MOE (MPa)

	Douglas 3 Fir (DF)	Red 2 Maple (RM)	Southern 3 Pine (SP)
Bending (Fbx)	37	37	37
Shear (Fvx)	3.10	4.17	3.80
Comp. Perp. to the Grain (Fcp)	6.20	8.33	6.20
Modulus of Elasticity (Ex)	10300	10300	10300

- 1.) In-service moisture content > 16% Design values based on published AITC 119-96 stresses for 24F-1.8E glulam combinations
- Values from ASHTO Table 8.4.1.2.3-1. Values reflect 24F V4 and 24F V3 glulam combination layups for Dauglas Fir and Southern Pine, respectively,

- Nominal resistance and modulus of elasticity values obtained by adjusting wet-use base resistance values with applicable modification factors according to AASHTO 8.4.4.
- 5. Live load deflection less than or equal to span/425.
- D. Longitudinal Panel Design

-Live load distribution for moment = no. of loads / no. of equivalent strips, AASHTO 4.6.2.1.3

1. Wet-Use Base Resistance & MOE (MPa)

11	Douglas T Fir (DF)	Red <sup>2</sup> Maple (RM)	Southern Pine (SP)
Bending (Fby)	27.6	25.8	29.7
Shear (Fvy)	2.80	3.70	3.50
Shear (Combination lay-up) (Fvy) (3)	1.50	1.90	1.70
Comp. Perp. to the Grain (Fcp)	5.17	6.61	5.17
Modulus of Elasticity (Ey)	9650	8040	9650

- In-service moisture content > 16%
   Values generated from AITC's approved computer program "GLDesVal". Values reflect H6 glulam combinations of No. 2 (N2) grade lumber for RM.(Reference: Pennsylvania D.O.T., BLC-560M).
- Shear values are for combination lay-up glulam lumber.
   Values from AASHTO Table 8.4.1.2.3-2 Value reflect 2 and 49 Glulam Combinations for Douglas Fir and Southern Pine respectively.
- Nominal resistance and modulus of elasticity values obtained by adjusting wet-use base resistance values with applicable modification factors according to AASHTO 8.4.4.
- Deflection less than or equal to span/425 and extreme relative deflection between adjacent edges less than or equal to 2.5 mm.
- Net Dimensions of Southern Pine, Red Maple, & Douglas Fir Glued Laminated Timber

Nominal Dimension (mm)	Net Minimum Finished Dimension (mm)	Net Minimum Finished Dimension (mm)
100	79	-
150	130	-
200	175	-
250	100-	219
300	- 10	264
350	-	314
400	-	365
450	-	410

- 1.) Single member lay-up
- 2.) Combination lay-up



# COMBINATION LAY-UP

# SINGLE MEMBER LAY-UP

- Preservative Treatment
  - A. All sawn lumber shall be treated in accordance with the requirements of AWPA Standard C14 with one of the following preservatives:
    - Creosote conforming to AWPA Standard P1.
       Pentachlorophenal conforming to AWPA Standard P8 in hydrocarbon solvent, Type A, conforming to AWPA Standard P9.
  - B. Treated material shall be free of excess preservative on the wood surface. The treating process for these preservatives shall include an expansion bath, steaming and/or dripping to minimize bleeding.
  - C. Treated wood shall be inspected and certified in accordance with AWPA Standard M2.
- ▼ Elastomeric Bearing Pads
  - A Material
    - 1. Elastomer 50 durometer hardness on Share A scale

# SUBSTRUCTURE

- Design Data
  - -Density of backfill material = 1900\_kg/m<sup>3</sup> -Density of concrete = 2400 kg/m<sup>3</sup>
  - -Equivalent fluid earth pressure = 5.5 Pa/mm of depth -Live load surcharge = refer ASHTO 3.11
  - -Neglect the effect of passive pressure due to soil in front of wall.
- II Concrete Design Criteria
- 20.7MPa cement concrete (abutments below bridge seat, wingwalls,
  - cheekwalls, and footings). - Grade 400 reinforcing steel bars
- I Timber Sill Substructure Design Criteria
  - A. Bearing Sill
    - 1. Design timber bearing sill to act as a continuous beam over the timber pelies. The proposed method of timber pile placement is to provide a timber pile at each abutment/wingwall intersection and then place the neccessory number of interior piles at equal spaces (see pile design criteria).
  - 2. For solid sawn lumber use Wet-Use Base Resistance & MOE from AASHTO Table 8 4 1 1 4-1
  - 3. Glulam Wet-Use Base Resistance & MOE (MPa) 1

	Douglas Y Fir (DF)	Red * Maple (RM)	Southern Pine (SP)
Bending (Fbx)	30.3	18.2	32.1
Shear (Fvx)	3.1	3.4	3.8
Modulus of Elasticity (Ex)	9650	7500	9650

- In-service moisture content > 16%
   Design values based on published AITC 119-96 stresses for H6 glulam combinations
- 3.) Values from AASHTO Table 8.4.1.2.3-2 Value reflect 2 and 49
- Glulam Combinations for Douglas Fir and Southern Pine respectively.
- Obtain nominal resistance and modulus of elasticity values by adjusting wat-use base resistance values with applicable modification factors according to AASHTO 8.4.4.
- B. Timber Lagging
- 1. Use Wet-Use Base Resistance & MOE from AASHTO Table 8.4.1.1.4-1
- Obtain nominal resistance and modulus of elasticity values by adjusting wet-use base resistance values with applicable modification factors according to AASHTO 8.4.4.
- C. Timber piles
- 1. Provide piles in occordance with AASHTO M168
- 2. Use Wet-Use Gase Resistance & MOE from AASHTO Table 8.4.1.3-1
- 3. Obtain nominal resistance and modulus of elasticity values by adjusting wet-use base resistance values with applicable modification factors according to AASHTO 8.4.4.
- 4. All piles are 300 mm diameter timber (dia. measured 900 mm from butt.)
- 5. Obtain approval of pile driving criteria from Engineer prior to construction.
- 6. Provide applicable pile driving notes
- 1. Provide piles in accordance with AASHTO 10.7
- 2. All piles are HP 254x63
- 3. Obtain approval of pile driving criteria from Engineer prior to construction.
- 4. Provide applicable pile driving notes

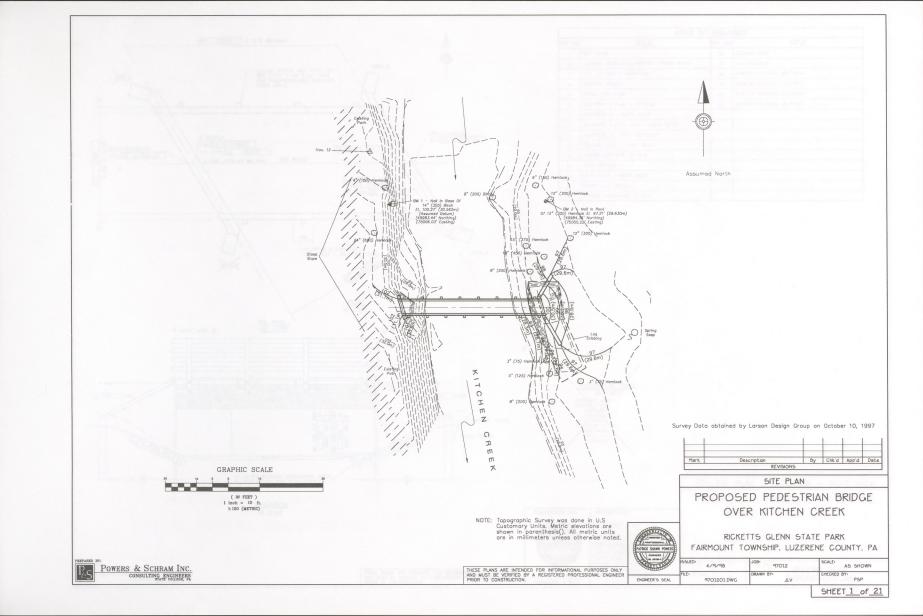
DESIGN CRITERIA RIES NO: SHEET NO PEDESTRIAN GLULAM 100M 2 TIMBER BRIDGE DESIGN

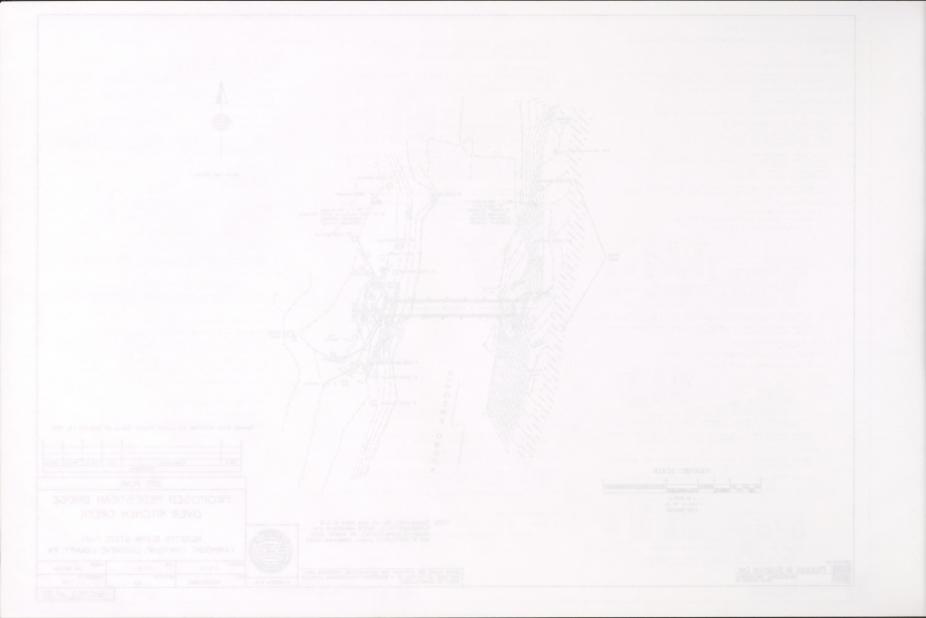
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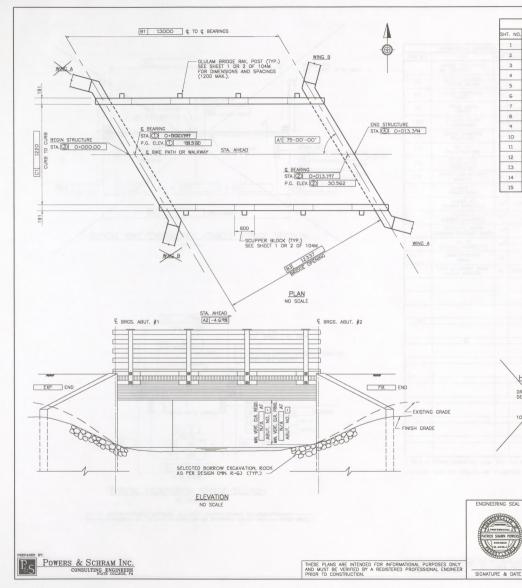
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13	DECK PLAN - RIGHT SKEW							
14	BRIDGE RAIL DETAILS							
15	TYPICAL HAPDWAPE DETAILS							

HYDRAULIC DATA
(DESIGNER)

DRAINAGE ARA DESIGN. FLOOD FROOD FRO

PREPARED BY:

POWERS + SCHRAM INC.

CONSULTING ENGINEERS

PHONE: (814) 238-1175

e-mail powers evicon.net

2545 N. ATHERTON STREET. SUITE 101 STATE COLLEGE. PA 16801 PHONE: (814) 238-1170 Mark Description By Child App'd Date REVISIONS

GENERAL PLAN & ELEVATION - RIGHT SKEW

PROPOSED PEDESTRIAN BRIDGE OVER KITCHEN CREEK

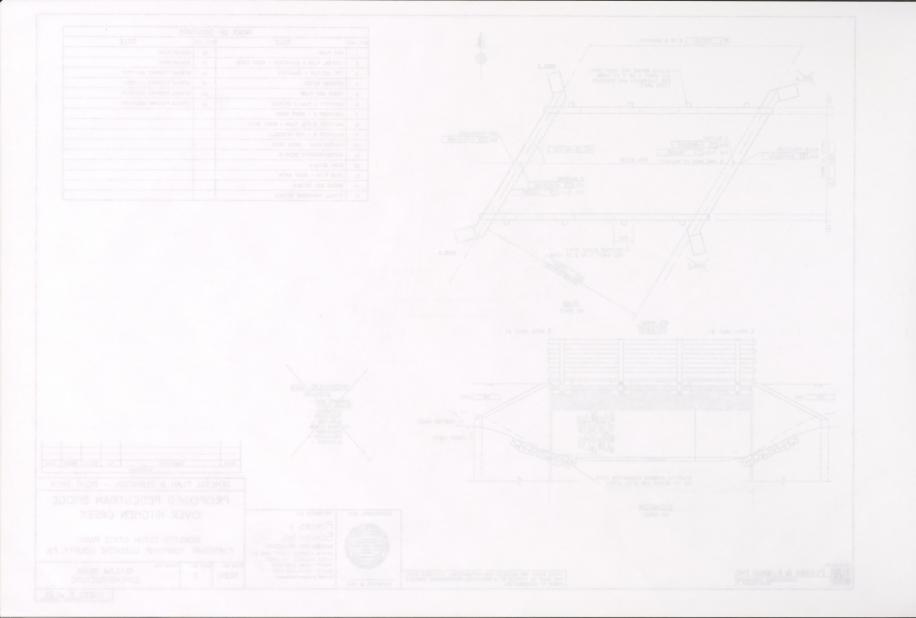
RICKETTS GLENN STATE PARK FAIRMOUNT TOWNSHIP, LUZERENE COUNTY, PA

SERIES NO: SHI

SHEET NO: SEI

GLULAM BEAM SUPERSTRUCTURE

SHEET 2 of 21





THESE PLANS ARE INTENDED FOR INFORMATIONAL PURPOSES ONLY AND MUST BE VERIFIED BY A REGISTERED PROFESSIONAL ENGINEER PRIOR TO CONSTRUCTION.

ENGINEER'S SEAL

FRIES NO-102M

Mark

GLULAM BEAM SUPERSTRUCTURE

SHEET 3 of 21

By Chk'd App'd Date

1220 CURB TO CURB BRIDGE RAIL SEE SHEET 1 OF 104M C WALKWAY OPTIONAL SELECT SURFACE TREATMENT (SEE NOTE BELOW) P.G. ELEVATION > \$ BEAM DATA SPECIES RED MAPLE 130 J2 2 630 DEPTH 305 H1 496 305 992 1602

CURB TO CURB

-GLULAM DECK

& BICYCLE PATH

DECK WIDTH

TYPICAL BIKE/EMERGENCY VEHICLE BRIDGE SECTION

NO SCALE

R.G. ELEVATION -BIT. WRG. SURFACE

HEAVY DUTY

WATERPROOF

MEMBRANE

TYPICAL PEDESTRIAN BRIDGE SECTION

NO SCALE -NOTE: SELECT SURFACE TREATMENT IS PERCOL ELASTIC CEMENT (MICROSURFACING)
-BY E.J. BRENEMAN, INC. (610-678-9691) OR AN APPROVED EQUAL: (10 mm THICK MAX.)

GLUE LAMINATED TIMBER (1) 0.20 0.20 SOLID SAWN TIMBER (1) 3.64 3.64 BEARING PLATE (1)(2) kg 63.45 63.45 SELECT SURFACE TREATMENT (1) N/A N/A 152 um POLYURETHANE 3.34 (1) 3.34 HEAVY DUTY WATERPROOF MEMBRANE (1) N/A N/A BITUMINOUS WEARING COURSE (1) N/A N/A kg CLASS 3 EXCAVATION 20 N/A 20 CLASS AA CEMENT CONCRETE m<sup>3</sup> 0.18 0.36 0.18 N/A CLASS A CEMENT CONCRETE 63.41 63.41 SELECT BORROW 15 N/A 16 XCAVATION, STRUCTURE, BACKFI NO. 57 COURSE AGGREGATE 1.6 1.6 REINFORCEMENT BARS 360661 N/A 360661 REINFORCEMENT BARS. kg 2700 937453 940153 AND

APPROXIMATE QUANTITIES - BRIDGE STRUCTURE, AS DESIGNED

UNIT ABUT. 1 ABUT. 2 SUPERSTRUCTURE

LS

3.25

ITEM NO.

(1)

SPECIES

WIDTH DEPTH

SEE SHEET 2 OF 104M

BEAM DATA

ITEM

BRIDGE STRUCTURE AS DESIGNED

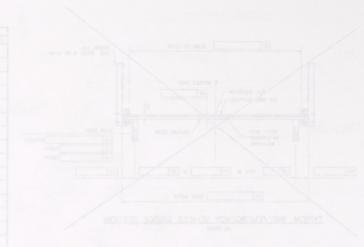
GLUE LAMINATED

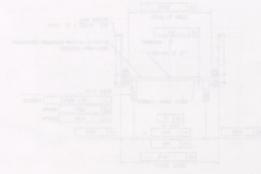
1. ITEMS IN BRIDGE STRUCTURE LUMP SUM ITEM GIVEN FOR INFORMATION ONLY. 2. QUANTITY DOES NOT INCLUDE ANY CONNECTION HARDWARE

# TYPICAL SECTION & QUANTIES

PROPOSED PEDESTRIAN BRIDGE OVER KITCHEN CREEK

RICKETTS GLENN STATE PARK FAIRMOUNT TOWNSHIP, LUZERENE COUNTY, PA SHEET NO:





TYPICAL PEDESTRIAN BRIDGE SECTION

I, ETHIS IN BRIDGE STRUCTURE COUP SUR ITEN ONER FOR INFORME & GENTLY DOES NOT MOULDE ANY CONFICENCY INFORMED

2207-AUO 4 LOWOSS HAIRNI

PROPOSED PEDESTRIAN BRIDGE

REMETTS GLENN STATE PARK EARHOUNT TOWNSHIP, LUZERZNE GOLUTY, PA

> GLULAM BEAM SUPERSTRUCTURE

JOS CHARLES

THE EXPLANATION OF MEMORY OF MEMORY PROPERTY TO SHAPE OF THE PROPERTY OF THE CONTRACT OF THE C

POWERS & SCHEAK INC.

IS to C Table

GENERAL NOTES:

DESIGN SPEMFICATIONS

AASHTO LRFD BRIDGE DESIGN SPECIFICATIONS (1994)

DESIGN IS IN ACCORDANCE WITH THE LOAD AND RESISTANCE FACTOR DESIGN METHOD.

DESIGN LIVE LOADS

TYPICAL DIVE /EMEDOCHOY VEHICLE DOIDOS

H DESIGN TRUCK (EMERGENCY VEHICLE) LOAD AT STRENGTH 1 LOAD COMBINATION (17.2KN FRONT AXLE AND 74.2KN REAR AXLE SPACED AT 4.3... TO 9.0...)

PEDESTRIAN LOAD AT STRENGTH 1 LOAD COMBINATION (4.1 x 10-3 MPu)

TYPICAL PEDESTRIAN BRIDGE

PEDESTRIAN LOAD AT STRENGTH 1 LOAD COMBINATION (4.1 x 10-3 MPa)

DEAD LOADS

TYPICAL BIKE/EMERGENCY VEHICLE BRIDGE

BITUMINOUS SURFACE OF 90 kg/m2

TIMBER BRIDGE COMPONENTS 800 kg/m3

STEEL BRIDGE COMPONENTS 7850 kg/m3

INCLUDES SURFACE AREA DENSITY OF 150 kg/m2 FOR FUTURE WEARING SURFACE ON THE DECK.

TYPICAL PEDESTRIAN BRIDGE

SELECT SURFACE TREATMENT OF 22.5 kg/m2

TIMBER BRIDGE COMPONENTS 800 kg/m3

STEEL BRIDGE COMPONENTS 7850 kg/m3

INCLUDES SURFACE AREA DENSITY OF 150 kg/m2 FOR FUTURE WEARING SURFACE ON THE DECK.

PROVIDE MATERIALS AND WORKMANSHIP IN ACCORDANCE WITH AASHTO/AWS/DI.5-88 BRIDGE WELDING CODE, AND CONTRACT SPECIAL PROVISIONS.

NOTIFY THE REGIONAL HEADQUARTERS OF THE FISH COMMISSION PRIOR TO CONSTRUCTION AND COOPERATE WITH FISH COMMISSION DURING CONSTRUCTION OF BRIDGES OVER FISHABLE STREAMS.

ALL DIMENSIONS SHOWN ARE HORIZONTAL AND IN MILLIMETERS UNLESS OTHERWISE NOTED.

SUPERSTRUCTURE DIMENSIONS SHOWN ARE FOR NORMAL TEMPERATURE OF 20° C.

SPREAD FOOTINGS MAY BE ORDERED BY THE ENGINEER TO BE AT ANY ELEVATION OR OF ANY DIMENSIONS NECESSARY TO PROVIDE A PROPER FOUNDATION.

THE SUPERSTRUCTURE MUST BE IN PLACE AND CONNECTED TO SUBSTRUCTURE BEFORE ABUTMENTS ARE

BACK FILL BOTH ABUTMENTS CONCURRENTLY. MAINTAIN SYMMETRICAL LOADING.

CONCRETE

PROVIDE 50 mm CONCRETE COVER ON REINFORCEMENT BARS, EXCEPT AS NOTED.

USE CLASS 20.7MPg CEMENT CONCRETE IN ABUTMENTS BELOW BRIDGE SEAT, WINGWALLS, AND FOOTINGS

USE CLASS 24.1MPg CEMENT CONCRETE IN CHEEKWALLS

A HIGHER CLASS CONCRETE MAY BE SUBSTITUTED FOR A LOWER CLASS CONCRETE AT NO ADDITIONAL COST TO THE OWNER.

PREPARE BEARING AREAS AS SPECIFIED IN CONTRACT DRAWINGS

SET ANCHOR BOLTS TO TEMPLATE OR IN PERFORMED HOLES. DO NOT DRILL UNLESS SPECIFICALLY INDICATED ON PLANS. FILL THE PERFORMED HOLES WITH NON-SHRINK GROUT. FILL THE CLEARANCE BETWEEN ANCHOR BOLTS AND HOLES IN MASONRY PLATES WITH APPROVED NONHARDENING CAULKING

FPOXY-COAT SUBSTRUCTURE REINFORCEMENT BARS AS INDICATED

RAKE-FINISH ALL HORIZONTAL CONSTRUCTION JOINTS, EXCEPT AS INDICATED.

REINFORCEMENT BAR SCHEDULE IS FOR INFORMATION ONLY. VERIFY IT PRIOR TO BIDDING AND FABRICATION.

PLACE CHEEKWALL CONCRETE AFTER BEAMS ARE SET IN POSITION.

CHAMFER EXPOSED CONCRETE EDGES 25 mm BY 25 mm EXCEPT AS NOTED

PROVIDE MINIMUM LAP AND EMBEDMENT LENGTH OF 30 DIAMETERS OR IN ACCORDANCE WITH ASSHTO SECTION A5.11 AND D5.11, WHICHEVER IS GREATER.

GENERAL NOTES CONTINUED

STEEL

HOT DIP GALVANIZE ALL TIMBER CONNECTION HARDWARE.

PROVIDE STRUCTURAL STEEL CONFORMING TO AASHTO M270, GRADE 250 (ASTM A709M, GRADE 250) DESIGNATION, EXCEPT WHEN NOTED OTHERWISE.

PROVIDE BOLTS AND LAG SCREWS CONFORMING TO ASTM A307 DESIGNATION, EXCEPT WHEN NOTED OTHERWISE.

PROVIDE BOLTS, NUTS, AND WASHERS IN ACCORDANCE WITH AASHTO LRFD BRIDGE DESIGN SPECIFICATION SECTION 6.4.3.

PROVIDE MALLEABLE IRON WASHER CONFORMING TO ASTM A47M, GRADE 24118.

PROVIDE LAG SCREWS CONFORMING TO ANSI 818.2.1 - 1981.

PROVIDE WOOD SCREWS IN ACCORDANCE WITH ANSI/ASME B18.6.1. WITH A MINIMUM THREADED PORTION OF TWO-THIRDS THE LENGTH OF THE SHAFT

MANUFACTURE SHEAR PLATE CONNECTORS FROM PRESSED STEEL MEETING SOCIETY OF AUTOMOTIVE ENGINEERS SPECIFICATION SAE-1010 OR AN APPROVED EGUAL.

COORDINATE THE REQUIREMENTS FOR PROTECTION AND/OR RELOCATION OF UTILITIES WITH THE UTILITY OWNER PRIOR TO STARTING WORK.

VERIFY AND LOCATE ALL EXISTING UTILITIES PRIOR TO STARTING WORK; CONDUCT OPERATIONS IN A MANNER WHICH ENSURES THAT THE UTILITIES WILL NOT BE DISTURBED OR ENDANGERED, AND ASSUME PULL RESPONSIBILITY FOR ANY DAMAGE TO UTILITIES DURING CONSTRUCTION. THE OPERATINENT ODES NOT ASSUME RESPONSIBILITY FOR REMINDIVESEMENT, PARTICIPATION IN DESIGN AND/OR REMISIONS, OR LUBRILITY FOR REMISIONS, OR LUBRILITY FOR REMISIONS, OR LUBRILITY FOR REMISIONS.

TIMBER

USE ONLY QUE LAMINATED TIMBER FARRICATED WITH EITHER SCUTHERN PINE, RED MAPLE OR 
DOUGLAS FIR LUMBER GRADED FOR NOTHEASTERN LUMBER MAUPLACTURER'S ASSOCIATION (RED MAPLE) 
WESTERN WOOD PRODUCTS ASSOCIATION (DOUGLAS FIR) OR SOUTHERN PINE INSPECTION BUREAU 
(SOUTHERN PINE) STANDARDS AND MANUFACTURED FOLLOWING ACTE 119, AITC 117 OR CURRENT SPECIFICATIONS.

PROVIDE MINIMUM WET-USE BASE RESISTANCES AND MOE VALUES IN ACCORDANCE WITH SHEET 2 OF 100M. USE GRADE NO. 2 OR BETTER FOR SOLID SAWN LUMBER.

ALL SAWN LUMBER SHALL BE TREATED IN ACCORDANCE WITH THE REQUIREMENTS OF AWPA STANDARD C14 WITH ONE OF THE FOLLOWING PRESERVATURES:

A. CREOSOTE CONFORMING TO AWPA STANDARD P1

CONFORMING TO AWPA STANDARD P1
PENTACHLOROPHENOL CONFORMING TO AWPA STANDARD P8 IN HYDROCARBON SOLVENT, TYPE A,
CONFORMING TO AWPA STANDARD P9 C. CCA CONFORMING TO AWPA STANDARD P5

GLULAM SHALL BE TREATED TO THE ABOVE REQUIREMENTS WITH CREOSOTE OR PENTACHLOROPHENOL

TREATED MATERIAL SHALL BE FREE OF EXCESS PRESERVATIVES ON THE WOODS SURFACE. THE TREATING PROCESS FOR THESE PRESERVATIVES SHALL INCLIDE AN EXPANSION BATH, STEAMING AND/OR DRIPPING TO ENSURE THAT THE PRESERVATIVE WILL NOT BLEED.

TREATED WOOD SHALL BE INSPECTED AND CERTIFIED IN ACCORDANCE WITH AWPA STANDARD M2.

TREAT ALL ABRASIONS AND CUTS MADE IN THE FIELD WITH THREE BRUSH COATS OF THE FIELD TREATMENT SOLUTION.

FIFED CUTTING IS NOT PERMITTED LINESS APPROVED BY THE ENGINEER

WHEN FIELD CUTTING. TREAT WITH BITUMINOUS ASPHALT BASED ROOF CEMENT, COPPER NAPHTHENATE PASTE, OR APPROVED PRESERVATIVE SYSTEM.

PROVIDE PILOT HOLES FOR LAG SCREWS IN RANGE OF (0.60)D TO (0.70)D

LEAD HOLES FOR LAG SCREWS WITH D< 12.7mm ARE D+ 0.8mm

LEAD HOLES FOR LAG SCREWS WITH D> 12.7mm ARE D+ 1.6mm

ALWAYS COAT LAG SCREW THREADS WITH BITUMINOUS ASPHALT BASED ROOF CEMENT, COPPER NAPHTHENATE PASTE, OR APPROVED PRESERVATIVE SYSTEM BEFORE INSTALLING LAG SCREW.

DO NOT DRIVE LAG SCREW WITH HAMMER. SCREW OR TORQUE LAG SCREWS.

PROVIDE SUFFICIENT LAG SCREW LENGTH SO LAG SCREW SHANK WILL PENETRATE RECEINING MEMBER.

SUBMIT SHOP DRAWINGS SHOWING DETAILS OF ALL GLULAM CONSTRUCTION FOR APPROVAL TO THE ENGINEER PRIOR TO FABRICATION OPERATIONS.

ALL TIMBER DIMENSIONS SHOWN ARE ACTUAL UNLESS OTHERWISE NOTED.

DO NOT PERMIT SPLICES IN PILES.

PROVIDE PILES IN ACCORDANCE WITH SHEET 2 OF 100M

Mark Chk'd App'd Date

GENERAL NOTES

PROPOSED PEDESTRIAN BRIDGE OVER KITCHEN CREEK

RICKETTS GLENN STATE PARK FAIRMOUNT TOWNSHIP, LUZERENE COUNTY, PA

102M

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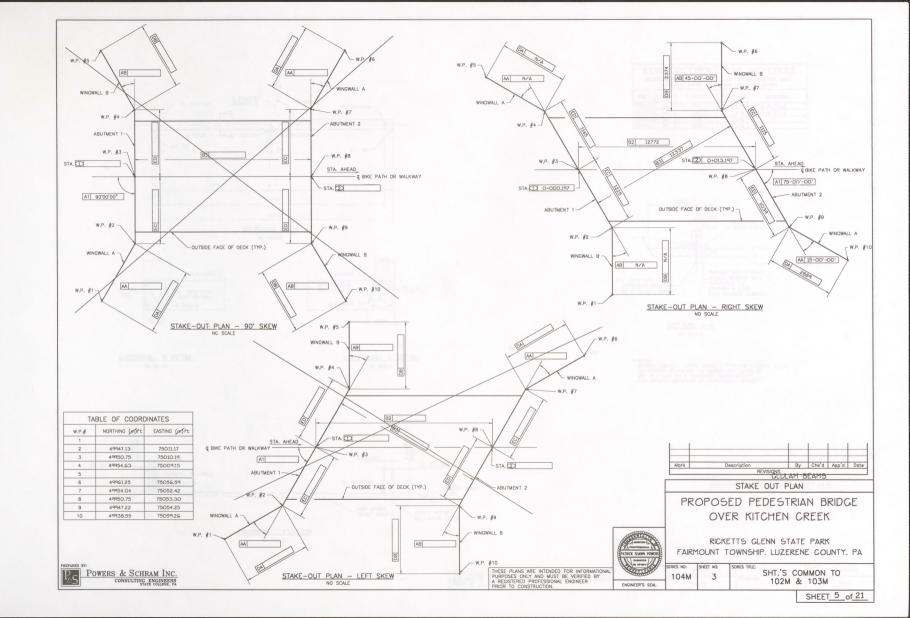
ENGINEER'S SEAL

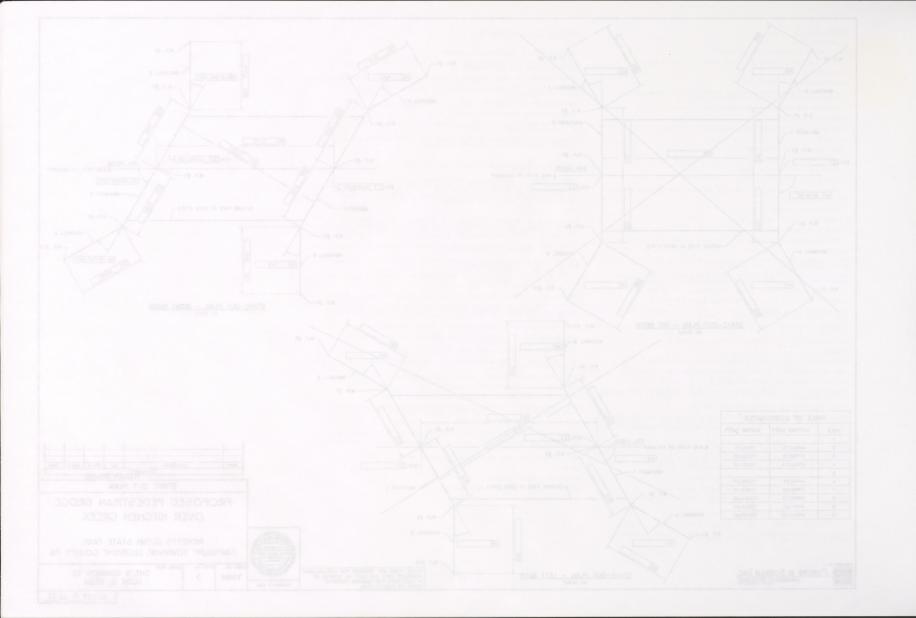
GLULAM BEAM SUPERSTRUCTURE

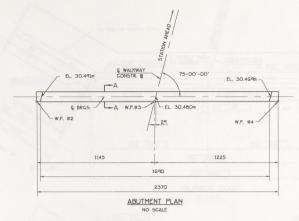


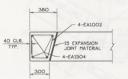
THESE PLANS ARE INTENDED FOR INFORMATIONAL PURPOSES ONLY AND MUST BE VERIFIED BY A REGISTERED PROFESSIONAL ENGINEER PRIOR TO CONSTRUCTION,

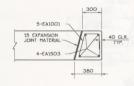






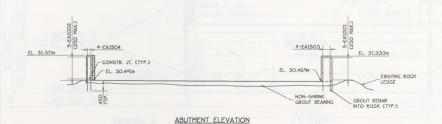






CHEEKWALL B DETAIL
NO SCALE

CHEEKWALL A DETAIL
NO SCALE



NO SCALE

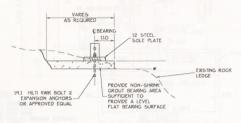


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REINFORCEMENT BAR SCHEDULE

(REINFORCEMENT BAR SCHEDULE IS FOR INFORMATION ONLY.

Telai I II I I I I I I I I I I I I I I I I												
MARK	SIZE	LENGTH	NO.	TYPE	REMARKS							
EA1001	10	981	5	STR.	BEND IN FIELD							
EA1002	10	1131	4	STR.	BEND IN FIELD							
EA1503	15	1314	5	STR.								
FA1504	15	1270	4	STR								



SECTION A-A

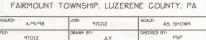
P NOTE: REPORT EXISTING DEBRIS, ROCK AND OTHER MATERIAL DOWN TO BEARNG ELEVATION OR LOWER AND CLEAN OR DRY SURFACE TO A COMBTION SATISFACTORY FOR PROFTER ADDIESTOR OF NON-SHRINK GROUT.



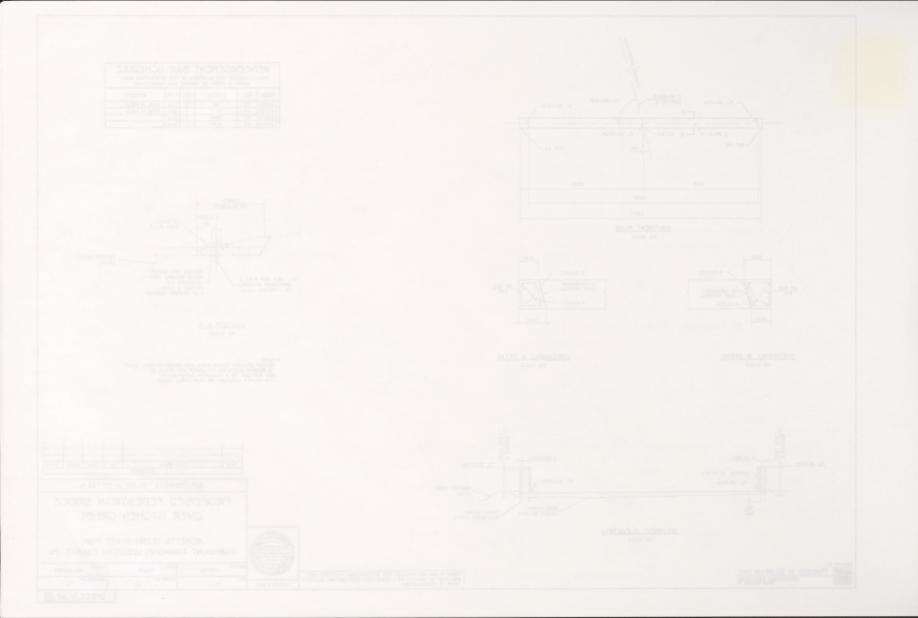
ABUTMENT 1 PLAN + DETAILS

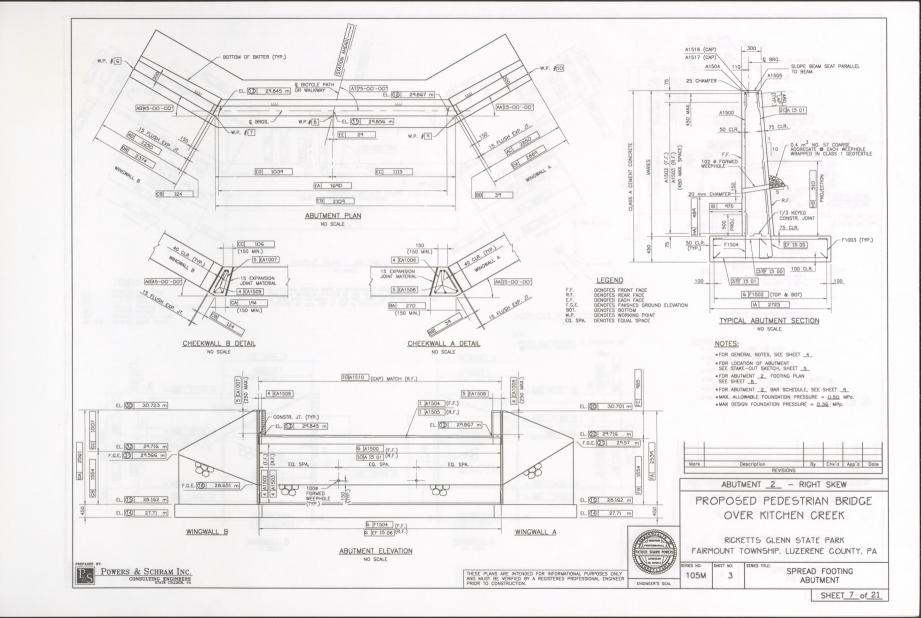
PROPOSED PEDESTRIAN BRIDGE OVER KITCHEN CREEK

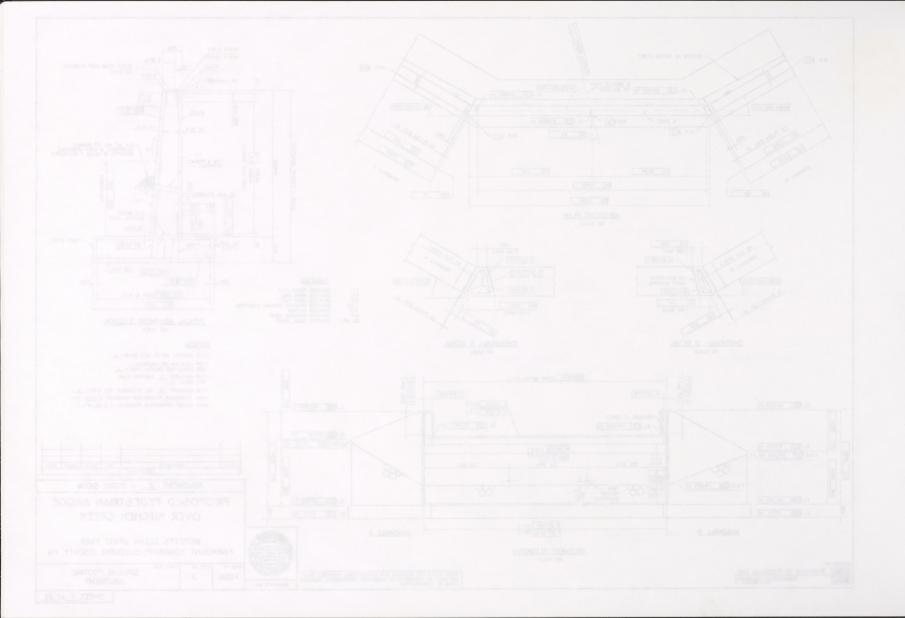
RICKETTS GLENN STATE PARK

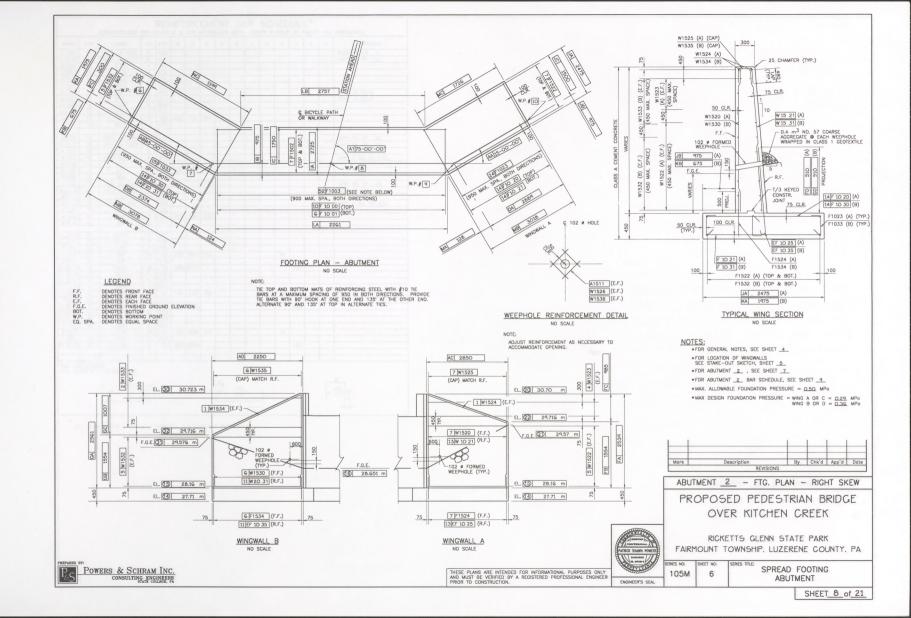


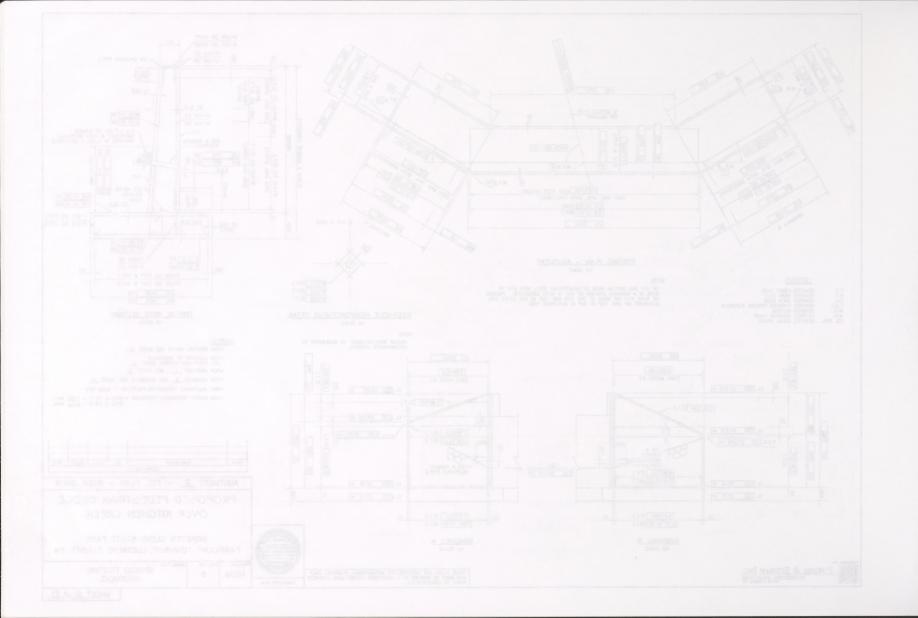
SHEET 6 of 21











MARK	SIZE	LENGTH	NO.	TYPE	A	В	С	D	Е	F	G	н	J	к	R	REMARKS
A1500	15	1655 to 1633	6	STR.								_			_	VARY EA. BY _4_
15 01	15	1655 to 1633	6	STR.												VARY EA. BY _4_
A1502	15	2153	4	STR.												
A1503	15	1963	4	STR.												
A1504	15	2153	1	STR.												
A1505	15	1963	1	STR.												
EA1006	10	950	4	STR.											_	BEND IN FIELD
EA1007	10	875	5	STR.				-							_	BEND IN FIELD
EA1508	15	1584	5	STR.										_		OCINO IN FICCO
EA1509	15	1328	4	STR.												
A1510	15	950	3	(3)	400	175	400							40		
A1511	15	300	16	STR.	100	170	100							-10	_	
AIJII	13	300	10	JIII.												
W1520	15	1504 to 2489	7	STR.						-						VARY EA. BY 141
W 15 21	15	1504 to 2489	7	STR.						-	-			95		VARY EA. BY 141
W_15_21	15	2750	5	STR.	_											45/11 CA. D1 141
W1522	15	1703 to 838	4	STR.						-						VARY 2 EA, BY 433
W1523	15	2915		STR.						-				3 3 7		17/11 2 LA. DI 433
W1524	15	975	4	3	400	175	400			-				40	100	
W1525	15	300	8	STR.	400	1/5	400					-		40		
W1530	15	1504 to 2511	23	STR.	_		10000			1					_	VARY EA. BY 168
W 20 31	20	1504 to 2511														VARY EA. BY 168
W1532	15		6	STR.	_	_	_	_	-		-				_	VART EA. BT 160
	15	2150 1349 to 641	10	STR.	_		_	_	-	-		-		_	_	144 DV 0 F4 DV 0 F4
W1533	15	2365	2	STR.	-			-	_			-			_	VARY 2 EA. BY 354
W1534				STR.	100	705	400							40		
W1535 W1536	15	975 300	3	(3)	400	325	400	_		-	-			40	_	
MIDDE	15	300	8	STR.	-		_		-	-				_	-	
F_15_00	15	2525	6	STR.	-		_		-	-				_	-	
F_15_01	15	2525	6	STR.			_		_					_	_	
F1502	15	2061	7	STR.						-					_	
F1003	10	550	16		125	450	125				_	75			_	
F1504	15	900	6	STR.	120	100	120				_	10			_	
F 15 06		1040	6	1	280	1100	-	-		-	-		200	_	_	
F_15_20	15	2275	8	STR.	200	1100	_			_	_	_	200		_	
F 15 21	15	2275	8	STR.						_	_	_			_	
F1522	15	2818	7	STR.							-					
F1023	10	700	20	(2)	125	450	125					75				
F1524	15	900	7	STR.	1.25							1				
F 15 25		1040	13	1	280	1020			-				200			
F_2030	20	1775	8	STR.	100	-020		7					100			
F 15 31	15	1775	8	STR.												
F1532	15	2878	5	STR.							100					
F1033	10	700	15	2	125	450	125	W				75				10 0000 00
F1534	15	900	6	STR.												
F 15 35		1040	6	1	180	1780							130			
				-		-							1			
BAR TYP		ND A STRAIGHT BAR		19	y	11	17									

<sup>\*</sup> USE 101M SHEETS 7 AND 8 TO COMPLETE BAR SCHEDULE INFORMATION.



ABUTMENT 2 BAR SCHEDULE

PROPOSED PEDESTRIAN BRIDGE OVER KITCHEN CREEK

RICKETTS GLENN STATE PARK
FAIRMOUNT TOWNSHIP, LUZERENE COUNTY, PA

PATRICK SHAWN POWERS

IN NOTING

ENGINEER'S SEAL.

105M

7 SERIES TITL

SPREAD FOOTING ABUTMENT

PREPARED BY:

POWERS & SCHRAM INC.

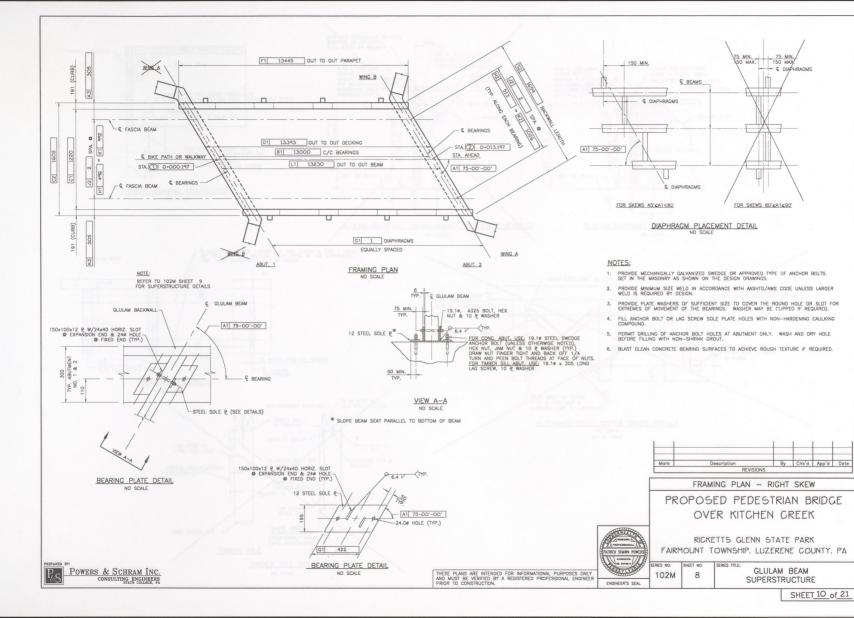
CONSULTING ENGINEERS

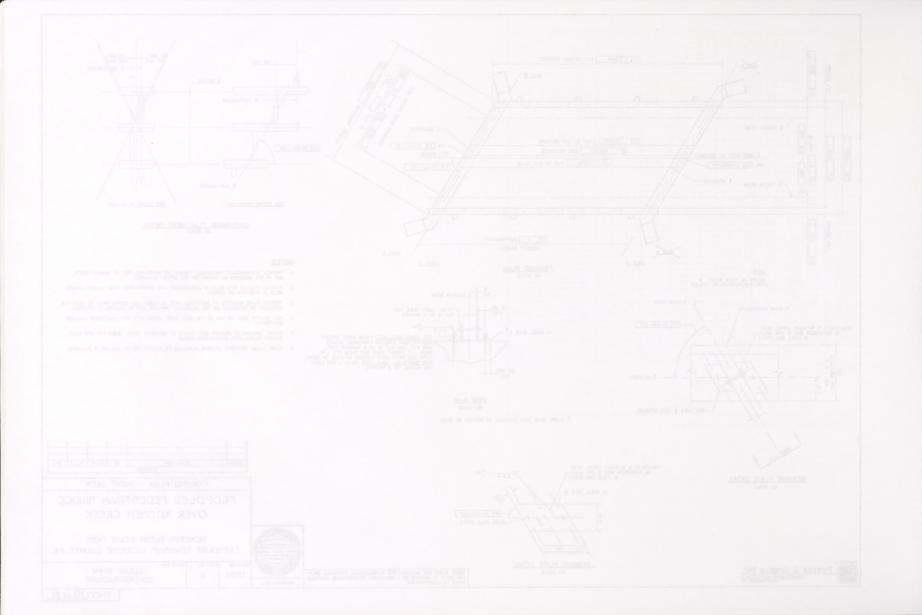
TATE COLLEGE, PA

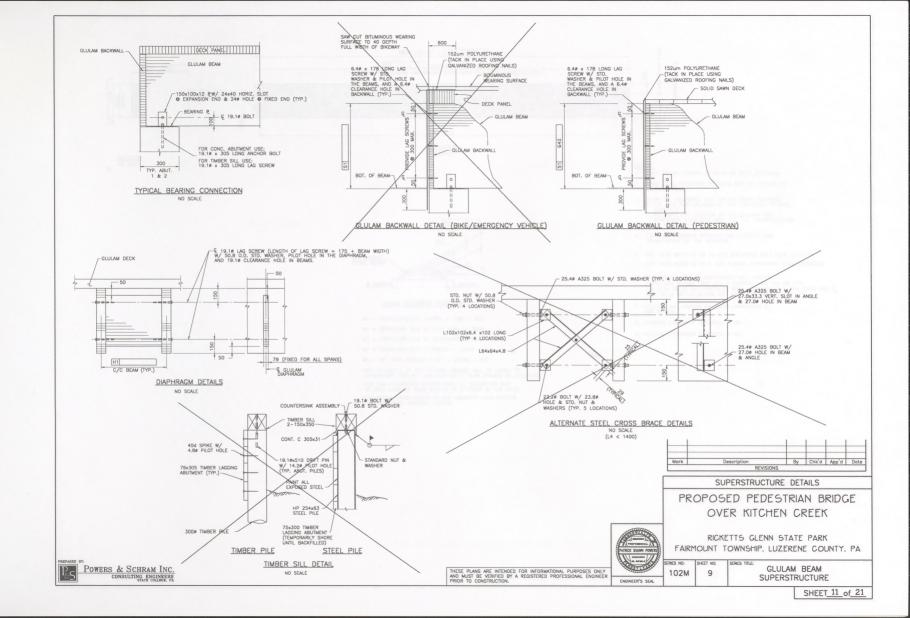
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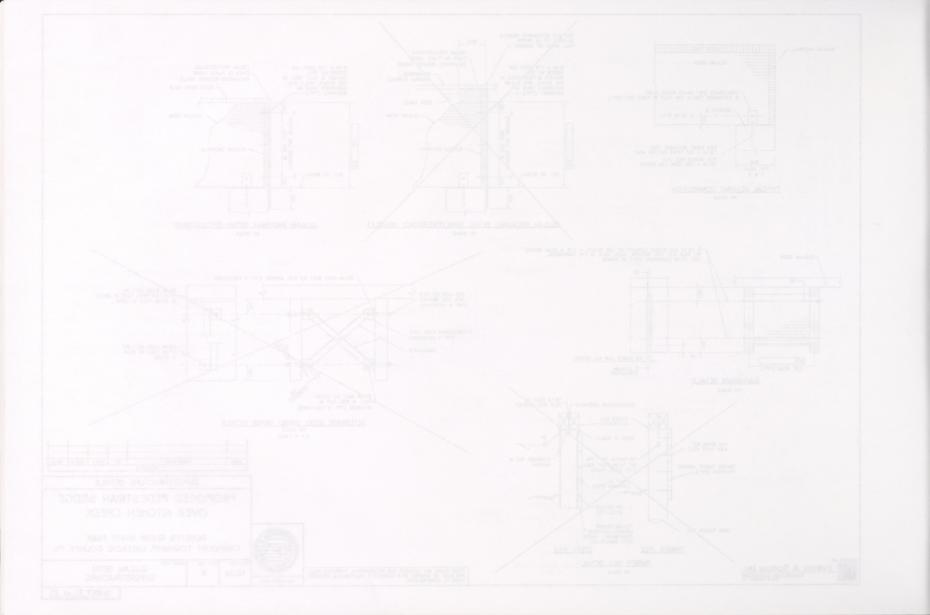
SHEET 9 of 21

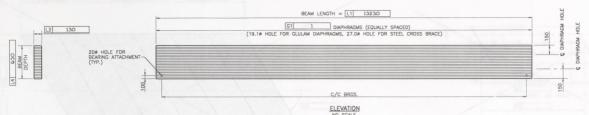




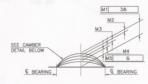








NO SCALE



# BEAM CAMBER DIAGRAM

- M1 = PRE-FABRICATED CAMBER = 3(M2 + M3)
- M2 = DEFLECTION DUE TO DEAD LOAD OF BEAM
- M3 = DEFLECTION DUE TO SUPERIMPOSED DEAD LOAD
- M4 = DEFLECTION DUE TO CREEP = 1.5(M2 + M3)
- M5 = NET FINAL CAMBER = M1 2.5(M2 + M3)
- THE THICKNESS OF THE WEARING COURSE WILL BE VARIED TO COMPENSATE FOR ANY INACCURACIES IN BEAM CAMBER AS APPLICABLE.
- \*THE PRE-FABRICATED CAMBER LESS THE DEFLECTION DUE TO DEAD LOAD OF BEAM SHOULD BE CHECKED IN THE FIELD.
- \*DEFLECTION CALCULATIONS DO NOT CONSIDER LOAD EFFECTS DUE TO FUTURE WEARING SURFACE.

- 1. SHOW DESIGN LENGTH OF BEAM ON SHOP DRAWINGS.
- 2. SHOW PLAN, ELEVATION, SECTIONS AND ALL DETAILS ON SHOP DRAWINGS.
- SHOW THE FOLLOWING DATA ON THE SHOP DRAWINGS:
   THE SIZE AND LOCATION OF THE TEMPORARY STORAGE
   THE TYPE AND LOCATION OF THE BRACING AND TEMPORARY SUPPORTS USED FOR THE TRANSPORTATION OF THE BEAMS.
- FABRICATOR CHECKS STABILITY FOR HANDLING AND TRANSPORTING OF THE MEMBERS.
- 5. SEE 102M SHEET 9 OR 10 FOR DIAPHRAGM BOLT HOLE LOCATIONS. SEE 102M SHEET 8 OR 9 FOR BEARING ATTACHMENT HOLE LOCATIONS.
- 6. CONSTRUCT BEAMS IN ACCORDANCE WITH CURRENT INSPECTION MANUAL, ATC 200 & CURRENT ATC 119 OR 117.

  ALL BEAM TO BE MANUFACTURED WITH A MINIMUM 16.5 MPg (2400 PSI) F AND 12410 MPa (1.8x10E6 PSI) MOE (DRY-USE VALUES).
- SPLICE JOINT LOCATION ON OUTER LAMINATIONS IS NOT CRITICAL.
- 8. MAXIMUM LAMINATION THICKNESS IS 50.
- 9. MINIMUM LAMINATION THICKNESS IS 20.

# BEAM DETAILS

# PROPOSED PEDESTRIAN BRIDGE OVER KITCHEN CREEK

RICKETTS GLENN STATE PARK FAIRMOUNT TOWNSHIP, LUZERENE COUNTY, PA

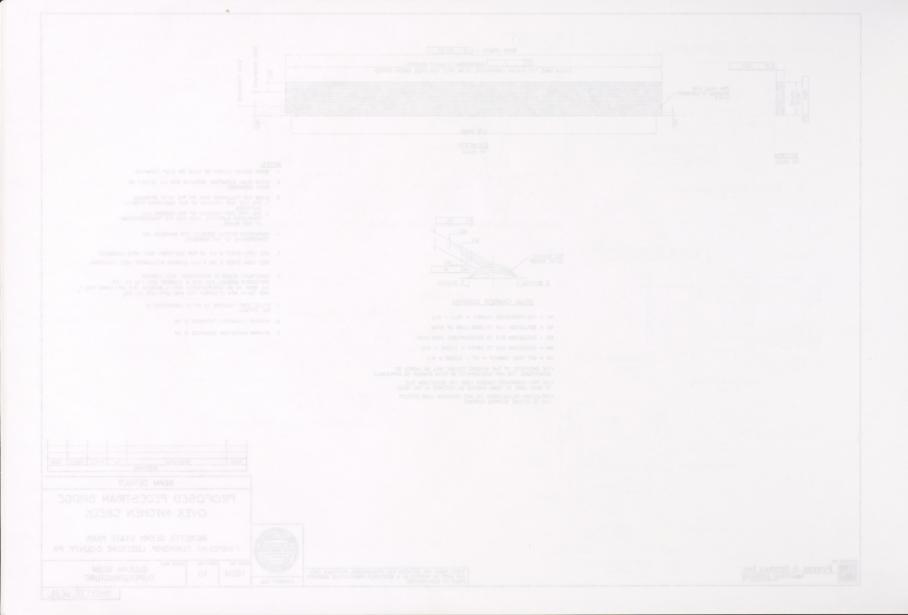
102M

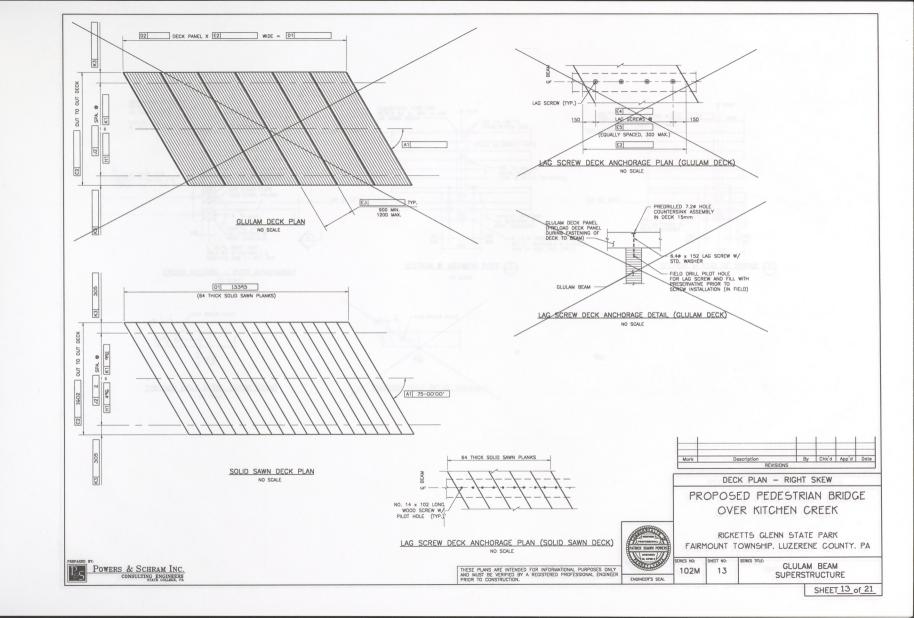
10

GLULAM BEAM SUPERSTRUCTURE

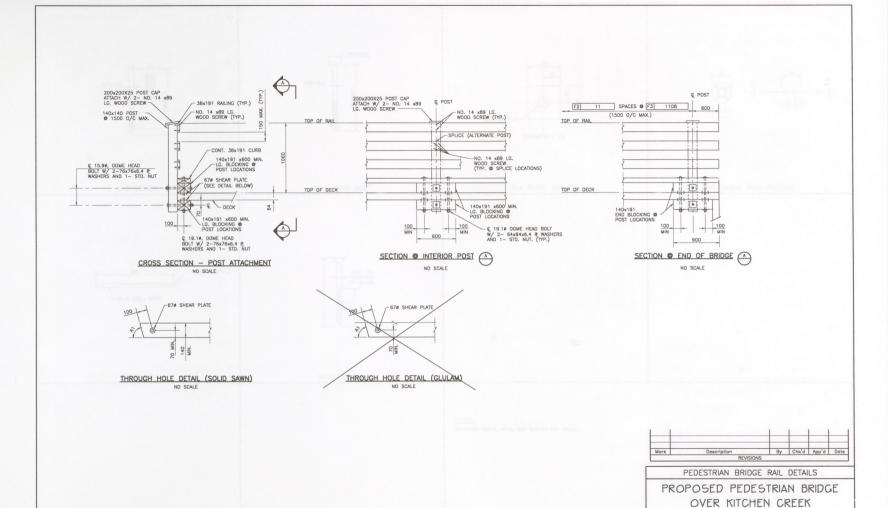
THESE PLANS ARE INTENDED FOR INFORMATIONAL PURPOSES ONLY AND MUST BE VERIFIED BY A REGISTERED PROFESSIONAL ENGINEER PRIOR TO CONSTRUCTION.

SECTION NO SCALE





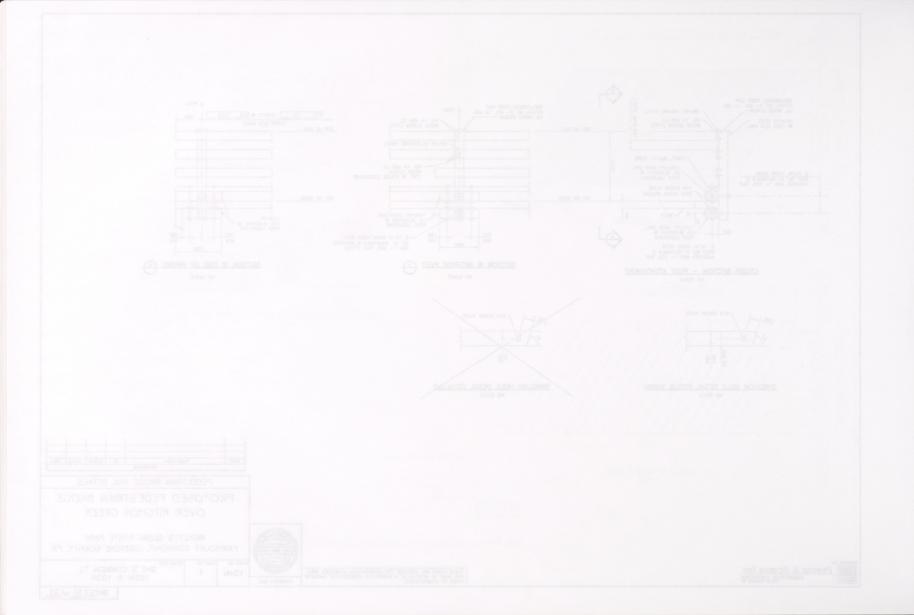


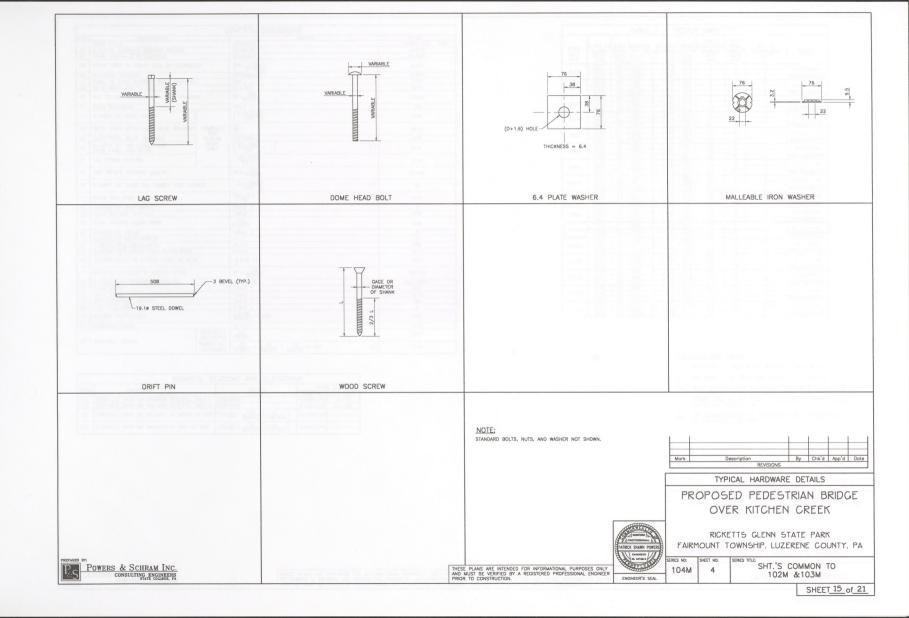


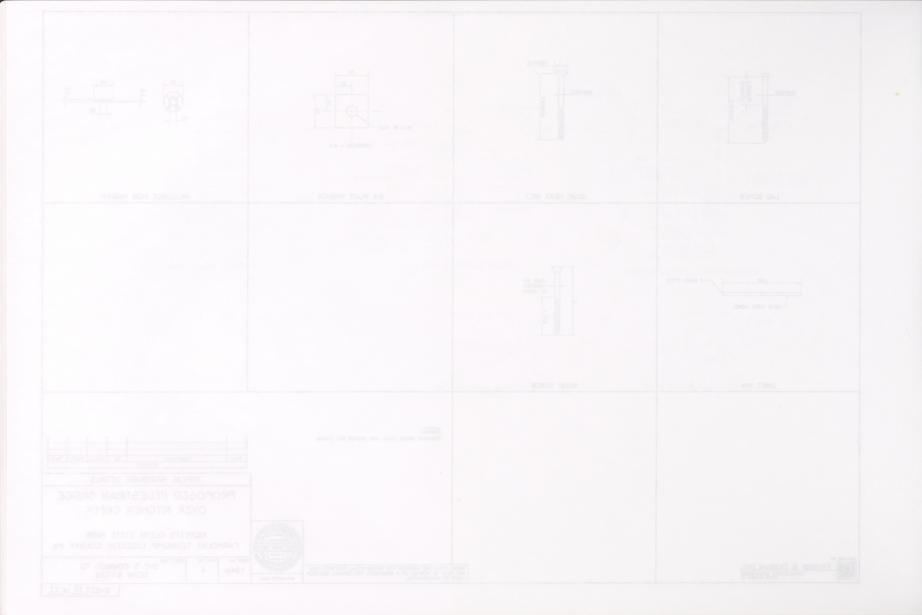


RICKETTS GLENN STATE PARK FAIRMOUNT TOWNSHIP, LUZERENE COUNTY, PA

THES NO: SHEET NO: SERIES TITLE: SHT.'S COMMON TO 102M & 103M







ODE	DESCRIPTION		ONTROL DIMENSIONS SOURCE	VALUE		
A1	DESCRIPTION SKEW ANGLE		DESIGNER	75-00'-00' DE		
A2			DESIGNER	-4.69Z		
B1	% GRADE (LOOKING STATIONS AHEAD)		DESIGNER	13000		
BI	SPAN LENGTH- € TO € BEARING					
B2	FRONT FACE TO FRONT FACE OF ABUTMEN	TS	$\left(81 - \frac{220}{SIN(A1)}\right)$	12772		
83	WATERWAY OPENING		(B2)SIN(A1)	12337		
C1	CURB TO CURB ROADWAY WIDTH (NORMAL)		TABLE 1	1220		
C2	DECK WIDTH OUT TO OUT		C1+382	1602		
D1	OUT TO OUT DECKING ALONG & OF ROADWA	AY	B1+380 SIN(A1)	13393		
D2	DECK THICKNESS		TABLE 1	64		
E1	NUMBER OF DECK PANELS	$\left\{\frac{D1*SIN(A1)}{1200}\right\}$ (1)				
E2	DECK PANEL WIDTH ALONG & OF ROADWAY	COMPLETE	D1 E1	N/A		
E3	DECK PANEL WIDTH (NORMAL)	FOR	E2*SIN(A1)	N/A		
	NUMBER OF LAG SCREWS PER	DECK	( 50 700 )			
E4	DECK PANEL PER BEAM	ONLY	( 300 )	) N/A		
E5	LAG SCREW SPACING		E2-300 E4-1	N/A		
F1	OUT TO OUT PARAPET LENGTH		D1+ 191 TAN(A1)	13445		
F2	NUMBER OF GUIDE RAIL TIMBER POST SPA	ACES	$\left\{\frac{D1-1200}{1200}\right\}$	) 11		
F3	GUIDE RAIL POST SPACING		D1-1200 F2	1108		
G1	NUMBER OF DIAPHRAGMS		TABLE 1	1		
H1	BEAM SPACING (NORMAL)		TABLE 1	496		
Н2	BEAM SPACING ALONG SKEW		H1 SIN(A1)	513		
J1	NUMBER OF BEAMS		TABLE 1	3		
12	NUMBER OF BEAM SPACES		J1-1	2		
K1	© FASCIA TO © FASCIA BEAM		H1*J2	992		
ζ2	€ FASCIA TO € FASCIA BEAM ALONG SKEW		H2*J2	1027		
(3	© FASCIA BEAM TO OUTSIDE FACE OF DECI	<	1/2 (C2-K1)	305		
L1	BEAM LENGTH (OUT TO OUT OF BEAM)		B1+ 222 Sin(A1)	13230		
2	GLULAM BEAM SPECIES COMBINATION		DESIGNER (S	) RED MAPLE		
1.3	BEAM WIDTH		TABLE 1	130		
L4	BEAM DEPTH		TABLE 1	630		
M1	PRE-FABRICATED CAMBER		TABLE 1	38		
45	NET FINAL CAMBER	7790	TABLE 1	6		
Q1	BEARING PLATE WIDTH		L3+36 SIN(A1) + 250	422		
S1	BACKWALL DEPTH		L4+12	642		
	P (1988)	CONCRETE	C2 SIN(AT)	1659		
S2	BACKWALL LENGTH	TIMBER SILL ABUTMENTS	$\frac{C2}{SIN(A1)} + \frac{76}{SIN(AA)} + \frac{76}{SIN(AB)} + 200$ (3)	) N/A		

	CONTROL ST	TATIONS AND ELEVATION	NS	
CODE	LOCATION	SOURCE	VALU	E (m)
CODE	LOCATION	SOURCE	STATION	P.G. ELEV.
Φ	& BICYCLE PATH OR WALKWAY AT & BRG. ABUT.1	DESIGNER	0+000.197	31.172
0	EBICYCLE PATH OR WALKWAY AT EBRG. ABUT.2	DESIGNER	0.+013.197	30.562
9	& BICYCLE PATH OR WALKWAY AT BEGIN OF STR.	$STA \bigcirc -\frac{190}{SIN(A1)} \left(\frac{m}{1*10^3 mm}\right)$	0+000.00	100
<b>(4)</b>	& BICYCLE PATH OR WALKWAY AT END OF STR.	STA 2 + 190 (m) (1*103 mm)	0+013.394	

			IAB	LE I	- 0	ESIG	N DATA (3	,,,,,		
SPAN (B1) mm	CURB TO CURB (C1)	DECK THICK. (E1)	BEAM SPA. (H1)	NO. OF BEAMS (J1)	BEAM WIDTH (L3)	BEAM DEPTH (L4)	PRE- FABRICATED CAMBER (M1)	NET FINAL CAMBER (M5) mm	NO. OF DIAPHRAGMS (G1)	BRIDGE TYPE
	1220	64	496	3	79	175	3	1	Ö	
3000	1625	64	698	3	79	210	3	0	0	PEDESTRIAN
0000	3600	79	1020	4	79	315	4	1	0	BIKE/EMERGENC
	1220	64	496	3	79	245	5	1	0	PEDESTRIAN
4000	1625	64	698	3	79	280	4	1	0	
	3600	79	1020	4	79	385	8	1	0	BIKE/EMERGENC
	1220	64	496	3	79	280	8	1	1	PEDESTRIAN
5000	1625	64	698	3	79	315	7	1	1	
	3600	79	1020	4	79	455 350	12	2	1	BIKE/EMERGENC
6000	1220 1625	64 64	496 698	3	79	385	9	1	1	PEDESTRIAN
6000	3600	79	1020	4	79	455	20	3	1	BIKE/EMERGENC
	1220	64	496	3	79	385	1.3	2	1	
7000	1625	64	698	3	79	455	11	2	1	PEDESTRIAN
	3600	79	1020	4	79	560	25	4	1	BIKE/EMERGENC
	1220	64	496	3	79	455	15	2	1	PEDESTRIAN
8000	1625	64	698	3	79	490	15	3	1	
	3600	79	1020	4	79	595	36	6	1	BIKE/EMERGENC
	1220	64	496	3	79	525	17	3	1	PEDESTRIAN
9000	1625	64	698	3	79	560	17	3	2	
	3600	79	1020	3	79 79	665 560	22	4	1	BIKE/EMERGENC
10000	1220 1625	64	496 698	3	79	630	19	3	2	PEDESTRIAN
10000	3600	79	1020	4	79	735	47	8	2	BIKE/EMERGENC
	1220	64	496	- 3	79	630	24	4	2	
11000	1625	64	698	3	130	595	26	4	1	PEDESTRIAN
	3600	79	1020	4	130	630	70	12	1	BIKE/EMERGENC
	1220	64	49€	3	130	560	36	6	1	PEDESTRIAN
12000	1625	64	698	3	130	630	32	5	1	
	3600	79	1020	4	130	770	74	12	1	BIKE/EMERGENC
13000 1	1220	64	496	3	130	630	38	6	1	PEDESTRIAN
13000	3600	79	1020	4	130	735	90	15	1	BIKE/EMERGENC
	1220	64	496	3	130	665	46	8	1	
14000	1625	64	698	3	130	735	41	7	1	PEDESTRIAN
	3600	79	1020	4	130	805	94	16	1	BIKE/EMERGENC
	1220	64	496	3	130	700	53	9	1	DEDEGERATION
15000	1625	64	698	3	130	805	44	7	1	PEDESTRIAN
	3600	79	1020	4	130	875	98	16	111	BIKE/EMERGENO
	1220	64	496	3	130	770	56	9	1	PEDESTRIAN
16000	1625	64	698	3	130	910	51 114	8 19	2	
	3600	79	1020	3	130	805	64	19	2	BIKE/EMERGENO
17000	1220	64	496 698	3	130	910	54	9	2 2	PEDESTRIAN
17000	3600	79	1020	4	130	980	119	20	2	BIKE/EMERGENO
	1220	64	496	-3	130	840	73	12	2	
18000	1625	64	698	3	130	945	62	10	2	PEDESTRIAN
	3600	79	1020	4	130	1050	124	21	2	BIKE/EMERGENO

- (1) ROUND TO THE NEXT WHOLE NUMBER ONLY WITHIN { }
- (2) SEE SHEET 11 OF 101M FOR VARIABLES "AA" AND "AB"
- (3) BEAMS DESIGNED WITH APPROPRIATE WET USE & SIZE FACTOR.
- (4) DESIGN TABLE DO NOT ACCOUNT FOR VERTICAL OR HORIZONTAL CURVES ON BRIDGE DECK.
- (5) USE EITHER DOUGLAS FIR, RED MAPLE, OR SOUTHERN PINE AS PER SHEET 2 OF 100M.

			-		
Mark	Description	By	Chk'd	App'd	Date
	REVISIO	INS			

#### GLULAM BEAM

# PROPOSED PEDESTRIAN BRIDGE OVER KITCHEN CREEK

RICKETTS GLENN STATE PARK FAIRMOUNT TOWNSHIP, LUZERENE COUNTY, PA



DATA ASSEMBLY SHEETS

ENGINEER'S SEAL



#### PROFESSION PROFESSION

- ) | Kerria York Madella Stoke Took air of deuter (7)
- (8) SEE SHEET IT OF TOTAL FOR WISHESSES (NA. 198, 198,
- STOTE OF THE SECOND WITH STANDARD WITH COMPARED SMICES. (C)
- dispersional contraction and tractional time and a four security. (5)
- CONVEX ON BRINGE DECK
- THE ENHANCE OF THE MED MAPUE, OR STUTNESS FINE

MARK BEAM

PROPOSED PEDESTRIAN BRIDGE OVER MITCHEN CREEK

RICKETTS CLERN STATE PARK LUZZERENE COUNTY, PA

STEER ASSEMBLY SHEETS



POWERS & SCHRAM INC.

ITEM	LA MINI	QUANTITY FORMULA	UNIT	SUBTOTAL	TOTAL
GLUE LAMINATED TIMBER BEAMS		J1*L1*L3*L4(\frac{m^3}{1*10^9 mm^3})	m³	3.25	3.25
DECK		C2*D1*D2 (m <sup>3</sup> / <sub>1*10</sub> s mm <sup>3</sup> )	m <sup>3</sup>	1.37	
RAILING POST		2 (F2+1)(140*140)(1200+D2) (m <sup>3</sup> / <sub>1*10<sup>9</sup> mm<sup>3</sup>)</sub>	m <sup>3</sup>	0.59	3.64
RAILING	SOLID SAWN	$2(3(F1)(191)(38))(\frac{m^3}{1*10^9 \text{ m/m}^3})$	m <sup>3</sup>	0.59	
CURB	Total Text	2(F1)(50)(191)(\frac{m^3}{1*10^9 \text{mm}^3})		0.26	
BLOCKING		2(2(F2-1)(600)(140)(191)+4(900)(140)(191))(m <sup>3</sup> / <sub>1*108 mm<sup>3</sup></sub> )	m³	0.83	
BACKWALL	GLUE	2(S2)(79)(S1)(100 mm <sup>3</sup> )	m <sup>3</sup>	0.17	3.64 0.20 63.45
DIAPHRAGMS	LAMINATED TIMBER	$(G1)J2(L4-100)79(H1-L3)(\frac{m^3}{1*10^9 \text{ mm}^3})$	m³	0.03	
BEARING PLATE ASSEMBLIES	300(5%)	$2(J1)((Q1)(195)(12)+2(150)(100)(12))(\frac{m^3}{1*10^9 \text{ mm}^3})(7580 \frac{\text{kg}}{m^3})$	kg	63.45	63.4
SELECT SURFACE TREATMENT	1350-(4	$(THICKNESS)(C1)D1(\frac{m^3}{1*10^3 mm^3})2250(\frac{kq}{m^3})$	kg	N/A	N/A
152um POLYURETHANE		$2(S2)(S1+D2+300)\left(\frac{m^2}{1+10^6mm^2}\right)$	m²	3.34	3.34

(1) THICKNESS IS DETERMINED BY DESIGNER (10 MAX.)

QUANTITIES FOR	BIKE/ EMEN	RGENCY VEHICLE BRIDGE SUPERSTRUCTURE  QUANTITY FORMULA	UNIT	SUBTOTAL	JOTAL
GLUE LAMINATED TIMBER BEAMS	19-10	J1*L1*L3*L4(m <sup>3</sup> /1*10 <sup>9</sup> mm <sup>3</sup> )	m3	-	0.7.2
DECK	19-0	C2*E1*E2*D2 (m <sup>3</sup> 1*10 <sup>9</sup> mm <sup>3</sup> )	MS		
BACKWALL	GLUE LAMINATED TIMBER	$2(S3)(79)\left(\frac{S1+S2}{2}\right)\left(\frac{m^3}{1*10^8 \text{ m/m}^3}\right)$	m <sup>3</sup>		
DIAPHRAGMS	TIMBER	(G1)J2(L4-100)79(H1-L3)(m <sup>3</sup> / <sub>1*10<sup>9</sup> mrp<sup>3</sup>/</sub>	m³		
RAILING POST		2(F2+1)(140*140)(1550+D2)(1*10*mm³)	m <sup>3</sup>		
RAILING	SOLID SAWN	2(4(F1)(191)(38))(1-40 <sup>8</sup> mm <sup>3</sup> )	m3		
CURB	SAWN	2(F1)(50)(191)(m <sup>3</sup> / <sub>1*10<sup>9</sup> mm<sup>3</sup>)</sub>	m <sub>3</sub>		
BLOCKING		2 (2(F2)(600)(140)(191)+4(900)(140)(191)) (m <sup>3</sup> / <sub>1</sub> 710 <sup>2</sup> mm <sup>3</sup> )	m3		
BEARING PLATE ASSEMBLIES	200	2(J1)((Q1)(195)(12)+2(150)(100)(12))(m <sup>3</sup> / <sub>1*10<sup>9</sup> mm<sup>3</sup>)(7580 m<sup>3</sup>/<sub>m<sup>3</sup></sub>)</sub>	kg		
152um POLYURETHANE		2(S2)(S1+D2+900)(m <sup>2</sup> /(1+10 <sup>6</sup> mm <sup>2</sup> )	m²		
WATERPROOF MEMBRANE		(D1)(C1)(\frac{m^2}{1*10^8 \text{mm}^2})	m²		
BITUMINOUS WEARING COURSE		$(40)(C1)D1\left(\frac{m^3}{1*10^9 \text{ mm}^3}\right)2250\left(\frac{\text{kg}}{m^3}\right)$	kg		

POWERS & SCHRAM INC.
CONSULTING ENGINEERS
STATE COLLEGE, PA



#### GLULAM BEAM

# PROPOSED PEDESTRIAN BRIDGE OVER KITCHEN CREEK

RICKETTS GLENN STATE PARK FAIRMOUNT TOWNSHIP, LUZERENE COUNTY, PA

SERIES NO: SHEET NO: SERIES

DATA ASSEMBLY SHEETS

PATROC SHAWN POWERS

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THESE PLANS ARE INTENDED FOR INFORMATIONAL PURPOSES ONLY AND ARE ACCOMPANIED BY NO WARRANTIES, EXPRESS OR IMPLIED, BY POWERS & SCHAMAI, INC., CONSULTING ENGINEERS. ODISTRUCTION PLANS PREPARED FROM DESIGN AND DETAIL INFORMATION SHOWN HERE IN MUST BE REVIEWED AND APPROVED BY A QUALIFIED PROFESSIONAL ENOIMER FOR SPECIFIC PROLECT REQUIREMENTS.

SHEET 17 of 21

GURAT ROL ZETORTO

Facult or Streets of Commercial in Section (1)

CULLM SEAM
PROPOSED PEDESTRIAN SRIDGE

PROPOSED PEDESTRIAN BRIDGE OVER MITCHEN CREEK

RICKETTS GLENN STATE PARK FAIRMOUNT TOWNSHIP, LUZERENE GOUNTY, PA

DATA ASSEMBLY SHEETS

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ACTURE DE DESENTE ATRIBUTAR DE 19 ACTUANDO EN TOLONO EN CONTROLLA DESENTAR L'AUCULANTICA DE TRANSICIO DE L'ARTE DE L

POWERS & SCHEAK INC

SHEET 17 of 21

A1 SKEW ANGLE A2 % GRADE (LOOKING STATIONS AHEAD) A2 (1) -4-4-62 C1 CURB TO CURB ROADWAY WIDTH (NORMAL) C1 CURB TO CURB ROADWAY WIDTH (NORMAL) C2 (1) 1 1220 C2 DECK WIDTH OUT TO OUT C2 DECK WIDTH OUT TO OUT C3 DECK THICKNESS C4 EACH C5 DECK THICKNESS C5 DECK THICKNESS C6 DECK THICKNESS C7 DECK THICKNESS C8 DECK THICKNESS C9 DECK THICK	ODE	DESCRIPTION	CONTROL DIMENSIONS T SOURCE		VALUE
A2		SKEW ANGLE		(1)	
CI   CURB ROGOWY WOTH (NORMAL)					
22   DECK WIGHT OUT TO OUT					
22   DEC PHICKNESS   D.2					
A BEAM DEPTH USE LA FOR GULLAM BEAM ON ZERO (0) FOR (1) 630  B BEAMING THICKNESS USE TWELVE (12) FOR GULLAM BEAM ON ZERO (1) 12  MINORALL 1 <sup>24</sup> SERW ANGLE USES TWELVE (12) FOR GULLAM BEAM ON ZERO (1) 12  BE SEMBER STORY OF THE SERVE ANGLE USES CONSTRUCTION (1) 43-00'-00' DES CONSTRUCTION (1) 45-00'-00' DES CONSTRUCTION (1) 45-00'-00'-00' DES CONSTRUCTION (1) 45-00'-00'-00'-00'-00'-00'-00'-00'-00'-00					
B BEARING THICKNESS			USE L4 FOR GLULAM BEAM OR ZERO (0) FOR		
AN INVIDICAL TO SEEW ANCIE DESIGNER (150000" MIN., 450000" MAX.) (4) 15-00-00" DESIGNER (150000" MIN., 450000" MIN., 4500000" MIN., 450000" MIN., 4500000" MIN., 45000000" MIN., 45000000 MIN., 450000000 MIN., 4500000000 MIN., 4500000000 MIN., 45000000000000000000000000000000000000	В	BEARING THICKNESS		(1)	12
B	AA.	WINGWALL "A" SKEW ANGLE	DESIGNER (15°00'00" MIN., 45°00'00" MAX.)	(4)	15-00'-00' DEC
\( \text{C} \) \( \text{NOWALL} \text{ \frac{\chi}{\chi} \text{ ENGTH} \\ \text{DESIGNER} \\ \text{(\$\chi)} \\ \text{2250} \\ \text{300} \\ \text{300} \\ \text{NOWALL} \text{ \frac{\chi}{\chi} \text{2250} \\ \text{300} \\ \text{300} \\ \text{NOWALL} \text{ \frac{\chi}{\chi} \text{2250} \\ \text{300} \\ \text{300} \\ \text{NOWALL} \text{ \frac{\chi}{\chi} \text{2250} \\ \text{300} \\ \text{300} \\ \text{NOWALL} \\ \text{ \frac{\chi}{\chi} \text{300}} \\ \text{300} \\ \text{NOWALL} \\ \text{ \frac{\chi}{\chi} \text{300}} \\ \text{300} \\ \text{NOWALL} \\ \text{ \frac{\chi}{\chi} \text{300}} \\ \text{300} \\ \text{100} \\ \te	AB	WINGWALL "B" SKEW ANGLE	DESIGNER (15°00'00" MIN., 45°00'00" MAX.)	(4)	45-00'-00' DEC
10. WINDWALL "9" EXPORTH DESIGNER (4) 2250 38. CHEEKWALL "A" 300 (TAN (ΔΔ)) 39 39. CHEEKWALL "A" 300 (TAN (ΔΔ)) 39 39. CHEEKWALL "A" 300 (TAN (ΔΔ)) 39 39. CHEEKWALL "B" 150 USE CONDITION 1 EQUATIONS, OTHERWISE USE CONDITION 2 EQUATIONS 300 (TAN (ΔΔ)) 190 300	AC	WINGWALL "A" LENGTH			
270   270	AD	WINGWALL "B" LENGTH	DESIGNER		2250
CHEEKWALL "A"   SOO(IAN(\frac{AD}{2})				(./	
F CA ≥ 150 USE CONDITION 1 EQUATIONS, OTHERWISE USE CONDITION 2 EQUATIONS  AS CALCULATED ABOVE   194  CA CHEEKWALL "B"   300 (**M(\$\frac{AB}{2}\$*))   124  CC C CHEEKWALL "B"   150   190  CONDITION 2 EQUATIONS  CHEEKWALL "B"   150   190  CC CHEEKWALL "B"   150 (**M(\$\frac{AB}{2}\$*))   190  CC CHEEKWALL "B"   150 (**M(\$\frac{AB}{2}**))   190  CC CHEKWALL "B"   150 (**M(\$\frac{AB}{2}**))	BB	CHEEKWALL "A"			39
F CA ≥ 150 USE CONDITION 1 EQUATIONS, OTHERWISE USE CONDITION 2 EQUATIONS  AS CALCULATED ABOVE   194  CA CHEEKWALL "B"   300 (**M(\$\frac{AB}{2}\$*))   124  CC C CHEEKWALL "B"   150   190  CONDITION 2 EQUATIONS  CHEEKWALL "B"   150   190  CC CHEEKWALL "B"   150 (**M(\$\frac{AB}{2}\$*))   190  CC CHEEKWALL "B"   150 (**M(\$\frac{AB}{2}**))   190  CC CHEKWALL "B"   150 (**M(\$\frac{AB}{2}**))	CA	CHEEKWALL "B"	$150 - \left(\frac{300}{TAN(A1)}\right) + 300\left(TAN\left(\frac{AB}{2}\right)\right)$		194
DOCUMENT   EQUATIONS   194   24   25   25   25   25   25   25   2	F C	A > 150 USE CONDITION 1 EQUATIONS, OTHERWISE USE			
CHERWALL "B"   150   190   1		DITION 1 EQUATIONS			
CHERWALL "B"   300 (IAN (AB) )   124		CHEEKWALL "B"	AS CALCULATED ABOVE		194
150   150	_				
DOCUMENT   2 GUATRONS   CA CHEERWALL 18"   150	-0	CUCEVANTE R	300 (IMM(2))		124
DOCUMENT   2 GUATRONS   CA CHEERWALL 18"   150	CC	CHEEKWALL "B"	150		150
A CHERWALL "B"  SO (**(N(AB))**  CC CHERWALL "B"  SO (**(N(AB))**  CC CHERWALL "B"  SO (**(N(AB))**  SO (*					
CHEEKWALL "B"  SOO(INN(AB)  CHEEKWALL "B"  SOO(INN(AB)  S		CHEEKWALL "B"	150		
DA   NORWALL   "A" LEIGHH	CB				
DA   NORWALL   "A" LEIGHH	CC	CHEEKWALL "B"	$150 + \left(\frac{300}{14N(A1)}\right) - 300\left(74N\left(\frac{AB}{2}\right)\right)$		
BB   MINGWALL "8" LENGTH	DA.	WINCWALL "A" LENCTH			2880
EA ABUTMENT LENGTH		WINCWALL "D" LENCTH			
SIN(AT)					
SA   ABUTMENT LENGTH			SIN(A1)		
ABUTMENT LENGTH	EB	ABUTMENT LENGTH			2153
29	EC	ABUTMENT LENGTH	EA +BA		1115
FA	ED	ABUTMENT LENGTH			1039
FA	EE	ABUTMENT LENGTH	110 mm TAN(A1)		29
FD	FA	WINGWALL "A" HEIGHT	(20) - (15)1000	(2)	2539
FOO   MINOWALL REINFORCEMENT PROJECTION   DESIGNER   (3)   510		WINGWALL "A" HEIGHT	(20 = (15))1000	(2)	
FOO   MINOWALL REINFORCEMENT PROJECTION   DESIGNER   (3)   510		WINOWALL "A" HEIGHT	(20 - (3)1000	(2)	
B			DESIGNED	(2)	
B   MINOWALL "8" FICHT   (32) - (3)1000   (2)   1594		WINDWALL "D" LICIOLOT		(3)	
AB   HEAPT OF FINISH GRADE CHAMFER (ABUTMENT)   ((10) - (13))1000   (2)   4994		WINGWALL B HEIGHT	(30- (15))1000	(2)	
AB   HEAPT OF FINISH GRADE CHAMFER (ABUTMENT)   ((10) - (13))1000   (2)   4994		WINGWALL B HEIGHT	(32) - (15)/1000	(2)	
AB   HEAPT OF FINISH GRADE CHAMFER (ABUTMENT)   ((10) - (13))1000   (2)   4994		WINDWALL D' HEIGHT		(2)	
HB   REAR FACE REINFORCEMENT PROJECTION (ABUTMENT)   DESIGNER   (3)   310   317   310		WINGWALL REINFORGEMENT PROJECTION	UESIGNER CONTRACT	(3)	
M. ABUTLENT FOOTING WIDTH   DESIGNER   (3)   2725		HEIGHT OF FINISH GRADE CHAMFER (ABUTMENT)		(2)	
B				(3)	
1750   1750					
AB WINGWALL "A" FOOTING WOTH   DESIGNER   (3)   2479				(3)	
AG   WINCWALL "8" FOOTING WOTH   DESIGNER   (3)   1475		ABUTMENT FOOTING WIDTH		(=)	
AG   WINCWALL "8" FOOTING WOTH   DESIGNER   (3)   1475		WINGWALL A FOOTING WIDTH		(3)	
AG   WINCWALL "8" FOOTING WOTH   DESIGNER   (3)   1475		WINGWALL "A" FOOTING WIDTH		(3)	
AG   WINCWALL "8" FOOTING WOTH   DESIGNER   (3)   1475		WINGWALL "A" FOOTING WIDTH			
KA - KB		WINGWALL "B" FOOTING WIDTH		(3)	
LA         ABUTMENT FOOTING LENGTH         EB TANIA(LA) * SIN(LA) * TANIA(LA) * TANIA		WINGWALL "B" FOOTING WIDTH		(3)	
ABUTMENT FOOTING LENGTH   EB+ TANIA(A) = "SIN(A) + TANIA(B)   SIN(AB)	_				
MA WINGWALL "A" FOOTING LENGTH \$\frac{18}{313(AA)} - \frac{18}{71AN(A)}\$ 128  ### WINGWALL "A" FOOTING LENGTH \$\frac{18}{313(AA)} - \frac{71AN(A)}{71AN(A)}\$ 3016  ### WINGWALL "A" FOOTING LENGTH \$\frac{18}{71AN(A)} - \frac{16}{31N(A)}\$ 1726  ### WINGWALL "B" FOOTING LENGTH \$\frac{18}{31N(AS)} - \frac{16}{71AN(AS)}\$ 704  ### WINGWALL "B" FOOTING LENGTH \$\frac{18}{31N(AS)} - \frac{18}{71AN(AS)}\$ 3076	_			-4-15	
MB         WINGWALL "A" FOOTING LENGTH         DA+ \$\frac{118}{3MAJ}\$ \tau^{1/3}MAJ\$         301b           MC         WINGWALL "A" FOOTING LENGTH         DA+ \$\frac{1JC}{3MAJ}\$ \tau^{1/3}MAJ\$         1726           NA         WINGWALL "B" FOOTING LENGTH         \$\frac{18}{3MAJ}\$ \tau^{1/3}MAJ\$         704           NB         WINGWALL "B" FOOTING LENGTH         \$\frac{18}{3MAJB}\$ \tau^{1/3}MAJ\$         307b	LB	ABUTMENT FOOTING LENGTH			2800
MC WINGWALL "A" FOOTING LENGTH DA+ "MC   1726    NA WINGWALL "B" FOOTING LENGTH   18   18   18   18   18    NB WINGWALL "B" FOOTING LENGTH   18   18   18   18    NB WINGWALL "B" FOOTING LENGTH   18   18   18   18    NB WINGWALL "B" FOOTING LENGTH   18   18   18   18    NB WINGWALL "B" FOOTING LENGTH   18   18    NB WINGWALL "B" FOOTING LENGTH   18   18    NB WINGWALL "B" FOOTING LENGTH   18    NB WINGWALL "B" FOOTING LENGT	MA	WINGWALL "A" FOOTING LENGTH			128
NA         WINGWALL "8" FOOTING LENGTH         SIN(AB) — TAN(AB) TAN(AB)         704           NB         WINGWALL "8" FOOTING LENGTH         08+ SIN(AB) — TAN(AB)         3078	MB	WINGWALL "A" FOOTING LENGTH			3018
NB WINGWALL "B" FOOTING LENGTH $DB + \frac{IB}{SIN(AB)} - \frac{KB}{TAN(AB)}$ 3078	МС	WINGWALL "A" FOOTING LENGTH			1726
	NA	WINGWALL "B" FOOTING LENGTH			704
NC WINGWALL "B" FOOTING LENGTH $DB + \frac{KC}{TAN(AB)} - \frac{IC}{SIN(AB)}$ 1199	NB	WINGWALL "B" FOOTING LENGTH			3078
	NC	WINGWALL "B" FOOTING LENGTH	$DB + \frac{KC}{TAN(AB)} - \frac{IC}{SIN(AB)}$		1199

- (1) SEE APPROPRIATE SUPERSTRUCTURE DATA ASSEMBLY SHEETS (SHEETS 1 THRU 4 FOR 101M).
- (2) SEE SHEET 6 OF 101M FOR CONTROL ELEVATIONS.
- (3) DESIGN ABUTMENT AND RETAINING WALLS IN ACCORDANCE WITH AASHTO LEFD SPECIFICATIONS. USE DATA ASSEMBLY AND CONSTRUCTION SHEETS TO CALCULAR THE NECESSARY DIMENSIONS AND REINFORCEMENT FOR THE ABUTMENT (WITHOUT BACKWALL), WINGWALLS, AND SPECAD FOOTING.
- (4) SEE SHEET 6 OF 101M FOR WINGWALL EXAMPLE.

					_
March	Description	By	Chk'd	App'd	Date

SPREAD FOOTING ABUTMENT 2

# PROPOSED PEDESTRIAN BRIDGE OVER KITCHEN CREEK

RICKETTS GLENN STATE PARK

101M

5

FAIRMOUNT TOWNSHIP, LUZERENE COUNTY, PA

ENGINEER'S SEAL

DATA ASSEMBLY SHEETS 10

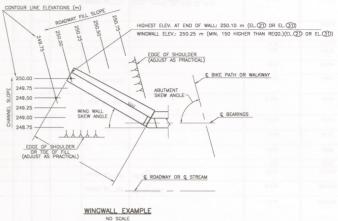
ERIES NO: SHEET NO: SERIES TITLE:

Powers & Schram Inc. CONSULTING ENGINEERS
STATE COLLEGE, PA

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		-30	CONTROL ELEVATIONS		
CODE	DESCRIPTION		SOURCE	A +0.89(4)	VALUE (m)
10	ABUTMENT ELEVATION	1) -60	USE 1) FOR ABUT. 1, OR 2) FOR ABUT. 2	(1)	30.562
0	TOTAL STRUCTURE	BICYCLE/EMERGENCY VEHICLE SUPER.	10-(40-D2-A)(m/1*10 <sup>3</sup> mm)	1-000 2 21	
1	ABUTMENT ELEVATION	PEDESTRIAN SUPERSTRUCTURE	$\bigcirc - \left( D2 - A \right) \left( \frac{m}{1*10^3 \text{ mm}} \right)$		29.856
12	ABUTMENT ELEVATION		$1 + \frac{A2}{100} \left( \frac{EA}{2} (COS(A1)) \right) \left( \frac{m}{1*10^3 mm} \right)$	ABUTMENT 1	29.867
	(USE APPROPRIATE EQUATION DEPENDING ON ABUTMENT NO	.)	$1 - \frac{A2}{100} \left( \frac{EA}{2} (COS(A1)) \right) \left( \frac{m}{1*10^3 mm} \right)$	ABUTMENT 2	
13)	ABUTMENT ELEVATION		$1 - \frac{A2}{100} \left( \frac{EA}{2} (COS(A1)) \right) \left( \frac{m}{1*10^3 \text{mm}} \right)$	ABUTMENT 1	29.845
	(USE APPROPRIATE EQUATION DEPENDING ON ABUTMENT NO	.)	$1 + \frac{A2}{100} \left( \frac{EA}{2} (COS(A1)) \right) \left( \frac{m}{1*10^3 \text{ mm}} \right)$	ABUTMENT 2	2 1015
14)	BOTTOM OF FOOTING ELEVATION	N	DESIGNER		27.712
15)	TOP OF FOOTING ELEVATION		$4 + 450 \left(\frac{m}{1*10^3 \text{ mm}}\right)$		28.162
16)	SCOUR DEPTH		DESIGNER		28.651
20	WINGWALL "A" ELEVATION		$\bigcirc -\left(\frac{A2}{100}\left(\frac{EA}{2}(COS(A1))\right) + 150\right)\left(\frac{m}{1*10^3 mm}\right)$	ABUTMENT 1	30.701
	(USE APPROPRIATE EQUATION DEPENDING ON ABUTMENT NO	.)	$10 + \left(\frac{A2}{100}\left(\frac{EA}{2}(COS(A1))\right) + 150\right)\left(\frac{m}{1*10^3 \text{ mm}}\right)$	ABUTMENT 2	00.701
2	WINGWALL "A" ELEVATION		DESIGNER (SEE WINGWALL EXAMPLE)		29.566
22	WINGWALL "A" ELEVATION		②D+150(m/1*103mm)		29.716
30	WINGWALL "B" ELEVATION		$10 + \left(\frac{A2}{100}\left(\frac{EA}{2}(COS(A1))\right) + 150\right)\left(\frac{m}{1*10^3 mm}\right)$	ABUTMENT 1	30.723
	(USE APPROPRIATE EQUATION DEPENDING ON ABUTMENT NO	).)	$10 - \left(\frac{A2}{100}\left(\frac{EA}{2}(COS(A1))\right) + 150\right)\left(\frac{m}{1*10^3 mm}\right)$	ABUTMENT 2	30.720
3	WINGWALL "B" ELEVATION		DESIGNER (SEE WINGWALL EXAMPLE)		29.566
32	WINGWALL "B" ELEVATION		$3) + 150 \left(\frac{m}{1*10^3 \text{ mm}}\right)$		29.716
_			(1-10-11111)		

IN GENERAL, PROVIDE WINGWALLS OF SUFFICIENT LENGTH TO RETAIN THE ROADWAY EMBANKMENT TO THE REQUIRED EXTENT AND TO FURNISH PROTECTION AGAINST EROSION COMPUTE WINGWALL LENGTHS USING THE ACTUAL CONDITION AT THE SITE. THE FOLLOWING METHOD IS PROPOSED TO COMPUTE THE REQUIRED LENGTHS.



		QUANTITIES			
ITEM		QUANTITY FORMULA	UNIT	SUBTOTAL	TOTAL
CLASS 3 EXCAVATION		DESIGNER	m³	20.0	20.0
CHEEKWALL A	CLASS	$\left(BB+150+\frac{BA-150-BB}{2}\right)300\left(\frac{m^2}{1*10^5 mm^2}\right)\left(20-12\right)$	m³	0.05	
CHEEKWALL B	AA CEMENT	$(CB+150+\frac{150+CB-CA}{2})300(\frac{m^2}{1*10^8 mm^2})(30-13)$ CONDITION 1	rm <sup>3</sup>	0.13	0.18
CHEERWALL B	CONCRETE	$\left(2(CB)-150+\frac{CC+CB-150}{2}\right)300\left(\frac{m^2}{1*10^6\text{mm}^2}\right)\left(30-33\right)$ CONDITION 2	rm <sup>3</sup>		
ABUTMENT		$\left[0.45\left(\boxed{1}\right)-\left(\boxed{5}\right)+\left(\frac{1}{2}\right)\left(\frac{1}{10}\right)\left(\boxed{1}\right)-\left(\boxed{5}\right)^{2}\right]\left(EB\right)\left(\frac{m}{1*10^{3}mm}\right)$	m3	2.51	
WINGWALL A	CLASS	$\left[0.45\left(22\right) + \frac{\text{(1)} - \text{(5)}}{2} - \text{(5)}\right) + \left(\frac{1}{2}\right)\left(\frac{1}{10}\right)\left(22\right) + \frac{\text{(1)} - \text{(5)}}{2} - \text{(5)}\right)^{2}\left[(AC)\left(\frac{m}{1 \cdot 10^{3} \text{ mm}}\right)\right]$	m <sup>3</sup>	31.7	63.4
WINGWALL B	CEMENT CONCRETE	$ \boxed{ \left[ 0.45 \left( \cancel{3}\cancel{2} + \frac{\cancel{3}\cancel{0} - \cancel{3}\cancel{2}}{2} - \cancel{1}\cancel{5} \right) + \left( \frac{1}{2} \right) \left( \frac{1}{10} \right) \left( \cancel{3}\cancel{2} + \frac{\cancel{3}\cancel{0} - \cancel{3}\cancel{2}}{2} - \cancel{1}\cancel{5} \right)^2 \right] (AD) \left( \frac{m}{1 + 10^3  \text{mm}} \right) } $	m <sup>3</sup>	14.5	65.4
FOOTING		$\left(\frac{1}{2}\right)$ (600) $\left((LA+LB)(A)+(MB+MC)(JA)+(NB+NC)(KA)\right)\left(\frac{m^3}{1*10^9 \text{ mm}^3}\right)$	m³	14.7	
SELECTED BORROW EXCAVATION, STRUCTURE BACKFILL		DESIGNER	m <sup>3</sup>	15.0	15.0
NO. 57 COARSE AGGREGATE		4 WEEPHOLES ( 0.4 m <sup>3</sup> )	m <sup>3</sup>	1.6	1.6
REINFORCEMENT BARS		DESIGNER - CALCULATE BAR MASS FROM SHEETS 7 & 8 OF 101M	kg	3606616	36066
REINFORCEMENT BARS, EPOXY COATED	ia.	DESIGNER - CALCULATE BAR MASS FROM SHEETS 7 & 8 OF 101M	kg	937453	93745

FOOTNOTES FOR TABLES

(1) SEE APPROPRIATE SUPERSTRUCTURE DATA ASSEMBLY SHEETS (101M SHEETS 1 THRU 4).



SPREAD FOOTING ABUTMENT 2

PROPOSED PEDESTRIAN BRIDGE OVER KITCHEN CREEK

RICKETTS GLENN STATE PARK
FAIRMOUNT TOWNSHIP, LUZERENE COUNTY, PA

SERIES NO: SHEI

SHEET NO:

DATA ASSEMBLY SHEETS 11



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SHEET 19 of 21





ODMORT FOR LABETS

SEE APPRIMISE SUPERMINISES DATA ASSOCIATE SHEETS
(1014 SHEETS : DHRU A)

PROPOSED PEDESTRIAN BRIDGE

RICKETTS GLENN STATE PARK FARMOUNT TOWNSHIP, LUZERENE COUNTY, PA

AN COL

101

POWERS & SCHOOL INC.

								BAR S										
		SOURCE		SOURCE	NO.	SOURCE	TYPE	A	В	С	Н	J	К	SOURCE	REMARKS	SOURCE	BAR MASS kg/m (4)	
500 1	5		FROM 1655	$[(1) - (3)(\frac{1000}{m})] - 50$	6	$\left\{ \frac{EB - 75}{450} + 0.99 \right\} + 1 \tag{1}$	STR.								VARIES BY4_	$((13-12)(\frac{1000}{m})\frac{1}{NO OF BARS}$	1.570	19622
5_01 1	15 D	ESIGNER (2)	FROM 1655	$ \left[ (\mathfrak{J} - \mathfrak{J}) \left( \frac{1000}{m} \right) \right] - 50 $ $ \left[ (\mathfrak{J} - \mathfrak{J}) \left( \frac{1000}{m} \right) \right] - 50 $	6	$ \left\{ \frac{EB-150(TAN(AA))-150(TAN(AB))}{REQ. SPA. (DESIGNER)} +0.99 \right\} +1  $ (1)(2)	STR.								VARIES BY 4	((13)-(12))(1000) 1 m) NO OF BARS	3.925	81758
502 1	15		TO 1633 2153	$\left[ (\boxed{3} - \boxed{5}) \left( \frac{1000}{\text{m}} \right) \right] -50$		18 SA (18 SA	STR.										1.570	1655G
002	2	***	2153	EB	1	$\left\{ \frac{(1) + (1) - (3) - (5)(\frac{1000}{m}) - 600}{450} + 0.99 \right\} + 1  (2)(3)$	SIR.										1.570	16336
	15		1963	EB-150(TAN(AA))-150(TAN(AB))	4	SAME AS A1502	STR.										1.570	15064
	15		2153	√(③ - ①)²+(EB)²	1	50 3 AV 600 3 A	STR.										1.570	3313
1011	15		1963	V(3) - (2)2+(EB-150(TAN(AA))-150(TAN(AB)))2	1	150(FASKAS))-180(FASKAS))	STR.										1.570	3484
006 1	10		950	$(BA-40)+490+\left(\frac{300}{SIN(A1)}-80\right)$	4	$\left\{ \frac{(20 - 12)(\frac{1000}{m}) - 100}{250} + 0.99 \right\} + 1 \tag{1}$	STR.								BEND IN FIELD		0.785	2983
007 1	10		875	$(CA-40)+(CC-80)+420+\left(\frac{300}{SIN(A1)}-80\right)$	5	$\left\{ \underbrace{(30 - 3) \left(\frac{1000}{m}\right) - 100}_{250} + 0.99 \right\} + 1 \tag{1}$	STR.								BEND IN FIELD		0.785	4439
508 1	15		1284	(20 - (2) (1000 m)+450	5	USE 4 BARS FOR 90° SKEWS, AND 5 BARS ALL OTHER SKEWS	STR.	1	12	100							1.570	9969
509 1	15		1328	(30 - (3) (1000 m) +450	4	(1)	STR.										1.570	8252
510 1			950	PARTY WHATE OUR PORCE	3	$\left\{ \frac{\text{NO. OF BARS FROM A}  01+1}{2} \right\} \tag{1}$		400	175	400			40	150			1.570	7458
	15	120	300		16	3. Drs. (televiser)	STR.										1.570	7536
	15		FROM 1504 TO 2489	FB-50 FA-50	7	$\left\{ \frac{AC - 150}{450} + 0.99 \right\} + 1 \tag{1}$	-								VARIES BY 141	FC NO OF BARS	1.570	72233
5_21 1	15 0	ESIGNER (2)	FROM 1504 TO 2489	FB-50 FA-50	7	$ \left\{ \frac{AC-150}{\text{REQ. SPA. (DESIGNER)}} +0.99 \right\} +1  $ (1)(2)	STR.		199						VARIES BY 141	FC NO OF BARS	3.925	180620
522 1	15		2750	AC-100	10	$\left\{\frac{FB-150}{450}+0.99\right\}+1$ SHOW ON DRAWINGS (1)	-										1.570	148836
		17.50		100.250-8	10	$2\left\{\frac{FB-150}{450}+0.99\right\}+1$ SHOW ON BAR SCHEDULE (1)					1			132			135	93073
523 1	15		FROM 1703	(FC-375)(AC-100) FC	2	$\left\{\frac{FC-675}{450} + 0.99\right\} + 1$ SHOW ON DRAWINGS (1)	STR.				1				VARIES BY 433	(LENGTH FROM 2892 ) - (LENGTH TO 240G)	1.570	22916
			TO <u>838</u>	300(AC-100) FC	4	2{FC-675 450 +0.99}+1 SHOW ON BAR SCHEDULE (TOTAL NO. OF BARS)												
524 1	15		2915	$\sqrt{FC^2 + AC^2} - 100$	1 2	SHOW ON DRAWINGS SHOW ON BAR SCHEDULE (TOTAL NO. OF BARS)	STR.										1.570	24994
525 1	15		975		4	$ \begin{cases} NO. OF BARS FROM W 21+1 \\ 2 \end{cases} $ (1)	3	400	175	400			40				1.570	15308
	15		300		8		STR.										1.570	3768
530 1		CCIONICO	FROM 1504 TO 2511	GB-50 GA-50 GB-50	6	$\left\{\frac{AD - 150}{450} + 0.99\right\} + 1\tag{1}$									VARIES BY 168	GC NO OF BARS	1.570	87838
532 1		ESIGNER (2)	FROM 1504 TO 2511 2150	GB-50 GA-50 AD-100	5	$ \left\{ \frac{AD-150}{REQ. SPA. (DESIGNER)} +0.99 \right\} +1  $ (1)(2)	OTD								VARIES BY 168	GC NO OF BARS	2.355	194770 186516
					10	$ \begin{cases} \frac{GB-150}{450} + 0.99 \\ +1 \end{cases} + 1  \text{Show on Drawings} \qquad (1) \\ 2 \begin{cases} \frac{GB-150}{450} + 0.99 \\ +1 \end{cases} + 1  \text{Show on Bar Schedule} \\ 1  \text{(1)} $											1.070	100016
533 1	15		FROM_1349	(GC-375)(AD-100) GC	2	${6C-675 \over 450} + 0.99 + 1$ SHOW ON DRAWINGS (1)									VARIES BY 354	(LENGTH FROMG213) - (LENGTH TO 2949)	1.570	28768
			TO641	300(AD-100) GC	4	$2\left\{\frac{GC-675}{450}+0.99\right\}+1\frac{SHOW ON BAR SCHEDULE}{(TOTAL NO. OF BARS)}$ (1)	-									NO OF BARS		

- (1) TAKE THE INTEGER VALUE OF THE QUANTITY WITHIN THE
- (2) DESIGN ABUTMENT AND RETAINING WALLS IN ACCORDANCE WITH ASSHTO LRFD SPECIFICATIONS. USE DATA ASSEMBLY AND CONSTRUCTION SHEETS TO CALCULAR THE RECESSARY DIMENSIONS AND REINFORCEMENT FOR THE ABUTMENT (WITHOUT BACKWALL), WINGWALLS, AND SPREAD FOOTING.
- (3) TAKE THE ABSOLUTE VALUE OF THE QUANTITY WITHIN THE | |
- (4) USE TABLE 1 ON THIS SHEET TO COMPLETE BAR MASS QUANTITIES.
- (5) TOTAL BAR MASS = (BAR LENGTH OR AVERAGE BAR LENGTH)(TOTAL NO. OF BARS)(BAR MASS)

BAR SIZE	HOOK DI	NDED END MENSIONS RADES) HOOKS	BAR MASS
	A	J	kg/m
10	150	90	0.785
15	180	130	1.570
20	220	160	2.355
25	280	200	3.925
30	400	300	5.495
35	470	360	7.850
45	670	530	11.775
55	860	680	19.625
	A	+ 1	



SPREAD FOOTING ABUTMENT 2

# PROPOSED PEDESTRIAN BRIDGE OVER KITCHEN CREEK

RICKETTS GLENN STATE PARK
FAIRMOUNT TOWNSHIP, LUZERENE COUNTY, PA

SERIES NO: SH

SHEET NO: S

DATA ASSEMBLY SHEETS 12



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SHEET 20 of 21

								-	BAR S	CHEC	ULE								
MARK	SIZE	SOUR	RCE	LENGTH	SOURCE	NO.	SOURCE	TYPE	A	В	С	Н	J	K	SOURCE	REMARKS	SOURCE	BAR MASS kg/m (4)	
1534	15			2365	$\sqrt{GC^2 + AD^2} - 100$	1 2	SHOW ON DRAWINGS SHOW ON BAR SCHEDULE (TOTAL NO. OF BARS)	STR.									PRE- NET	1.570	31246
1535	15	18.9		975	HONE AND THE PERSON	3	$\left\{ \frac{\text{NO. OF BARS FROM W}}{2} \frac{31+1}{2} \right\} $ (1	3	400	175	400			40	7017 1 00	B THE STATE OF	EL HISTORIOSTEN GOLDEN CAMBER	1.570	26023
1536	15			300		8		STR.									1,000 1000 1 000 1 000	1.570	3768
15 00	15	DESIG (2	NER )	2525	IA-200	6	$\left\{ \frac{\text{LA}-150}{\text{REQ. SPA. (DESIGNER)}} + 0.99 \right\} + 1$ (1)(2	STR.							3000 = 3			5.495	32970
15 01	15	DESIG (2	NER )	2525	IA-200	6	$\left\{ \frac{\text{LA}-150}{\text{REQ. SPA. (DESIGNER)}} + 0.99 \right\} + 1$ (1)(2)	STR.										2.355	14130
1502	15	OUT	70 000	2061	LA-200	7	$\left\{\frac{IA-200}{450} + 0.99\right\} + 1$ (1	STR.										1.570	13018
1003	10	1000	6.14 05	550	1 700.5	16	$\left(\left\{\frac{-\text{IA}-200}{950}+0.99\right\}+1\right)\left(\left\{\frac{-\text{IA}-150}{950}+0.99\right\}+1\right)$ (1	2	125	300	125	75						0.785	5181
1504	15			900	11.12	6	$\left\{ \frac{EB}{450} + 0.99 \right\} + 1$ (1	STR.							8000 [34			1.570	8478
15 06	15	DESIG (2	NER!)	1040	HB+350+A FOR "A" VARIABLE SEE TABLE 1	6	{ EB-150(TAN(AA))-150(TAN(AB)) +0.99}+1 (1)(2	0							SEE TABLE 1 (B = HB + 350)			3.925	54165
15 20	15	DESIG (2	NER	2275	JA-200	8	$   \left\{ \frac{MB-150}{REQ. SPA. (DESIGNER)} + 0.99 \right\} + 1  $ (1)(2)	STR.										5.495	104405
15 21	15	DESIG (2	ENER	2275	JA-200	8	{ MB-150 REQ. SPA. (DESIGNER) +0.99}+1 (1)(2	) STR.										1.570	29830
1522	15	900	20180	2818	MB-200	7	$\left\{\frac{JA-200}{450}+0.99\right\}+1$ (1	) STR.										1.570	49480
1023	10	100		700	THE PERFORMANCE 1925	20	$\left(\left\{\frac{JA-200}{950}+0.99\right\}+1\right)\left(\left\{\frac{MB-150}{950}+0.99\right\}+1\right)$ (1	) 2	125	300	125	75			10000 [7]			0.785	16485
1524	15	0.00	e. no.	900	Page 191-19	7	$\left\{ \frac{AC - 150}{450} + 0.99 \right\} + 1 \tag{1}$	) STR.							I man I is			1.570	26847
15.2	15	DESIG	ENER	1040	FD+350+A FOR "A" VARIABLE SEE TABLE 1	13	$ \begin{cases} AC-150 \\ REQ. SPA. (DESIGNER) + 0.99 \\ + 1 \end{cases} + 1 $ (1)(2)	) ①							SEE TABLE 1 (B = FD + 350)			3.925	180864
15_30	15	DESIG	ENER	1775	KA-200	8		) STR.										2.355	82425
15 3	15	DESIG	SNER	1775	KA-200	8	\[ \begin{align*} \text{NB-150} & \text{REQ. SPA. (DESIGNER)} & \text{+0.99} \\ \text{+1} & \text{(1)(2)} \end{align*}	) STR.							1 1000			1.570	68950
1532	15			2878	NB-200	5	$\frac{KA-200}{450}+0.99$ +1 (1	) STR.							14000 [1]	3		1.570	63108
1033	10	1	000	700	mot see as atom	15	$\left(\left(\frac{KA-200}{950}+0.99\right)+1\right)\left(\frac{NB-150}{950}+0.99\right)+1\right)$ (1	) ②	125	300	125	75			1000	1 19 1 1951 3		0.785	19782
1534	15	90.80		900	1 (2) OF \$1000 11 11 11 11 11 11 11 11 11 11 11 11	6	$\left\{\frac{AD-150}{450}+0.99\right\}+1$ (1	) STR.								8 - 2 - 22 - 3		1.570	32499
15 3	5 15	DESIG	SNER	1040	GD+350+A FOR "A" VARIABLE SEE TABLE 1	6	{ AD-150 REQ. SPA. (DESIGNER) +0.99}+1 (1)(2)	) ①							SEE TABLE 1 (B = GD + 350)	0 10 10 10	1150 1210 114 11 14	2.355	99475

- (1) TAKE THE INTEGER VALUE OF THE QUANTITY WITHIN THE }
- (2) DESIGN ABUTMENT AND RETAINING WALLS IN ACCORDANCE WITH AASHTO LRFD SPECIFICATIONS. USE DATA ASSEMBLY AND CONSTRUCTION SHEETS TO CALCULAR THE RECESSARY DIMENSIONS AND REINFORCEMENT FOR THE ABUTMENT (WITHOUT BACKWALL), WINGWALLS, AND SPECAD FOOTING.
- (3) TAKE THE ABSOLUTE VALUE OF THE QUANTITY WITHIN THE
- (4) USE TABLE 1 ON THIS SHEET TO COMPLETE BAR MASS QUANTITIES.
- (5) TOTAL BAR MASS = (BAR LENGTH OR AVERAGE BAR LENGTH)(TOTAL NO. OF BARS)(BAR MASS)

BAR SIZE	HOOK DI	NDED END MENSIONS RADES) HOOKS	BAR MASS
	A	J	kg/m
10	150	90	0.785
15	180	130	1.570
20	220	160	2.355
25	280	200	3.925
30	400	300	5.495
35	470	360	7.850
45	670	530	11.775
55	860	680	19.625
	<u></u>	1	



SPREAD FOOTING ABUTMENT 2

# PROPOSED PEDESTRIAN BRIDGE OVER KITCHEN CREEK

RICKETTS GLENN STATE PARK FAIRMOUNT TOWNSHIP. LUZERENE COUNTY, PA

101M

8

DATA ASSEMBLY SHEETS



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SHEET 21 of 21



ODE	DESCRIPTION		ONTROL DIMENSIONS SOURCE		VALUE	
A1	SKEW ANGLE		DESIGNER		VALUE	DEG
A2	% GRADE (LOOKING STATIONS AHEAD)		DESIGNER			DEG
B1	SPAN LENGTH- ¢ TO ¢ BEARING		DESIGNER			_
						_
B2	FRONT FACE TO FRONT FACE OF ABUTMEN	TS	$\left(81 - \frac{220}{SIN(A1)}\right)$		100	
B3	WATERWAY OPENING		(B2)SIN(A1)			
C1	CURB TO CURB ROADWAY WIDTH (NORMAL)		TABLE 1		100	
C2	DECK WIDTH OUT TO OUT		C1+382			
D1	OUT TO OUT DECKING ALONG & OF ROADWA	Υ	B1+380 SIN(A1)			
D2	DECK THICKNESS		TABLE 1			
E1	NUMBER OF DECK PANELS		{D1*SIN(A1)} 1200	(1)		
E2	DECK PANEL WIDTH ALONG & OF ROADWAY	COMPLETE	D1 E1			
E3	DECK PANEL WIDTH (NORMAL)	FOR	E2*SIN(A1)			_
	NUMBER OF LAG SCREWS PER	DECK	{ E2-300 + 1}			-
E4	DECK PANEL PER BEAM	ONLY	( 300 )	(1)		
E5	LAG SCREW SPACING		E2-300 E4-1	The Paris		
F1	OUT TO OUT PARAPET LENGTH		D1+ 191 TAN(A1)	(%)		
F2	NUMBER OF GUIDE RAIL TIMBER POST SPA	CES	$\left\{ \frac{D1-1200}{1200} \right\}$	(1)		
F3	GUIDE RAIL POST SPACING		D1-1200 F2	PROTRETES POR		
G1	NUMBER OF DIAPHRAGMS		TABLE 1			
H1	BEAM SPACING (NORMAL)		TABLE 1			
Н2	BEAM SPACING ALONG SKEW		H1 SIN(A1)			
J1	NUMBER OF BEAMS		TABLE 1			
J2	NUMBER OF BEAM SPACES		J1-1			
K1	€ FASCIA TO € FASCIA BEAM		H1*J2			
K2	© FASCIA TO © FASCIA BEAM ALONG SKEW		H2*J2			-
кз	€ FASCIA BEAM TO OUTSIDE FACE OF DECI	(	1/2 (C2-K1)			
L1	BEAM LENGTH (OUT TO OUT OF BEAM)	OPE SEKE,	B1+ 222 SIN(A1)	WELLSTINE.	1905	
L2	GLULAM BEAM SPECIES COMBINATION		DESIGNER	(5)		
L3	BEAM WIDTH		TABLE 1	\-/		
L4	BEAM DEPTH		TABLE 1			
М1	PRE-FABRICATED CAMBER		TABLE 1			
M5	NET FINAL CAMBER		TABLE 1			
Q1	BEARING PLATE WIDTH		L3+36 SIN(A1) + 250			
S1	BACKWALL DEPTH		L4+12			-
	4000	CONCRETE ABUTMENTS	C2 SIN(A1)			
S2	BACKWALL LENGTH	TIMBER SILL ABUTMENTS	$\frac{C2}{SIN(A1)} + \frac{76}{SIN(AA)} + \frac{76}{SIN(AB)} + 200$	(2)		

	CONTROL ST	TATIONS AND ELEVATION	VS	
CODE	LOCATION	SOURCE	VALU	E (m)
CODE	LOCATION	SOURCE	STATION	P.G. ELEV.
0	@ BICYCLE PATH OR WALKWAY AT @ BRG. ABUT.1	DESIGNER		
0	© BICYCLE PATH OR WALKWAY AT © BRG. ABUT.2	DESIGNER		
9	& BICYCLE PATH OR WALKWAY AT BEGIN OF STR.		77	
<b>(3)</b>	& BICYCLE PATH OR WALKWAY AT END OF STR.	$STA \bigcirc + \frac{190}{SIN(A1)} \left(\frac{m}{1*10^3 \text{ mm}}\right)$	F-1777	

	T		170	LE 1	- D	23101	N DATA (3				
SPAN (B1) mm	CURB TO CURB (C1)	DECK THICK. (E1)	BEAM SPA. (H1)	NO. OF BEAMS (J1)	BEAM WIDTH (L3) mm	BEAM DEPTH (L4)	PRE- FABRICATED CAMBER (M1)	NET FINAL CAMBER (M5) mm	NO. OF DIAPHRAGMS (G1)	BRIDGE TYPE	
	1220	64	496	3	79	175	3	1	0		
3000	1625	64	698	3	79	210	3	0	0	PEDESTRIAN	
	3600	79	1020	4	79	315	4	1	0	BIKE/EMERGENC	
	1220	64	496	3	79	245	5	1	0	PEDESTRIAN	
4000	1625	64	698	3	79	280	4	1	0		
	3600	79	1020	4	79	385	8	1	0	BIKE/EMERGENC	
	1220	64	496	3	79 79	280	8 7	1	1	PEDESTRIAN	
5000	1625	64	698	3 4	79	315 455	12	1 2	1		
	3600 1220	79 64	1020	3	79	350	9		1	BIKE/EMERGENC	
6000	1625	64	698	3	79	385	9	2	1	PEDESTRIAN	
0000	3600	79	1020	- 3	79	455	20	3	1	BIKE/EMERGENC	
	1220	64	496	3	79	385	13	2	1		
7000	1625	64	698	3	79	455	11	2	1	PEDESTRIAN	
, 000	3600	79	1020	4	79	560	25	4	1	BIKE/EMERGENC	
	1220	64	496	3	79	455	15	2	1		
8000	1625	64	698	3	79	490	15	3	1	PEDESTRIAN	
	3600	79	1020	4	79	595	36	6	1	BIKE/EMERGENC	
	1220	64	496	3	79	525	17	3	1	PEDESTRIAN	
9000	1625	64	698	3	79	560	17	3	2		
	3600	79	1020	4	79	665	41	7	1	BIKE/FMERGENC	
	1220	64	496	3	79	560	22	4	2	PEDESTRIAN	
10000	1625	64	698	3	79 79	630	19	3	2		
	3600 1220	79 64	1020	3	79	735 630	47 24	8	2	BIKE/EMERGENC	
11000	1625	64	698	3	130	595	26	4	2	PEDESTRIAN	
11000	3600	79	1020	4	130	630	70	12	1	BIKE/EMERGENC	
-	1220	64	496	3	130	560	36	6	1	-	
12000	1625	64	698	3	130	630	32	5	1	PEDESTRIAN	
	3600	79	1020	4	130	770	74	12	1	BIKE/EMERGENC	
	1220	64	496	3	130	630	38	6	1		
13000	1625	64	698	3	130	700	34	6	1	PEDESTRIAN	
	3600	79	1020	4	130	735	90	15	1	BIKE/EMERGENC	
	1220	64	496	3	130	665	46	8	1	PEDESTRIAN	
14000	1625	64	698	3	130	735	41	7	1		
	3600	79 64	1020	3	130	805	94 53	16	1	BIKE/EWERGENC	
15000	1220	64	496	3	130	700 805	53	9 7	1	PEDESTRIAN	
13000	1625 3600	79	1020	4	130	875	98	16	1	BIKE/EMERGENC	
	1220	64	496	3	130	770	56	9	1	-	
16000	1625	64	698	3	130	840	51	8		PEDES I RIAN	
. 5000	3600	79	1020	4	130	910	114	19	2 2	BIKE/EMERGENC	
	1220	64	496	3	130	805	64	11	2		
17000	1625	64	698	3	130	910	54	9	2	PEDESTRIAN	
	3600	79	1020	4	130	980	119	20	2	BIKE/EMERGENC	
	1220	64	496	3	130	840	73	12	2	PEDESTRIAN	
18000	1625	64	698	3	130	945	62	10	2		
	3600	79	1020	4	130	1050	124	21	2	BIKE/EMERGENC	

- (1) ROUND TO THE NEXT WHOLE NUMBER ONLY WITHIN } }
- (2) SEE SHEET 11 OF 101M FOR VARIABLES "AA" AND "AB"
- (3) BEAMS DESIGNED WITH APPROPRIATE WET USE & SIZE FACTOR.
- (4) DESIGN TABLE DO NOT ACCOUNT FOR VERTICAL OR HORIZONTAL CURVES ON BRIDGE DECK.
- (5) USE EITHER DOUGLAS FIR, RED MAPLE, OR SOUTHERN PINE AS PER SHEET 2 OF 100M.

Mark	Description	Bv	Chk'd	App'd	Date

Mark Des	scription REVISIO	Ву	Chk'd	App'd	Date
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ENGINEER'S SEAL	SERIES NO:	SHEET NO:	DATA ASSEMBLY SHEETS

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I I WHITE YOU W RESERVE TANK THE DE CHOICE (1)

1 3 MINUTES A TOTAL OF MARRIED STOLEN DESIGNATION OF CONTRACT (1)

ALTERNATION OF THE CONTRACT OF

(4) DESKIN TABLE OF MOT ACCOUNT FOR VERTICAL OR HORIZONS CHARGES ON TRADES ORGAN.

USE ETHER COUGLAS THE RED MARIE, OR SOUTHORN FIVE

TE PAGE ATE MITTED AT RETRIBUTED REPORTS ONLY HE ACCOUNTED IN IN HIGHER TEN PAGE AT THE PA

POWERS & SCHOOL INC.

SHEET of

QUAN	ITITIES FOR PED	DESTRIAN BRIDGE SUPERSTRUCTURE			
ITEM		QUANTITY FORMULA	UNIT	SUBTOTAL	TOTAL
GLUE LAMINATED TIMBER BEAMS		J1*L1*L3*L4(\frac{m^3}{1*109 mm^3})	m <sup>3</sup>		
DECK	(customs / / /	$C2*D1*D2\left(\frac{m^3}{1*10^9 \text{ mm}^3}\right)$	m <sup>3</sup>		
RAILING POST		2 (F2+1)(140*140)(1200+D2) (m <sup>3</sup> / <sub>1*10<sup>9</sup> mm<sup>3</sup></sub> )	m <sup>3</sup>		
RAILING	SOLID SAWN	$2(3(F1)(191)(38))(\frac{m^3}{1*10^9 \text{ mm}^3})$	m3		
CURB		2(F1)(50)(191)(\frac{m^3}{1*10^8 \text{mm}^3})	rm <sup>3</sup>		
BLOCKING		$2(2(F2-1)(600)(140)(191)+4(900)(140)(191))(\frac{m^3}{(1*10^9 \text{ mm}^3)})$	m <sup>3</sup>		
BACKWALL	GLUE	2(S2)(79)(S1)(1*10° mm <sup>3</sup> )	m3		
DIAPHRAGMS	TIMBER	$(G1)J2(L4-100)79(H1-L3)(\frac{m^3}{1*10^9 \text{ mm}^3})$	m³		
BEARING PLATE ASSEMBLIES	se la	$2(J1)(Q1)(195)(12)+2(150)(100)(12)(\frac{m^3}{1*10^9 \text{ mm}^3})(7580 \frac{\text{kg}}{m^3})$	kg		
SELECT SURFACE TREATMENT	91	$(THICKNESS)(C1)D1(\frac{m^3}{1*10^9 mm^3})2250(\frac{kq}{m^3})$	kg		
152um POLYURETHANE	or someons 1 50	$2(S2)(S1+D2+300)\left(\frac{m^2}{1*10^6mm^2}\right)$	m²		

(1) THICKNESS IS DETERMINED BY DESIGNER (10 MAX.)

QUANTITIES FOR E	BIKE/EMER	GENCY VEHICLE BRIDGE SUPERSTRUCTURE			
ITEM		QUANTITY FORMULA	UNIT	SUBTOTAL	TOTAL
GLUE LAMINATED TIMBER BEAMS		J1*L1*L3*L4\(\frac{m^3}{1*10^9 mm^3}\)	m <sup>3</sup>		
DECK		C2*E1*E2*D2 (m³/(1*10*)mm³/)	m <sup>3</sup>		
BACKWALL	GLUE LAMINATED TIMBER	$2(S3)(79)\left(\frac{S1+S2}{2}\right)\left(\frac{m^3}{1*10^9 \text{ mm}^3}\right)$	m <sup>3</sup>		
DIAPHRAGMS	IIMDER	$(G1)J2(L4-100)79(H1-L3)(\frac{m^3}{1*10^9 \text{ mm}^3})$	m³		
RAILING POST		2 ((F2+1)(140*140)(1550+D2)) (m <sup>3</sup> / <sub>1*10<sup>9</sup> mm<sup>3</sup></sub> )	m³		
RAILING	SOLID SAWN	$2(4(F1)(191)(38))(\frac{m^3}{1*10^9 \text{ mm}^3})$	m <sup>3</sup>		
CURB		2(F1)(50)(191)(\frac{m^3}{1*10^9 mm^3})	m <sup>3</sup>		
BLOCKING		$2(2(F2)(600)(140)(191)+4(900)(140)(191))(\frac{m^3}{1*10^9 \text{ mm}^3})$	m3		
BEARING PLATE ASSEMBLIES		$2(J1)(Q1)(195)(12)+2(150)(100)(12)(\frac{m^3}{1*10^9 \text{ mm}^3})(7580 \frac{kq}{m^3})$	kg		
152um POLYURETHANE		$2(S2)(S1+D2+900)\frac{m^2}{1*10^6 \text{ mm}^2}$	m²		
WATERPROOF MEMBRANE		$(D1)(C1)\left(\frac{m^2}{1*10^6 \text{ mm}^2}\right)$	m²		
BITUMINOUS WEARING COURSE	0010 10	$(40)(C1)D1\left(\frac{m^3}{1*10^9 \text{ mm}^3}\right)2250\left(\frac{\text{kg}}{\text{m}^3}\right)$	kg		

Mark	Description	By	Chk'd	App'd	Date
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GLULAM BEAM

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ENGINEER'S SEAL

SERIES NO: 101M

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DATA ASSEMBLY SHEETS

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(1) THORIES IS DETERMINED BY DESIGNER (10 M

CLURAM BEAM

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POWERS & SCHRAM INC.

		CONTROL DIMENSIONS			
ODE	DESCRIPTION	SOURCE	THE WATER CONTRACTOR	VALUE	
A1	SKEW ANGLE	DESIGNER	ORMANIA		DEG
A2	% GRADE (LOOKING STATIONS AHEAD)	DESIGNER			
B1	SPAN LENGTH- & TO & BEARING	DESIGNER			
82	FRONT FACE TO FRONT FACE OF ABUTMENTS	$\left(81 - \frac{220}{SIN(A1)}\right)$			
B3	WATERWAY OPENING	(B2)SIN(A1)			
C1	CURB TO CURB ROADWAY WIDTH (NORMAL)	TABLE 1	men's		
C2	DECK WIDTH OUT TO OUT	C1+382			
C3	DECK WIDTH OUT TO OUT ALONG SKEW	C2 SIN(A1)			
D1	OUT TO OUT LONGITUDINAL PANEL LENGTH	B1+380 SIN(A1)	amount of 3		
D2	NUMBER OF LONGITUDINAL PANELS	TABLE 1	(1)		
E1	LONGITUDINAL PANEL SPECIES COMBINATION	TABLE 1	Charles and the same		
E2	LONGITUDINAL PANEL DEPTH	TABLE 1	100		
E3	LONGITUDINAL PANEL WIDTH (NORMAL)	<u>C2</u> <u>D2</u>			
E4	LONGITUDINAL PANEL WIDTH ALONG SKEW	<u>C3</u> <u>02</u>	CONTRACTOR FOR THE C		
F1	OUT TO OUT PARAPET LENGTH	D1+ 191 TAN(A1)	(1) THICHOLD IS SETTING		rin si
F2	NUMBER OF GUIDE RAIL TIMBER POST SPACES	$\left\{ \frac{D1-1200}{1200} \right\}$	(1)		
F3	GUIDE RAIL POST SPACING	D1-1200 F2			
G1	NUMBER OF CONTINUOUS STIFFENER BEAMS	TABLE 1			
J1	BEARING PAD LENGTH CONSTRAINT #1	$\frac{E4}{2} - \frac{125}{2} - \frac{100}{TAN(A1)} - 50$	(CONCRETE ABUTMENT)		
0.	DENING FAD ECIGIN CONSTITUTING	$\frac{E4}{3} - \frac{125}{2} - \frac{100}{TAN(A1)} - 50$	(PILE ABUTMENT)		
J2	BEARING PAD LENGTH CONSTRAINT #2	$\frac{E4}{3}$ - 125	(PILE ABUTMENT)		
J3	BEARING PAD LENGTH	USE THE VALUE J1	(CONCRETE ABUTMENT)		
00	DENGINO I AD CENTONI	USE THE LESSER VALUE BTWN. J1 & J2	(PILE ABUTMENT)		
J4	NUMBER OF BEARING PADS	D2*4	(CONCRETE ABUTMENT)		
0-1	HOWDER OF BEARING FAUS	D2*6	(PILE ABUTMENT)		

	CONTROL STA	TIONS AND ELEVATIONS		
CODE	LOCATION	SOURCE	VALU	JE (m)
CODE	LOCATION	SOURCE	STATION	P.G. ELEV.
0	& BICYCLE PATH OR WALKWAY AT & BRG. AE	BUT.1 DESIGNER		
0	€ BICYCLE PATH OR WALKWAY AT € BRG. AE	BUT.2 DESIGNER		
3	& BICYCLE PATH OR WALKWAY AT BEGIN OF	STR. STA $\bigcirc -\frac{190}{\text{SIN(A1)}} \left(\frac{\text{m}}{1*10^3 \text{mm}}\right)$		
<b>(1)</b>	& BICYCLE PATH OR WALKWAY AT END OF	STR. $STA \bigcirc + \frac{190}{SIN(A1)} \left( \frac{m}{1*10^3 \text{ mm}} \right)$		

	TABLE 1 -	- DESIGN D	ATA (2,3,4)	
SPAN (B1) mm	CURB TO CURB (C1) mm	PANEL DEPTH (L4)	NO. OF STIFFENER BEAMS (G2)	BRIDGE TYPE
3000	1220 1625	130	0	PEDESTRIAN
3000	3600	175	1	BIKE\EMERGENCY
4000	1220 1625	130 130	0	PEDESTRIAN
4000	3600	219	1	BIKE\EMERGENC
5000	1220 1625	219 219	0	PEDESTRIAN
	3600	219	2	BIKE\EMERGENC*
6000	1220 1625	219 219	0	PEDESTRIAN
	3600	219	2	BIKE\EMERGENC"

- (1) ROUND TO THE NEXT WHOLE NUMBER ONLY WITHIN { }
- (2) PANELS DESIGNED WITH APPROPRIATE WET USE & SIZE FACTOR.
- (3) DESIGN TABLE DO NOT ACCOUNT FOR VERTICAL OR HORIZONTAL CURVES ON BRIDGE DECK.
- (4) USE EITHER DOUGLAS FIR, RED MAPLE, OR SOUTHERN PINE AS PER SHEET 2 OF 100M.

Mark	Description	Bv	Chk'd	App'd	Date
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GLULAM LONGITUDINAL PANEL

SHEET NO: SERIES NO: SERIES TITLE: 101M 3

DATA ASSEMBLY SHEETS

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SHEET of

QUANTI	TIES FOR PE	DESTRIAN BRIDGE SUPERSTRUCTURE			
ITEM		QUANTITY FORMULA	UNIT	SUBTOTAL	TOTAL
GLUE LAMINATED LONGITUDINAL PANELS		C2*E2*D1\(\frac{m^3}{1*10^9 mm^3}\)	m <sup>3</sup>		
GLUE LAMINATED STIFFENER BEAMS		$(G1)(150)^{2}(C3)\left(\frac{m^{3}}{1*10^{9} \text{ mm}^{3}}\right)$	m <sup>3</sup>		
RAILING POST		2(F2+1)(140*140)(1200+D2)(\frac{m^3}{1*10^9 \text{mm}^3})	m³		
RAILING	SOLID SAWN	$2(3(F1)(191)(38))(\frac{m^3}{1*10^9 \text{ mm}^3})$	m <sup>3</sup>		
CURB		2(F1)(50)(191)(m <sup>3</sup> / <sub>1*10<sup>8</sup> mm<sup>3</sup>)</sub>	m3		
BLOCKING		$2(2(F2-1)(600)(140)(191)+4(900)(140)(191))(\frac{m^3}{1*10^9 \text{ mm}^3})$	m <sup>3</sup>		
SELECT SURFACE TREATMENT		$(THICKNESS)(C1)D1(\frac{m^3}{1*10^8 mm^3})2250(\frac{kq}{m^3})$ (1)	kg		
152um POLYURETHANE		$2(C3)(E2+300)\left(\frac{m^2}{1*10^5 mm^2}\right)$	m²		

(1) THICKNESS IS DETERMINED BY DESIGNER (10 MAX.)

QUANTITIES FOR	BIKE/EMER	GENCY VEHICLE BRIDGE SUPERSTRUCTURE			
ITEM		QUANTITY FORMULA	UNIT	SUBTOTAL	TOTAL
GLUE LAMINATED LONGITUDINAL PANELS		$C2*E2*D1\left(\frac{m^3}{1*10^9 \text{ mm}^3}\right)$	m³		
GLUE LAMINATED STIFFENER BEAMS		$(G1)(150)^2(C3)\left(\frac{m^3}{1*10^9 \text{mm}^3}\right)$	m <sup>3</sup>		
RAILING POST	1738(23)	2((F2+1)(140*140)(1550+D2))(\frac{m^3}{1*10^9\text{ mm}^3})	m3		
RAILING	SOLID	$2(4(F1)(191)(38))(\frac{m^3}{1*10^9 \text{ mm}^3})$	m3		
CURB	SAWN	$2(F1)(50)(191)\left(\frac{m^3}{1*10^9 \text{ mm}^3}\right)$	m <sup>3</sup>		
BLOCKING		$2(2(F2-1)(600)(140)(191)+4(900)(140)(191))(\frac{m^3}{1*10^9 \text{ mm}^3})$	m3		
152um POLYURETHANE		$2(C3)(E2+900)\left(\frac{m^2}{1*10^6 \text{ mm}^2}\right)$	m²		
WATERPROOF MEMBRANE		(D1)(C1)(m <sup>2</sup> /1+10 <sup>8</sup> mm <sup>2</sup> )	m²		
BITUMINOUS WEARING COURSE		$(40)(C1)D1\left(\frac{m^3}{1*10^9 \text{ mm}^3}\right)2250\left(\frac{\text{kg}}{m^3}\right)$	kg		

Mark	Description	By	Chk'd	App'd	Date
	REVISIO				

GLULAM LONGITUDINAL PANEL

PREPARED BY:

POWERS & SCHRAM INC.

CONSULTING ENGINEERS STATE COLLEGE, PA

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SERIES NO: 101M

ERIES NO: SHEET NO: 4

DATA ASSEMBLY SHEETS

COOTHOTE FOR TABLE?

(1) THOOMESS IS DETERMINED BY DESIGNED (10 MAK.)

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POWERS & SCHRAM INC.

CODE	MOLEGIGGGGG	CONTROL DIMENSIONS	3/41115
A1	DESCRIPTION SKEW ANGLE	SOURCE (1)	VALUE
A2	% GRADE (LOOKING STATIONS AHEAD)	A1 (1) A2 (1)	DEG.
C1	CURB TO CURB ROADWAY WIDTH (NORMAL)	A2 (1)	
C2	DECK WIDTH OUT TO OUT	C1 (1)	
		C2 (1)	
D2	DECK THICKNESS	02 (1)	
Α	BEAM DEPTH	USE L4 FOR GLULAM BEAM OR ZERO (0) FOR (1) LONG. PANEL	
В	BEARING THICKNESS	USE TWELVE (12) FOR GLULAM BEAM OR TWENTY (20) FOR LONG. PANEL (1)	
AA	WINGWALL "A" SKEW ANGLE WINGWALL "B" SKEW ANGLE	DESIGNER (15'00'00" MIN., 45'00'00" MAX.) (4) DESIGNER (15'00'00" MIN., 45'00'00" MAX.) (4)	DEG.
AB	WINGWALL "B" SKEW ANGLE	DESIGNER (15°00'00" MIN., 45°00'00" MAX.) (4)	DEG
AC	WINGWALL "A" LENGTH	DESIGNER (4)	
AD	WINGWALL "B" LENGTH	DESIGNER (4)	
BA	CHEEKWALL "A"	$150+\left(\frac{300}{TAN(A1)}\right)+300\left(TAN\left(\frac{AA}{2}\right)\right)$	4200000
BB	CHEEKWALL "A"	300 (TAN(AA))	and the second
CA	CHEEKWALL "B"	$150 - \left(\frac{300}{TAN(AT)}\right) + 300\left(TAN\left(\frac{AB}{2}\right)\right)$	
15.0	L ASS USE CONDITION A SOUTHOUS OF USERNOS LINES		
IF C	A ≥ 150 USE CONDITION 1 EQUATIONS, OTHERWISE USE	CONDITION 2 EQUATIONS	
	OTTION 1 EQUATIONS	I se estado esta	
	CHEEKWALL "B"	AS CALCULATED ABOVE	
CB	CHEEKWALL "B"	$300\left(TAN\left(\frac{AB}{2}\right)\right)$	
00	OUESTIMAN TOTAL	1 \ \-11	
	CHEEKWALL "B"	150	
CON	DITION 2 EQUATIONS	7 100 / 5 100 / 100 miles	
CA	CHEEKWALL "B"	150	
CB	CHEEKWALL "B"	$300\left(TAN\left(\frac{AB}{2}\right)\right)$	
СС	CHEEKWALL "B"	$150+\left(\frac{300}{TAN(A1)}\right)-300\left(TAN\left(\frac{AB}{2}\right)\right)$	
DA	WINGWALL "A" LENGTH	AC+BB	
DB	WINGWALL "B" LENGTH	AD+CB	
F4		C2+30	
EA	ABUTMENT LENGTH	C2+30 SIN(A1)	
EB	ABUTMENT LENGTH	EA+BA+CA	
EC	ABUTMENT LENGTH	EA +BA	
ED	ABUTMENT LENGTH	EA 2 + CA	
EE	ABUTMENT LENGTH	110 mm TAN(AT)	
		TAN(A1)	
FA	WINGWALL "A" HEIGHT	(20 - (5)1000 (2) (22 - (5)1000 (2) (20 - 22)1000 (2)	
FB	WINGWALL "A" HEIGHT	((22) - (15))1000 (2)	
FC	WINGWALL "A" HEIGHT	(② - ⑤)1000 (2) (② - ⑥)1000 (2) (② - ②)1000 (2)	
FD	WINGWALL REINFORCEMENT PROJECTION	DESIGNER (3)	
GA	WINGWALL "B" HEIGHT WINGWALL "B" HEIGHT WINGWALL "B" HEIGHT	DESIGNER (3) (30- (5))1000 (2)	
GB	WINGWALL "B" HEIGHT	(32 - (5))1000 (2)	
GC	WINGWALL "B" HEIGHT	(3) - (5)1000 (2) (3) - (32)1000 (2)	
GD	WINGWALL REINFORCEMENT PROJECTION	DESIGNER (3)	
HA	HEIGHT OF FINISH GRADE CHAMFER (ABUTMENT)	DESIGNER (3) ((16) - (15))1000 (2)	
нВ	REAR FACE REINFORCEMENT PROJECTION (ABUTMENT)	DESIGNER (3)	
IA	ABUTMENT FOOTING WIDTH	DESIGNER (3) DESIGNER (3)	<del></del>
18	ABUTMENT FOOTING WIDTH		99-43
IC	ABUTMENT FOOTING WIDTH	DESIGNER (3)	
JA	WINGWALL "A" FOOTING WIDTH		NAME OF THE OWNER OWNER OF THE OWNER O
JB	WINGWALL "A" FOOTING WIDTH		
JC I	WINDWALL "A" COOTING WIDTH	DESIGNER (3)	
	WINDWALL A FUUTING WIDTH	JA-JB	A STATE OF THE STA
KA (C)	WINDWALL B FOUTING WIDTH	DESIGNER (3)	
(B	WINGWALL "A" FOOTING WIDTH WINGWALL "B" FOOTING WIDTH WINGWALL "B" FOOTING WIDTH WINGWALL "B" FOOTING WIDTH	DESIGNER (3)	Water
KC LA	WINGWALL "B" FOOTING WIDTH ABUTMENT FOOTING LENGTH	KA-KB  EB-   IB	10/06 (00 - 02)
LB	ABUTMENT FOOTING LENGTH		
MA	WINGWALL "A" FOOTING LENGTH	$EB + \frac{IC}{TAN(AA)} - \frac{JC}{SIN(AA)} + \frac{IC}{TAN(AB)} - \frac{KC}{SIN(AB)}$ $IB \qquad JB$	
-		IB JB SIN(AA) TAN(AA)	
MB	WINGWALL "A" FOOTING LENGTH	DA+ IB JB TAN(AA)	a territoria de la composição de la comp
MC	WINGWALL "A" FOOTING LENGTH	$DA + \frac{JC}{TAN(AA)} - \frac{IC}{SIN(AA)}$	
	WINGWALL "B" FOOTING LENGTH	IB SIN(AB) TAN(AB)	
NA			
NA NB	WINGWALL "B" FOOTING LENGTH	DB+ \frac{\text{IB}}{\text{SIN(AB)}} - \frac{\text{KB}}{\text{TAN(AB)}}  DB+ \frac{\text{KC}}{\text{TAN(AB)}} - \frac{\text{C}}{\text{SIN(AB)}}	

- SEE APPROPRIATE SUPERSTRUCTURE DATA ASSEMBLY SHEETS (SHEETS 1 THRU 4 FOR 101M).
- (2) SEE SHEET 6 OF 101M FOR CONTROL ELEVATIONS.
- (3) DESIGN ABUTMENT AND RETAINING WALLS IN ACCORDANCE WITH ASSHTO LEFO SPECIFICATIONS. USE DATA ASSEMBLY AND CONSTRUCTION SHEETS TO CALCULARE THE NECESSARY DIMENSIONS AND REINFORCEMENT FOR THE ABUTMENT (WITHOUT BACKWALL), WINGWALLS, AND SPACED FOOTING.
- (4) SEE SHEET 6 OF 101M FOR WINGWALL EXAMPLE.



REVISIONS

SPREAD FOOTING ABUTMENT

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ENGINEER'S SEAL

SHEET NO: SERIES TITLE:

5 DATA ASSEMBLY SHEETS 10

SHEET\_\_\_of\_\_

POWERS & SCHRAM INC.

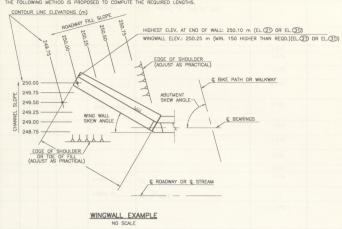
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			CONTROL ELEVATIONS		
CODE	DESCRIPTION		SOURCE	3.99 VI	VALUE (m)
10	ABUTMENT ELEVATION		USE 1 FOR ABUT. 1, OR 2 FOR ABUT. 2	(1)	
		BICYCLE/EMERGENCY VEHICLE SUPER.	$10 - (40 - D2 - A) \frac{m}{1*10^3 \text{ mm}}$	00 2	
1	ABUTMENT ELEVATION	PEDESTRIAN SUPERSTRUCTURE	(D-(D2-A)(m/1*103 mm)		
12	ABUTMENT ELEVATION		$1 + \frac{A2}{100} \left( \frac{EA}{2} (COS(A1)) \right) \left( \frac{m}{1*10^3 \text{ mm}} \right)$	ABUTMENT 1	
	(USE APPROPRIATE EQUATION DEPENDING ON ABUTMENT N	0.)	$1 - \frac{A2}{100} \left( \frac{EA}{2} (COS(A1)) \right) \left( \frac{m}{1*10^3 \text{ m/m}} \right)$	ABUTMENT 2	
13)	ABUTMENT ELEVATION		$1 - \frac{A2}{100} \left( \frac{EA}{2} (COS(A1)) \right) \left( \frac{m}{1*10^3 \text{ mm}} \right)$	ABUTMENT 1	
	(USE APPROPRIATE EQUATION DEPENDING ON ABUTMENT N	0.)	$1 + \frac{A2}{100} \left( \frac{EA}{2} (COS(A1)) \right) \left( \frac{m}{1*10^3 \text{ m/m}} \right)$	ABUTMENT 2	
14)	BOTTOM OF FOOTING ELEVAT	ION	DESIGNER		
15)	TOP OF FOOTING ELEVATION		$450 \left(\frac{m}{1*10^3 \text{ mm}}\right)$	*1	
16)	SCOUR DEPTH		DESIGNER		
20	WINGWALL "A" ELEVATION		$\bigcirc -\left(\frac{A2}{100}\left(\frac{EA}{2}(COS(A1))\right) + 150\right)\left(\frac{m}{1*10^3 \text{ mm}}\right)$	ABUTMENT 1	
	(USE APPROPRIATE EQUATION DEPENDING ON ABUTMENT N	0.)	$10 + \left(\frac{A2}{100}\left(\frac{EA}{2}(COS(A1))\right) + 150\right)\left(\frac{m}{1*10^3 mm}\right)$	ABUTMENT 2	
20	WINGWALL "A" ELEVATION		DESIGNER (SEE WINGWALL EXAMPLE)		
22	WINGWALL "A" ELEVATION		2) +150(m/1*103 mm)		
30	WINGWALL "B" ELEVATION		$10 + \left(\frac{A2}{100}\left(\frac{EA}{2}(\cos(A1))\right) + 150\right)\left(\frac{m}{1*10^3 \text{ mm}}\right)$	ABUTMENT 1	
	(USE APPROPRIATE EQUATION DEPENDING ON ABUTMENT N	0.)	$\bigcirc -\left(\frac{A2}{100}\left(\frac{EA}{2}(\cos(A1))\right) + 150\right)\left(\frac{m}{1*10^3 \text{mm}}\right)$	ABUTMENT 2	
3	WINGWALL "B" ELEVATION		DESIGNER (SEE WINGWALL EXAMPLE)	24-29/2/05	
32)	WINGWALL "B" ELEVATION		$(3) + 150 \left( \frac{m}{1*10^3 \text{ mm}} \right)$	Tor myster	

IN GENERAL, PROVIDE WINGWALLS OF SUFFICIENT LENGTH TO RETAIN THE ROADWAY EMBANKMENT TO THE REQUIRED EXTENT AND TO FURNISH PROTECTION AGAINST EROSION COMPUTE WINGWALL LENGTHS USING THE ACTUAL CONDITION AT THE SITE. THE FOLLOWING METHOD IS PROPOSED TO COMPUTE THE REQUIRED LENGTHS.



		QUANTITIES						
ITEM		QUANTITY FORMULA	UNIT	SUBTOTAL	TOTAL			
CLASS 3 EXCAVATION		DESIGNER	m <sup>3</sup>					
CHEEKWALL A	CLASS	$\left(BB+150+\frac{BA-150-BB}{2}\right)300\left(\frac{m^2}{1*10^8 \text{ mm}^2}\right)\left(20-12\right)$	m <sup>3</sup>					
CHEEKWALL B	AA CEMENT	$ \left( \text{CB+150+}  \frac{150 + \text{CB-CA}}{2} \right) 300 \left( \frac{\text{m}^2}{\text{1*10^6 mm}^2} \right) \left( \boxed{30}  -  \boxed{3} \right) $	m³					
CHEERWALL D	CONCRETE	$\left(2(CB)-150+\frac{CC+CB-150}{2}\right)300\left(\frac{m^2}{1*10^8\mathrm{mm}^2}\right)\left(30-33\right)$ CONDITION 2	m³					
ABUTMENT		$\left[0.45\left(\boxed{1}\right)-\boxed{\boxed{5}}+\left(\frac{1}{2}\right)\left(\frac{1}{10}\right)\left(\boxed{1}\right)-\boxed{\boxed{5}}\right)^{2}\left[\left(EB\right)\left(\frac{m}{1*10^{3}\mathrm{mm}}\right)$	m³					
WINGWALL A	CLASS	$\left[0.45\left(22 + \frac{10 - 15}{2} - 15\right) + \left(\frac{1}{2}\right)\left(\frac{1}{10}\right)\left(22 + \frac{10 - 15}{2} - 15\right)^{2}\right](AC)\left(\frac{m}{1 \cdot 10^{3} \text{mm}}\right)$	m³					
WINGWALL B	CEMENT	$\left[0.45\left(39 + \frac{30 - 39}{2} - 15\right) + \left(\frac{1}{2}\right)\left(\frac{1}{10}\right)\left(39 + \frac{30 - 39}{2} - 15\right)^{2}\right](AD)\left(\frac{m}{1*10^{3}mm}\right)$	m <sub>3</sub>					
FOOTING		$\left(\frac{1}{2}\right)$ (600) $\left((LA+LB)(IA)+(MB+MC)(JA)+(NB+NC)(KA)\right)\left(\frac{m^3}{1*10^3 \text{ mm}^3}\right)$	m <sup>3</sup>					
SELECTED BORROW EXCAVATION, STRUCTURE BACKFILL		DESIGNER	m <sup>3</sup>					
NO. 57 COARSE AGGREGATE		4 WEEPHOLES ( Q.4m <sup>3</sup> WEEPHOLE )	m <sup>3</sup>	1.6	1.6			
REINFORCEMENT BARS		DESIGNER - CALCULATE BAR MASS FROM SHEETS 7 & 8 OF 101M	kg					
REINFORCEMENT BARS, EPOXY COATED		DESIGNER - CALCULATE BAR WASS FROM SHEETS 7 & 8 OF 101M	kg					

FOOTNOTES FOR TABLES

(1) SEE APPROPRIATE SUPERSTRUCTURE DATA ASSEMBLY SHEETS (101M SHEETS 1 THRU 4).

_			-		
Mork	Description	By	Chk'd	App'd	Date
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SPREAD FOOTING ABUTMENT

SERIES NO: SHEET NO:

ENGINEER'S SEAL

DATA ASSEMBLY SHEETS 11

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					10/			CHEC								
MARK SIZ		CE LENGTH	SOURCE	NO.	SOURCE		A	В	C	Н	J	K	SOURCE	REMARKS	SOURCE	BAR MASS kg/m (4) TOTAL BAR MASS
1500 15		FROM	$\left[ (2 - 5) \left( \frac{1000}{m} \right) \right] - 50$		$\left\{ \frac{EB - 75}{450} + 0.99 \right\} + 1 \tag{1}$	STR.								VARIES BY	$((3-12)(\frac{1000}{m})\frac{1}{NO \text{ OF BARS}}$	1.570
		то	$\left[ (\sqrt{3} - \sqrt{5}) \left( \frac{1000}{m} \right) \right] - 50$													
01	DESIGN (2)		$\left[ (2 - 5) \left( \frac{1000}{m} \right) \right] - 50$		$\left\{ \frac{EB-150(TAN(AA))-150(TAN(AB))}{REQ. SPA. (DESIGNER)} +0.99 \right\} +1 $ (1)(2)	STR.								VARIES BY	$((3-2)(\frac{1000}{m})\frac{1}{NO OF BARS}$	
		то	$\left[ (\mathfrak{I} - \mathfrak{I} \mathfrak{B}) \left( \frac{1000}{m} \right) \right] - 50$		10-10 market 200 (198)											
1502 1			EB	1	$\left\{ \underbrace{(1) + (1) - (3) - (5)(\frac{1000}{m}) - 600}_{450} + 0.99 \right\} + 1 $ (2)(3)	STR.										1.570
1503 1		1 000	EB-150(TAN(AA))-150(TAN(AB))		SAME AS A1502	STR.										1.570
1504 1		500	√(③ - ①)²+(EB)²	1	-0.0841 (c) 1993	STR.										1.570
1505 1	1		$\sqrt{(3-1)^2+(EB-150(TAN(AA))-150(TAN(AB)))^2}$	1	CTANCACI - ISOCIANCION AU DOSAN (COMP.)	STR.						SE DAY				1.570
1006 10			$(8A-40)+490+\left(\frac{300}{SIN(A1)}-80\right)$	100	$\left\{ \underbrace{(20 - (2)(\frac{1000}{m}) - 100}_{250} + 0.99 \right\} + 1 \tag{1}$	STR.								BEND IN FIELD		0.785
1007 1			$(CA-40)+(CC-80)+420+\left(\frac{300}{SIN(A1)}-80\right)$	NES Por 19	$\left\{ \underbrace{(3) - (3)(\frac{1000}{m}) - 100}_{250} + 0.99 \right\} + 1 \tag{1}$	STR.								BEND IN FIELD		0.785
1508 1	5	200	(20 - (12) (1000 m) +450	144	USE 4 BARS FOR 90' SKEWS, AND 5 BARS ALL OTHER SKEWS	STR.		125	179							1.570
1509 1	5		(30) - (13) (1000 m) +450	4	40,000 +1	STR.										1.570
1510 1	5	950	H "A" WHIMEL SIE TAILE 1	1880	$\left\{ \begin{array}{c} NO. \text{ OF BARS FROM A} & D1+1 \\ \hline 2 \end{array} \right\} $ (1)	3	400	175	400			40	+ 250)			1.570
1511 1	5	300		16	WA (UKSI) OF THE PARTY OF THE P	STR.										1.570
1520 1		FROMTO	FB-50 FA-50		$\left\{ \frac{AC - 150}{450} + 0.99 \right\} + 1 \tag{1}$	STR.								VARIES BY	FC NO OF BARS	1.570
21	DESIGN (2)		FB-50 FA-50	K PA-	$ \left\{ \frac{AC-150}{REQ. SPA. (DESIGNER)} + 0.99 \right\} + 1  $ (1)(2)	STR.	100	195						VARIES BY	FC NO OF BARS	178
1522 1		1	AC-100	10-1	$\left\{ \frac{FB-150}{450} + 0.99 \right\} + 1$ SHOW ON DRAWINGS (1)	STR.										1.570
			DESIGNATION OF THE PARTY I		$2\left\{\frac{FB-150}{450}+0.99\right\}+1$ SHOW ON BAR SCHEDULE (1)								1 1			
1523 1		FROM	(FC-375)(AC-100) FC		$\left\{ \frac{FC-675}{450} + 0.99 \right\} + 1$ SHOW ON DRAWINGS (1)	STR.								VARIES BY	(LENGTH FROM) - (LENGTH TO	1.570
		то	300(AC-100) FC		2{FC-675 450 +0.99}+1 SHOW ON BAR SCHEDULE (TOTAL NO. OF BARS)										10 01 0110	
1524 1			√FC <sup>2</sup> +AC <sup>2</sup> −100	1 2	SHOW ON DRAWINGS SHOW ON BAR SCHEDULE (TOTAL NO. OF BARS)	STR.										1.570
1525 1		975		1	SHOW ON BAR SCHEDULE (TOTAL NO. OF BARS)  \[ \{ \begin{array}{c ccc} NO. OF BARS FROM W & 21+1 \\ 2 & 2 & 2 \end{array} \} \] \[ \left\{ \begin{array}{c ccc} NO. OF BARS FROM W & 21+1 \\ 2 & 2 & 2 & 2 \end{array} \} \] \[ \left\{ \begin{array}{c ccc} NO. OF BARS & 2 & 2 & 2 & 2 & 2 & 2 & 2 & 2 & 2 &	3	400	175	400			40				1.570
1526 1		300		8		STR.										1.570
1530 1		FROMTO	GB-50 GA-50		$\left\{ \frac{AD - 150}{450} + 0.99 \right\} + 1 \tag{1}$	STR.								VARIES BY	GC NO OF BARS	1.570
31	DESIGN (2)	NER FROM	GB-50 GA-50		$ \left\{ \frac{AD-150}{REQ. SPA. (DESIGNER)} + 0.99 \right\} + 1  $ (1)(2)	STR.								VARIES BY	GC NO OF BARS	
1532 1			AD-100		$\left\{\frac{GB-150}{450}+0.99\right\}+1$ SHOW ON DRAWINGS (1)	STR.										1.570
1533 1			(CC_375)(AD_100)		$2\left\{\frac{\text{GB}-150}{450} + 0.99\right\} + 1 \text{ SHOW ON BAR SCHEDULE} $ (1)	STR.									(LENOTH EDOM ) (LENOTH TO	) 1,570
1333 1		FROM	(GC-375)(AD-100) GC 300(AD-100)		$\left\{\frac{GC-675}{450}+0.99\right\}+1 \text{ SHOW ON DRAWINGS} \tag{1}$	JIK.								VARIES BY	(LENGTH FROM) - (LENGTH TO NO OF BARS	1.570
		ТО	300(AD-100) GC		$2\left\{\frac{GC-675}{450}+0.99\right\}+1\frac{SHOW ON BAR SCHEDULE}{(TOTAL NO. OF BARS)}$											

- (1) TAKE THE INTEGER VALUE OF THE QUANTITY WITHIN THE }
- (2) DESIGN ABUTMENT AND RETAINING WALLS IN ACCORDANCE WITH ASSHTO LEFD SPECIFICATIONS. USE DATA ASSEMBLY AND CONSTRUCTION SHEETS TO CALCULAR THE RECESSARY DIMENSIONS AND REINFORCEMENT FOR THE ABUTMENT (WITHOUT BACKWALL), WINGWALLS, AND SPREAD FOOTING.
- (3) TAKE THE ABSOLUTE VALUE OF THE QUANTITY WITHIN THE
- (4) USE TABLE 1 ON THIS SHEET TO COMPLETE BAR MASS QUANTITIES.
- (5) TOTAL BAR MASS = (BAR LENGTH OR AVERAGE BAR LENGTH)(TOTAL NO. OF BARS)(BAR MASS)



Mork Description By Chk'd App'd Date
REVISIONS

SPREAD FOOTING ABUTMENT \_

SERIES NO: SHEET NO: SERIES TO THE TOTAL SERIES SERIES TO THE SERIES SERIES TO THE SERIES SER

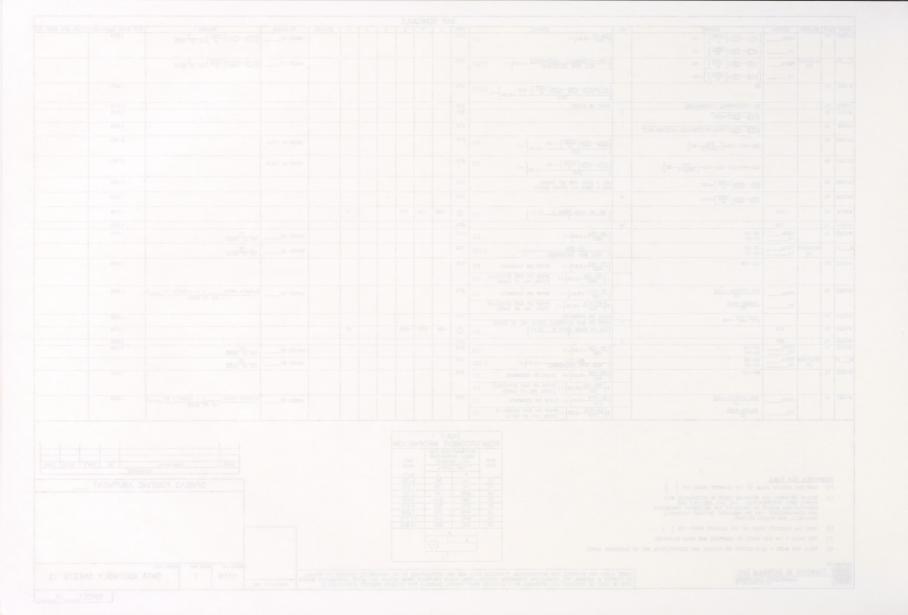
ENGINEER'S SEAL

DATA ASSEMBLY SHEETS 12

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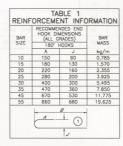
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							E	BAR S	CHED	ULE								
		SOURCE	LENGTH	SOURCE	NO.	SOURCE		I A	В	С	н	J	К	SOURCE	REMARKS	SOURCE	BAR MASS kg/m (4)	TOTAL BAR MASS
1534	15	-		$\sqrt{GC^2 + AD^2} - 100$		SHOW ON DRAWINGS SHOW ON BAR SCHEDULE (TOTAL NO. OF BARS)	STR.									DICTROL ELEVATIONS	1.570	
1535	15		975			$ \left\{ \begin{array}{ccc} NO. \text{ OF BARS FROM W} & 31+1 \\ 2 & & \end{array} \right\} $ (1	3	400	175	400		DESCRI	40		1	Source	1.570	(10)
1536	15		300		8		STR.								Land Contract	and a confidence state of	1.570	
00		DESIGNER (2)		IA-200		$\left\{ \frac{\text{LA}-150}{\text{REQ. SPA. (DESIGNER)}} +0.99 \right\} +1$ (1)(2)					-			The second second	er man	N m		
01		DESIGNER (2)		IA-200		$\left\{ \frac{\text{LA}-150}{\text{REQ. SPA. (DESIGNER)}} + 0.99 \right\} + 1$ (1)(2)	STR.		10	1 40%	OVERT -	agan		1000000		V a V		
1502	15			LA-200		$\left\{\frac{IA-200}{450}+0.99\right\}+1$ (1	STR.									Arrest Ar	1.570	
003	10		550			$\left(\left\{\frac{\text{IA}-200}{950}+0.99\right\}+1\right)\left(\left\{\frac{\text{LA}-150}{950}+0.99\right\}+1\right)$ (1	2	125	300	125	75					Security of the second	0.785	
1504	15		900			$\left\{ \frac{E8}{450} + 0.99 \right\} + 1$ (1	STR.			-1111	ENDAIG:	ON ASS	Market N	1903		Average Many	1.570	
06	5	DESIGNER (2)	Control 1	HB+350+A FOR "A" VARIABLE SEE TABLE 1		{ EB-150(TAN(AA))-150(TAN(AB)) +0.99}+1 (1)(2	0		119				-	SEE TABLE 1 (B = HB + 350)		A constraint on A		
20		DESIGNER (2)	CERTIFICATION OF THE PARTY OF T	JA-200		${MB-150 \over REQ. SPA. (DESIGNER)} +0.99}+1$ (1)(2	STR.		170		Distriction Co.	94 27			DEMONES			
21	1	DESIGNER (2)	преди	JA-200		${MB-150 \over REQ. SPA. (DESIGNER)} +0.99}+1$ (1)(2	STR.			100	OF FO	MASS S	EVATE		(D ++50)	(5) mm		
1522	15	DE CHARGES		MB-200		$\left\{ \frac{JA-200}{450} + 0.99 \right\} + 1 \tag{1}$	STR.		10	sos	IN DEF	TM .			DESCRIPE		1.570	
1023	10		700		R. III	$\left(\left\{\frac{JA-200}{950}+0.99\right\}+1\right)\left(\left\{\frac{MB-150}{950}+0.99\right\}+1\right)$ (1	2	125	300	125	75	X 8	DVASCOS		(A)-(A)	\$ (0.0(A1))=100 \ 1010 \ 1010 \ 1000 \	0.785	
524	15		900		501170	$\left\{\frac{AC-150}{450}+0.99\right\}+1$ (1	STR.			1 (US	AMPR	Del Alle	(1)X,10.7		Op - (-8)	\$ (cas(A1)) - 160 ( sapple 22)	1.570	
25	5	DESIGNER (2)		FD+350+A FOR "A" VARIABLE SEE TABLE 1		{ AC-150 REQ. SPA. (DESIGNER) +0.99}+1 (1)(2	1		10	CRE	TYPINELL	W 21		SEE TABLE 1 (B = FD + 350)	00+(Ws	\$ (036(41)) +150 (1710 (1710)	AN ASSESSOR 1	
30		DESIGNER (2)		KA-200		{ NB-150 REQ. SPA. (DESIGNER) +0.99}+1 (1)(2	STR.	1		10.8	70 PR	Mary San	COLEXT	100	0-(8)	A COMMENT OF STREET THE STREET	ASTRONO 21	
31	1	DESIGNER (2)		KA-200		\[ \begin{align*} \text{NB-150} \\ \text{REQ. SPA. (DESIGNER)} +0.99\Big\ +1 \end{align*} +1 \tag{1}(2)	) STR.											
1532	15			NB-200		$\left\{\frac{KA-200}{450}+0.99\right\}+1$ (1	) STR.										1.570	
1033	10		700			$\left(\frac{KA-200}{950}+0.99\right)+1\left(\frac{NB-150}{950}+0.99\right)+1$	2	125	300	125	75						0.785	
1534	15		900			$\left\{ \frac{AD-150}{450} + 0.99 \right\} + 1 \tag{1}$	) STR.										1.570	
35	5	DESIGNER (2)		GD+350+A FOR "A" VARIABLE SEE TABLE 1		{ AD-150 REQ. SPA. (DESIGNER) +0.99}+1 (1)(2	0							SEE TABLE 1 (B = GD + 350)				

- (1) TAKE THE INTEGER VALUE OF THE QUANTITY WITHIN THE {
- (2) DESIGN ABUTMENT AND RETAINING WALLS IN ACCORDANCE WITH ASSITO LEFD SPECIFICATIONS. USE DATA ASSEMBLY AND CONSTRUCTION SHEETS TO CALCULAR THE RECESSARY DIMENSIONS AND REINFORCEMENT FOR THE ABUTMENT (WITHOUT BACKWALL), WINGWALLS, AND SPREAD FOOTING.
- (3) TAKE THE ABSOLUTE VALUE OF THE QUANTITY WITHIN THE
- (4) USE TABLE 1 ON THIS SHEET TO COMPLETE BAR MASS QUANTITIES.
- (5) TOTAL BAR MASS = (BAR LENGTH OR AVERAGE BAR LENGTH)(TOTAL NO. OF BARS)(BAR MASS)



SPREAD FOOTING ABUTMENT \_\_\_\_\_

SPREAD FOOTING ABUTMENT \_\_\_\_

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		CONTROL DIMENSIONS		
CODE	DESCRIPTION	SOURCE		VALUE
A1	SKEW ANGLE	A1	(1) (1) (1)	DEG
A2	% GRADE (LOOKING STATIONS AHEAD)	A2	(1)	
C1	CURB TO CURB ROADWAY WIDTH (NORMAL)	C1	(1)	197
C2	DECK WIDTH OUT TO OUT	C2	(1)	
02	DECK THICKNESS	02	(1)	
Α	BEAM DEPTH	USE L4 FOR GLULAM BEAM OR ZERO (0) FOR LONG. PANEL	(1)	
В	BEARING THICKNESS	USE TWELVE (12) FOR GLULAM BEAM OR TWENTY (20) FOR LONG. PANEL	(1)	
AA	CHEEKWALL LENGTH	300+300 TAN(A1)	(4)	
EA	ABUTMENT LENGTH	C2+30 SIN(A1)		
EB	ABUTMENT LENGTH	EA+BA+CA		99 ( )
EC	ABUTMENT LENGTH	EA +BA		
ED	ABUTMENT LENGTH	EA +CA		
EA	ABUTMENT LENGTH	110 mm TAN(A1)		
FA	WINGWALL "A" HEIGHT	(20 - (5)1000	(2)	
GA	WINGWALL "B" HEIGHT	(30- (5)1000	(2)	
HA	HEIGHT OF FINISH GRADE CHAMFER (ABUTMENT)	(16 - (15)1000	(2)	
НВ	REAR FACE REINFORCEMENT PROJECTION (ABUTMENT)	DESIGNER	(3)	17
IA	ABUTMENT FOOTING WIDTH	DESIGNER	(3)	
IB	ABUTMENT FOOTING WIDTH	DESIGNER	(3)	
IC	ABUTMENT FOOTING WIDTH	IA-IB		

			CONTROL ELEVATIONS	1.0.3			
CODE DESCRIPTION			SOURCE		VALUE (m)		
10	ABUTMENT ELEVATION		USE 1 FOR ABUT. 1, OR 2 FOR ABUT. 2	(1)			
		ICYCLE/EMERGENCY VEHICLE SUPER.	$(0) - (40 - D2 - A) \frac{m}{(1*10^3 \text{ mm})}$				
1	ABUTMENT ELEVATION	PEDESTRIAN SUPERSTRUCTURE	$\boxed{\bigcirc} - \left(D2 + A + B\right) \left(\frac{m}{1 \cdot 10^3 \text{ mm}}\right)$	1570			
12	ABUTMENT ELEVATION		$1 + \frac{A2}{100} \left( \frac{EA}{2} (COS(A1)) \right) \left( \frac{m}{1*10^3 \text{ mm}} \right)$ ABUTM	ENT 1			
	(USE APPROPRIATE EQUATION DEPENDING ON ABUTMENT NO.)		$1 - \frac{A2}{100} (COS(A1)) \frac{m}{1*10^3 mm}$ ABUTM	ENT 2			
13)	13 ABUTMENT ELEVATION		$\boxed{1} - \frac{A2}{100} \left( \frac{EA}{2} (COS(A1)) \right) \left( \frac{m}{1*10^3 \text{mm}} \right)$ ABUTM	ENT 1			
	(USE APPROPRIATE EQUATION DEPENDING ON ABUTMENT NO.)		$\boxed{1} + \frac{A2}{100} \left( \frac{EA}{2} (COS(A1)) \right) \left( \frac{m}{1 \cdot 10^3 \text{ mm}} \right)$ ABUTM	ENT 2			
14)	BOTTOM OF FOOTING ELEVATION		DESIGNER				
15)	TOP OF FOOTING ELEVATION		$14 + 450 \left( \frac{\text{m}}{1*10^3 \text{mm}} \right)$				
16	SCOUR DEPTH		DESIGNER				
20	CHEEKWALL "A" ELEVATION		$\boxed{\bigcirc -\left(\frac{A2}{100}\left(\frac{EA}{2}(\cos(A1))\right) + 150\right)\left(\frac{m}{1*10^3 mm}\right)}$ ABUTM	ENT 1			
	(USE APPROPRIATE EQUATION DEPENDING ON ABUTMENT NO.)		$100 + \left(\frac{A2}{100}\left(\frac{EA}{2}(COS(A1))\right) + 150\right)\left(\frac{m}{1*10^3 mm}\right)$ ABUTM	ENT 2			
30	CHEEKWALL "B" ELEVATION		$\boxed{10} + \left(\frac{A2}{100} \left(\frac{EA}{2} (COS(A1))\right) + 150\right) \left(\frac{m}{1*10^3 mm}\right) $ ABUTM	ENT 1			
	(USE APPROPRIATE EQUATION DEPENDING ON ABUTMENT NO.)		$\boxed{\bigcirc -\left(\frac{A2}{100}\left(\frac{EA}{2}(\cos(A1))\right) + 150\right)\left(\frac{m}{1*10^3 \text{ mm}}\right)}$ ABUTM	ENT 2			

		QUANTITIES				
ITEM		QUANTITY FORMULA	UNIT	SUBTOTAL	TOTAL	
CLASS 3 EXCAVATION		DESIGNER		m³		
CHEEKWALL A	CLASS	$900+1/2\left(\frac{300}{TAN(A1)}\right)300\left(\frac{m^2}{1*10^6 mm^2}\right)\left(20-12\right)$		m3		
CHFEKWALL B	AA CEMENT	$900+1/2(\frac{300}{TAN(A1)})300(\frac{m^2}{1*10^8 mm^2})(30 - (13))$	CONDITION 1	m <sup>3</sup>		
GREENWALL B	CONCRETE	$\left(2(CB)-150+\frac{CC+CB-150}{2}\right)300\left(\frac{m^2}{1*10^8 \text{ mm}^2}\right)\left(30-3\right)$	CONDITION 2	m3		
ABUTMENT	CLASS	$\left[0.45\left(11\right) - 15\right) + \left(\frac{1}{2}\right)\left(\frac{1}{10}\right)\left(11\right) - 15\right)^{2}\left[(EB)\left(\frac{m}{1*10^{3} \text{ mm}}\right)\right]$		m3		
FOOTING	CEMENT CONCRETE	$(450(EA)(IA))(\frac{m^3}{1*10^9 \text{ mm}^3})$		m <sup>3</sup>		
SELECTED BORROW EXCAVATION, STRUCTURE BACKFILL		DESIGNER		m <sup>3</sup>		
NO. 57 COARSE AGGREGATE	GGREGATE 2 WEEPHOLES $\left(\frac{0.4\text{m}^3}{\text{WEEPHOLE}}\right)$		m <sup>3</sup>	0.8	0.8	
REINFORCEMENT BARS		DESIGNER - CALCULATE BAR MASS FROM SHEETS 11 & 12 OF 101M		kg		
REINFORCEMENT BARS, EPOXY COATED		DESIGNER - CALCULATE BAR MASS FROM SHEETS 11 & 12 OF 101M	(20,000)	kg		

- (1) SEE APPROPRIATE SUPERSTRUCTURE DATA ASSEMBLY SHEETS (SHEETS 1 THRU 4 FOR 101M).
- (2) SEE THIS SHEET FOR CONTROL ELEVATIONS.
- (3) DESIGN ABUTMENT AND RETAINING WALLS IN ACCORDANCE WITH AASHTO LEFD SPECIFICATIONS. USE DATA ASSEMBLY AND CONSTRUCTION SHEETS TO CALCULARE THE NECESSARY DIMENSIONS AND REINFORCEMENT FOR THE ABUTMENT (WITHOUT BACKWALL), WINGWALLS, AND SPREAD FOOTING.
- (4) SEE SHEET 6 OF 101M FOR WINGWALL EXAMPLE.

Mark	Description	By	Chk'd	App'd	Date
	REVISIO		1 0	1400	- 500

SPREAD FOOTING ABUTMENT \_\_\_\_ W/O WINGWALLS

ES NO: SHEET NO: SERIES TITLE

SERIES NO: SHEET NO: SERIES TO

DATA ASSEMBLY SHEETS

POWERS & SCHRAM INC.

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								BAR	SCHE	DULE								
MARK	SIZE S	SOURCE	LENGTH	SOURCE	NO.	SOURCE	TYF		В	C	Н	J	K	SOURCE	REMARKS	SOURCE	BAR MASS kg/m (4)	TOTAL BAR MASS (
A1500	15	And the	FROM	$\left[ (2 - 15) \left( \frac{1000}{m} \right)^{-1} \right] -50$		$\left\{\frac{EB-150}{450}+0.99\right\}+1$	1) STE	2.							VARIES BY4_	$((3-12)(\frac{1000}{m})\frac{1}{NO OF BARS}$	1.570	19622
	3	W. 112	TO	$\left[ (\boxed{3} - \boxed{5}) \left( \frac{1000}{m} \right) \right] -50$		[1]					I				CONTROL S	ATIONS AND ELEVATIONS		-
01	D	ESIGNER (2)		$[(2-5)(\frac{1000}{m})]-50$		$\left\{ \frac{EB-150}{REQ. SPA. (DESIGNER)} + 0.99 \right\} + 1$ (1)	2) STI	₹.			10			DESCRIPTION	VARIES BY 2	$((3-2)(\frac{1000}{m})\frac{1}{NO \ OF \ BARS}$		135 (m)
			то	$\left[ (\boxed{3} - \boxed{5}) \left( \frac{1000}{m} \right) \right] -50$			-		-			1 100		DEWINN	USE (1) FOR	por 1, sin (1) ron since g	(9)	
A1502	15	0 00	Case is	EB-100		$\left\{ \frac{(1) + (1) - (3) - (5)(\frac{1000}{m}) - 600}{450} + 0.99 \right\} + 1 $ (2)	3) STI	₹.				0 140	heest	E.C. OTTON	GB-(40-918	100-4-0-0-12(mi69mm)	1.570	
A1503	15	41.76	SKEW WILL	EB-100		SAME AS A1502	STI	2.		+			115535		199	Maria Maria Sami	1.570	
A1504	15			√(③ - ①)²+(EB)²	2		STI	₹.				188		DAMATE COUNTRY	(s)		1.570	
A1006	10			$(AA-40)+640+\left(\frac{300}{SIN(A1)}-80\right)$	(m (7))	$\left\{ \frac{(20 - (2)(\frac{1000}{m}) - 100}{250} + 0.99 \right\} + 1$	1) STI	₹.				1 10	DALEST C. JONES	DENIES CENTRE	BEND IN FIELD		0.785	
A1007	10		CONNUN DIS	$(AA-40)+640+\left(\frac{300}{SIN(A1)}-80\right)$	1900 1900 (1900)	$\left\{ \frac{(30 - (3))(\frac{1000}{m}) - 100}{250} + 0.99 \right\} + 1$	1) STI	₹.					1200		BEND IN FIELD	of A. Shares Y for South Ma.)	0.785	
A1508	15		grenten i	(20 - (2) (1000 m)+450	1393		STI	₹.			1	0 100		ET ELEVATION	10-181	(-)-Quan-N	1.570	
A1509	15	ME TO		$(30 - (3)(\frac{1000}{m}) + 450$	4		ST	₹.				186	Green Entors	CH MRUNEN ROJ	00 Kill (2	2	1,570	
A1510	15		950	180 THE RESERVE TO SERVE T		{ NO. OF BARS FROM A 01+1 }	1) (3	) 4	00 175	400	1 3		40	s* ELEochew	OTSKOUTH (SSE	MANAGER (VARIOUS)	1.570	
A1511	15		300	1300	16		ST					7 199		A TALLYANDA	1900 - 190,000		1.570	
00	C	ESIGNER (2)		IA-200	- 19000 - 19000	EB-150 REQ. SPA. (DESIGNER) +0.99 $+1$ (1)	2) ST	₹.			1 13		1000	LOLD LOAD	DESCRIEN			
01	C	ESIGNER (2)	EDWART LIN	IA-200	25 (to ( (3E) )	${EB-150 \over REQ. SPA. (DESIGNER)} +0.99}+1$ (1)	2) ST	₹.				1 100	and the same		V-9 (400 (41)	MANY THE AMERICA		
F1502	15	40 X	our to our	EB-200	0-1-160	4	1) ST	₹.					10000	ON ASSEMBLE NO.)	100 100 10	MANAGEMENT AND THE	1.570	
F1003	10		550	PLS DWORSTON DWOLS XE-150 (1907)	) (g 24g)	$\left(\left(\frac{1A-200}{950}+0.99\right)+1\right)\left(\left(\frac{EB-150}{950}+0.99\right)+1\right)$	1) ②	) 12	25 300	125	75			P. D.C. STORY			0.785	
F1504	15	5007 623	875	ARAT. 300 + 15.0(TAN(AA))	(580 1035)		1) ST	₹.						I LIVERS	1001000	Proft)	1.570	
F05	C	ESIGNER (2)	(Ties	HB+350+A FOR "A" VARIABLE SEE TABLE 1	( 30	{ EB-150(TAN(AA))-150(TAN(AB)) +0.99}+1 (1)	2) (1							SEE TABLE 1 (B = HB + 350)				

- (1) TAKE THE INTEGER VALUE OF THE QUANTITY WITHIN THE
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- (3) TAKE THE ABSOLUTE VALUE OF THE QUANTITY WITHIN THE
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- (5) TOTAL BAR MASS = (BAR LENGTH OR AVERAGE BAR LENGTH)(TOTAL NO. OF BARS)(BAR MASS)



SPREAD FOOTING ABUTMENT \_\_\_\_ W/O WINGWALLS

SPREAD FOOTING ABUTMENT \_\_\_\_ W/O WINGWALLS

SERES NO: SPEET NO: SURES ITILE:

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DE	DESCRIPTION		CONTROL DIMENSIONS SOURCE	VALUE
	ANGLE		A1 (1)	DE
2 % GRA	ADE (LOOKING STATIONS AHEAD)		A2 (1)	
1 CURB	TO CURB ROADWAY WIDTH (NORMAL)		C1 (1)	
	WIDTH OUT TO OUT		C2 (1)	
	OR LONG. PANEL THICKNESS		USE E1 FOR GLULAM & STEEL BEAM OR E2 FOR LONG. PANEL (1)	
, ocon	or coro. Trace Triorites		E2 FOR LONG. PANEL	
BEAM	DEPTH		USE L4 FOR GLULAM BEAM, L5 FOR STEEL BEAM OR ZERO (0) FOR LONG, PANEL (1)	
1 1000000			ZERO (0) FOR LONG. PANEL	
BEARIN	NG PAD THICKNESS		USE N3 OR P3 FOR GLULAM AND STEEL BEAM OR TWENTY (20) FOR LONG. PANEL (1)	
			IWENTY (20) FOR LONG, PANEL	
A WINGW	WALL "A" SKEW ANGLE WALL "B" SKEW ANGLE		DESIGNER (15'00'00" MIN., 45'00'00" MAX.) (2) DESIGNER (15'00'00" MIN., 45'00'00" MAX.) (2)	DE
B WINGW.	WALL "B" SKEW ANGLE WALL "A" LENGTH		DESIGNER (15'00'00" MIN., 45'00'00" MAX.) (2)	DE
D WINGW	WALL "B" LENGTH		DESIGNER (2) DESIGNER (2)	
A WINGW	WALL "A" CORNER DIMENSIONS		$300 + \left(\frac{375}{TAN(A1)}\right) + 375\left(TAN\left(\frac{AA}{2}\right)\right)$	
B WINGW	WALL "A" CORNER DIMENSIONS		$375\left(TAN\left(\frac{AA}{2}\right)\right) + \left(\frac{76}{TAN(AA)}\right) + 100(COS(AA))$	
A WINGW	WALL "B" CORNER DIMENSIONS		$300 - \left(\frac{375}{TAN(A1)}\right) + 375\left(TAN\left(\frac{AB}{2}\right)\right)$	
CA > 15	50 USE CONDITION 1 EQUATIONS, OTHER	WISE USE	CONDITION 2 FOLIATIONS	
ONDITION 1	1 EQUATIONS			
A WINGW	WALL "B" CORNER DIMENSIONS		AS CALCULATED ABOVE	
	WALL "B" CORNER DIMENSIONS		$375\left(TAN\left(\frac{AB}{2}\right)\right) + \left(\frac{76}{TAN(AB)}\right) + 100(COS(AB))$	
	WALL "B" CORNER DIMENSIONS		300	
	2 EQUATIONS			
A WINGW	WALL "B" CORNER DIMENSIONS		300	
B WINGW	WALL "B" CORNER DIMENSIONS		$375\left(TAN\left(\frac{AB}{2}\right)\right)+\left(\frac{76}{TAN(AB)}\right)+100(COS(AB))$	
C WINGW	WALL "B" CORNER DIMENSIONS		$300 + \left(\frac{450}{TAN(A1)}\right) - 375\left(TAN\left(\frac{AB}{2}\right)\right)$	
-				
A WINGW	WALL "A" OUT TO OUT PILE DIMENSION		$AC-150 + \left(\frac{150}{TAN(AA)}\right) - \left(\frac{254}{TAN(AA)}\right)$	
B WINGW	WALL "B" OUT TO OUT PILE DIMENSION	TIMBER	$AD-150 + \left(\frac{150}{TAN(AB)}\right) - \left(\frac{254}{TAN(AB)}\right)$	
-		PILE	V - V - M - V - M	
A ABUTM	MENT LENGTH	ABUT.	$300+150(TAN(AA))-\left(\frac{150}{SIN(AA)COS(AA)}\right)+\left(\frac{254}{TAN(AA)}\right)$	
D ADUTA	JENT LENGTH		00.450(744/40)) / 150 )./ 254 )	
B ABUTM	MENT LENGTH		$CC+150(TAN(AB))-\left(\frac{150}{SIN(AB)COS(AB)}\right)+\left(\frac{254}{TAN(AB)}\right)$	
A WINGW	WALL "A" OUT TO OUT PILE DIMENSION	CONTRACTOR OF	$AC-150 + \left(\frac{150}{SIN(AA)}\right) - \left(\frac{DC}{TAN(AA)}\right) - \left(\frac{199}{TAN(AA)}\right)$	
A WINGH	WALE A GOT TO GOT FILE DIMENSION		AC-130 T(SIN(AA)) TAN(AA))	
B WINGW	WALL "B" OUT TO OUT PILE DIMENSION		$AD-150 + \left(\frac{150}{SIN(AB)}\right) - \left(\frac{DD}{TAN(AB)}\right) - \left(\frac{199}{TAN(AB)}\right)$	
			(SIN(AB)) (TAN(AB)) (TAN(AB))	
C WINGW	WALL "A" PILE OFFSET	STEEL	178(COS(46.1-AA))-123	
-		PILE		
D WINGW	WALL "B" PILE OFFSET	ABUT.	178(COS(46.1-AB))-123	
-			4 450 > 4 50 > 4 400 > 4 47 > 4 450 >	
A ABUTM	MENT LENGTH		$300+150(TAN(AA))-\left(\frac{150}{SIN(AA)COS(AA)}\right)+\left(\frac{DC}{SIN(AA)}\right)+\left(\frac{199}{SIN(AA)}\right)+\left(\frac{K3}{SIN(A1)}\right)+\left(\frac{150}{TAN(A1)}\right)$	
-				
B ABUTM	MENT LENGTH		$ \left( \frac{150}{\text{SIN(AB)}} \right) + \left( \frac{150}{\text{SIN(AB)}} \right) + \left( \frac{199}{\text{SIN(AB)}} \right) + \left( \frac{\text{K3}}{\text{SIN(A1)}} \right) - \left( \frac{150}{\text{TAN(A1)}} \right) $	
_				
C ABUTM	MENT LENGTH		$\left(\frac{C2}{(2)SIN(A1)}\right)$ +EA	
D ARUTM	VENT LENGTH		117 177	
ABUTM	MENT LENGTH		$\left(\frac{C2}{(2)SIN(A1)}\right)$ +EB	
E TIMBER	R BEARING SILL LENGTH		(	
		7 74		
F NUMBE	BER OF PILES (ABUTMENT)		DESIGNER (3)	
G PILE S	SPACING (ABUTMENT)	131	EF EC+ED	
A NUMBE	BER OF PILES (WINGWALL "A")		DESIGNER (3)	
B PILE S	SPACING (WINGWALL "A")		(DA FA)	
B PILE S	SPACING (WINGWALL "B")			
A CHANG	OF IN WINCHALL "A" HEIGHT			
B CHANG	CE IN WINGWALL A HEIGHT		(30) - (32)1000	
WINGW	WALL "A" SLOPE		10(-XC)	
	107 0.005			
MINGM	WALL B SLOPE		10(AD)	
	WALL TAP COOKING LEMOTH		$(10^2 + 14^2)^{0.5}$	
A WINGW	WALL A COPING LENGTH		10 (AC+150)	
D WILLIAM	MALL "D" CODING LENCTH		(10 <sup>2</sup> +18 <sup>2</sup> <sup>20.5</sup> )/40.450	
			10 (AU+150)	
A EXPOS	SED ABUTMENT HEIGHT		((1)-(4)1000)-350	
			((10 <sup>2</sup> +IA <sup>2</sup> ) <sup>0.5</sup> \255)	
- HIII-OW	TONE LENGTH	PILE	10 /2007	
		ABUT.	$(10^2 + 18^2)^{0.5}$ (256)	
B PILE S A CHANG B CHANG WINGW B WINGW A WINGW B WINGW A EXPOS	GE IN WINGWALL "A" HEIGHT GE IN WINGWALL "B" HEIGHT WALL "A" SLOPE WALL "B" SLOPE WALL "A" COPING LENGTH WALL "B" COPING LENGTH	STEEL	DESIGNER (3) (9B) (3D - 22)11000 (3D - 22)11000 10 (-14A	

	(			
CODE	DESCRIPTION	SOURCE		VALUE (m)
10	ABUTMENT ELEVATION	USE 1 FOR ABUT. 1, OR 2 FOR ABUT. 2	(1)	
1	ABUTMENT ELEVATION	$10 - \left(40 - \frac{C1}{2}(0.02) - A - B - C - 12\right)\left(\frac{m}{1*10^3 \text{ mm}}\right)$		
12	ABUTMENT ELEVATION	$1 + \frac{A2}{100} \left( \frac{C2}{2(TAN(A1))} \right) \left( \frac{m}{1*10^3 mm} \right)$	ABUTMENT 1	
	(USE APPROPRIATE EQUATION DEPENDING ON ABUTMENT NO.)	$1 - \frac{A2}{100} \left( \frac{C2}{2(TAN(A1))} \right) \left( \frac{m}{1 \cdot 10^3 mm} \right)$	ABUTMENT 2	
13)	ABUTMENT ELEVATION	$10 - \frac{A2}{100} \left( \frac{C2}{2(TAN(A1))} \right) \left( \frac{m}{1*10^3 \text{mm}} \right)$	ABUTMENT 1	
	(USE APPROPRIATE EQUATION DEPENDING ON ABUTMENT NO.)	$1 + \frac{A2}{100} \left( \frac{C2}{2(TAN(A1))} \right) \left( \frac{m}{1*10^3 mm} \right)$	ABUTMENT 2	
14)	SCOUR DEPTH	DESIGNER (SEE DM-4, PART A, CHAPTER 7 FOR SCOUR REQ.)		
(15)	ABUTMENT PILE TIP ELEVATION	DESIGNER		
20	WINGWALL "A" ELEVATION	$\boxed{\bigcirc -\left(\frac{A2}{100}\left(\frac{C2}{2(TAN(A1))}\right) - \frac{C1}{2}(0.02) - A\right)\left(\frac{m}{1*10^3 mm}\right)}$	ABUTMENT 1	
	(USE APPROPRIATE EQUATION DEPENDING ON ABUTMENT NO.)	$\boxed{ \bigcirc + \left(\frac{A2}{100} \left(\frac{C2}{2(TAN(A1))}\right) - \frac{C1}{2}(0.02) - A\right) \left(\frac{m}{1*10^3 mm}\right) }$	ABUTMENT 2	
20	WINGWALL "A" ELEVATION	DESIGNER (SEE WINGWALL EXAMPLE)		
22	WINGWALL "A" ELEVATION	2) +150(m/(1*10 <sup>3</sup> mm)		
(23)	WINGWALL "A" PILE TIP ELEVATION	DESIGNER		
30	WINGWALL "B" ELEVATION	$ (10) + \left(\frac{A2}{100} \left(\frac{C2}{2(TAN(A1))}\right) - \frac{C1}{2}(0.02) - A\right) \left(\frac{m}{1*10^3 mm}\right) $	ABUTMENT 1	
	(USE APPROPRIATE EQUATION DEPENDING ON ABUTMENT NO.)	$\boxed{\bigcirc -\left(\frac{A2}{100}\left(\frac{C2}{2(TAN(A1))}\right) - \frac{C1}{2}(0.02) - A\right)\left(\frac{m}{1*10^3 mm}\right)}$	ABUTMENT 2	
31)	WINGWALL "B" ELEVATION	DESIGNER (SEE WINGWALL EXAMPLE)		
32	WINGWALL "B" ELEVATION	②D+150(m/1*103 mm)		
(33)	WINGWALL "B" PILE TIP ELEVATION	DESIGNER		

- (1) SEE APPROPRIATE SUPERSTRUCTURE DATA ASSEMBLY SHEETS (101M SHEETS 1 THRU 4).
- (2) SEE SHEET 12 OF 101M FOR WINGWALL EXAMPLE.
- (3) DESIGN PILES IN ACCORDANCE WITH 100M SHEET 2.



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SERIES NO:
101M
ENGINEER'S SEAL

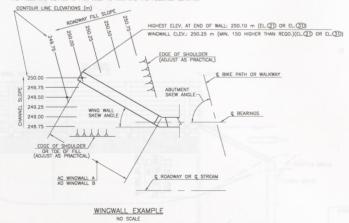
HEET NO: SERIES TITLE:

11 DA

DATA ASSEMBLY SHEETS

		QUANTITIES			
ITEM		QUANTITY FORMULA	UNIT	SUBTOTAL	TOTAL
CLASS 3 EXCAVATION		DESIGNER	m <sup>3</sup>		
TIMBER BEARING SILL		$(EE(300)(350))(\frac{m^3}{1*10^8 \text{ mm}^3})$	m <sup>3</sup>		
ABUTMENT		$(EF)(1) - 350 - (5)(\frac{m}{1*10^3 mm})$	m		
WINGWALL A	PILES	$(FA-1)\left(\frac{2}{3}(HA)+22-23\right)\left(\frac{m}{1*10^3 \text{ mm}}\right)$	m		
WINGWALL B	7-7-	$(GA-1)\left(\frac{2}{3}(HB)+32-33\right)\left(\frac{m}{1*10^3 mm}\right)$	m		
ABUTMENT	1/2	$EE(76)(KA+915)\left(\frac{m^3}{1*10^9 \text{mm}^3}\right)$	m <sub>2</sub>		
WINGWALL A	TIMBER LAGGING	$(DA+450)(75)(\frac{2}{3}(HA)+22)-(14)+915)(\frac{m^3}{1*10^9 \text{ mm}^3})$	m <sup>3</sup>		
WINGWALL B	1811	$(DB+450)(76)\left(\frac{2}{3}(HB)+32-14+915\right)\left(\frac{m^3}{1*10^9 \text{ mm}^3}\right)$	m <sup>3</sup>		
WINGWALL A COPING		$130(375)\sqrt{JA + \frac{1}{2} \left(BA + BB + 300 + \frac{76}{TAN(AA)} + 100(COS(AA))\right) \left(\frac{m^3}{1*10^9 \text{ m/m}^3}\right)}$	m <sup>3</sup>		
WINGWALL B COPING		$130(375) \sqrt{JB + \frac{1}{2} \left(CA + CB + CC + \frac{76}{TAN(AB)} + 100(COS(AB)) \left(\frac{m^3}{1*10^9 \text{ mm}^3}\right)}$	m <sup>3</sup>		
SELECTED BORROW EXCAVATION, STRUCTURE	BACKFILL	DESIGNER	m <sup>3</sup>		
PILE TIP REINFORCEMENT		EF+FA+GA-2	EA		

IN GENERAL, PROVIDE WINGWALLS OF SUFFICIENT LENGTH TO RETAIN THE ROADWAY EMBANKWENT TO THE REQUIRED EXTENT AND TO FURNISH PROTECTION AGAINST EROSION COMPUTE WINGWALL LENGTHS USING THE ACTUAL CONDITION AT THE SITE. THE FOLLOWING METHOD IS PROPOSED TO COMPUTE THE REQUIRED LENGTHS.



REVISIONS PILE SUPPORTED TIMBER SILL

SHEET NO:

101M

DATA ASSEMBLY SHEETS

SHEET\_\_\_of\_

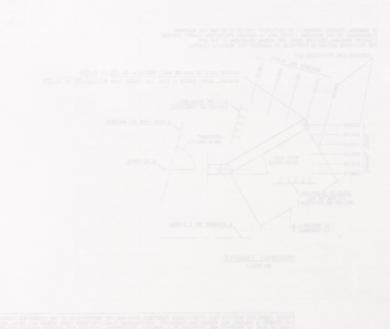
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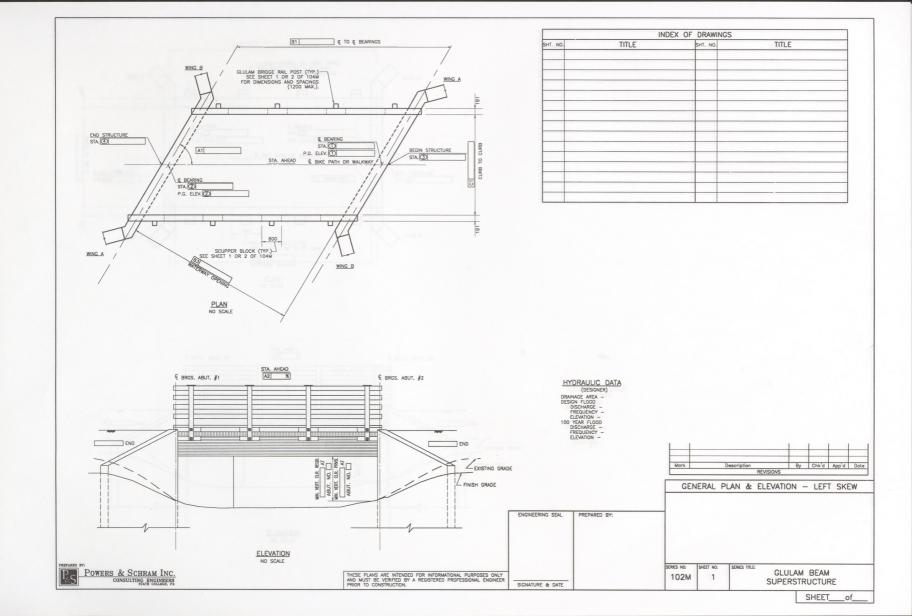
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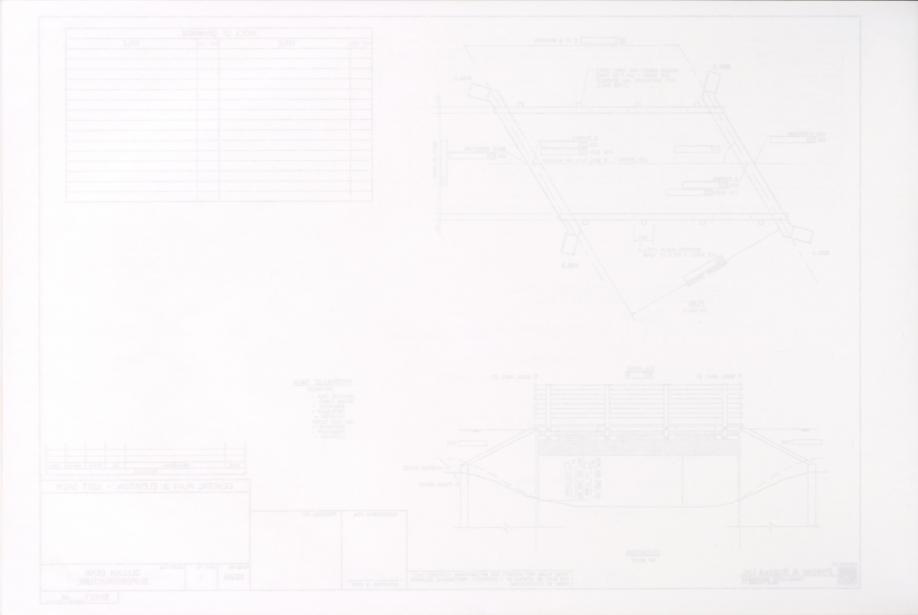
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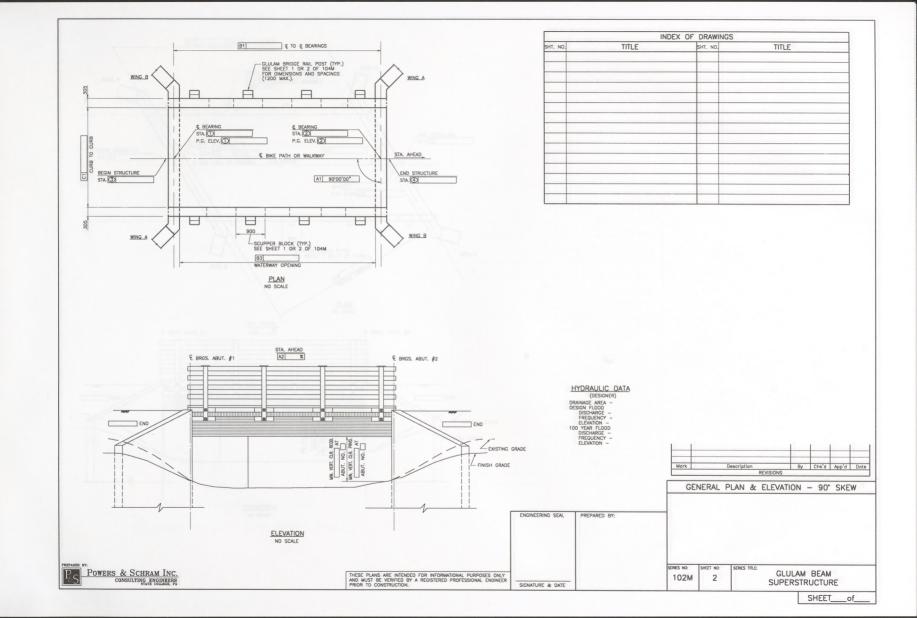
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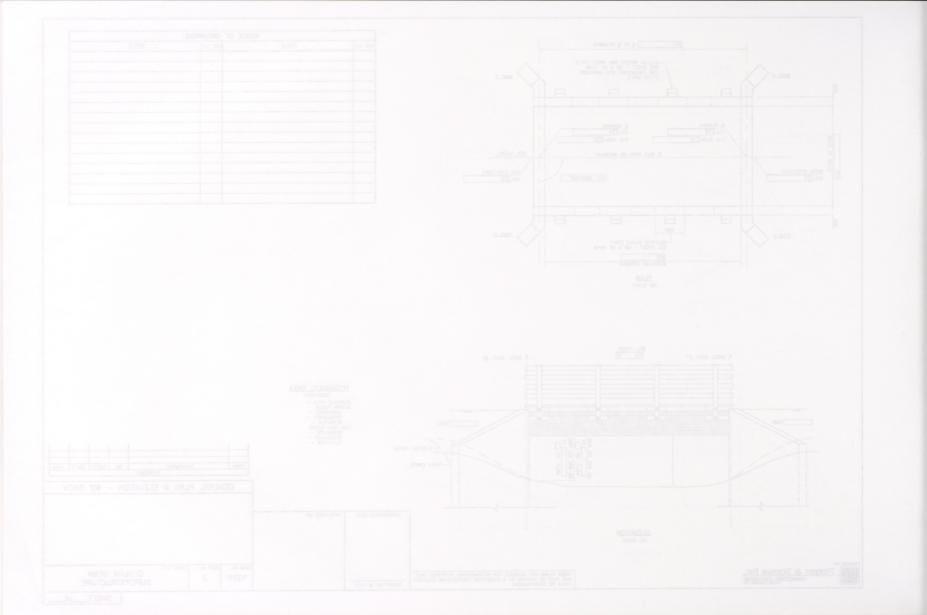
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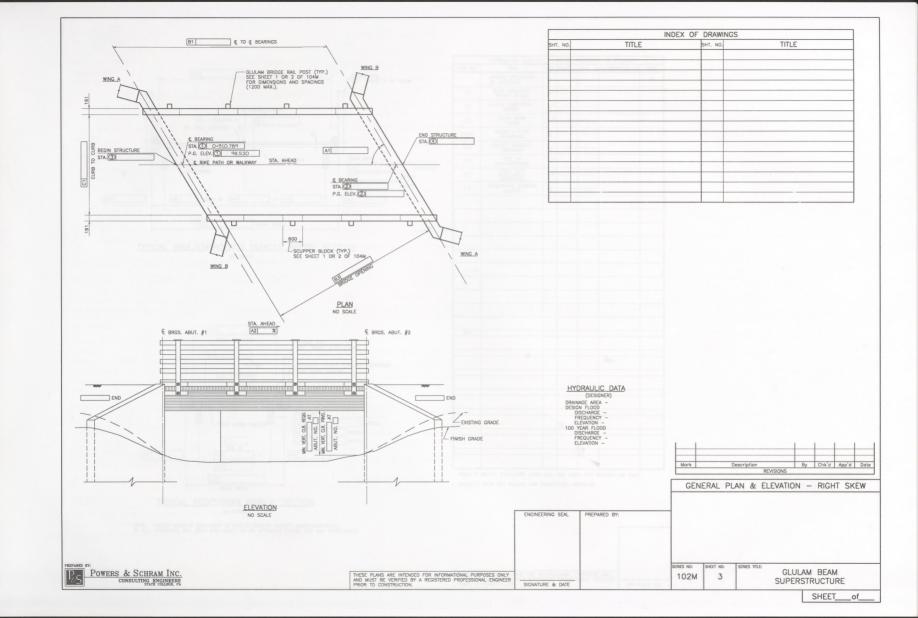




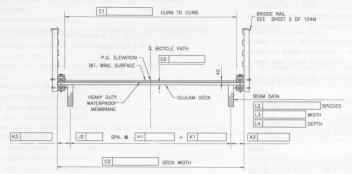




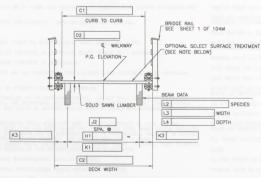








TYPICAL BIKE/EMERGENCY VEHICLE BRIDGE SECTION NO SCALE



TYPICAL PEDESTRIAN BRIDGE SECTION NO SCALE

NOTE: SELECT SURFACE TREATMENT IS PERCOL ELASTIC CEMENT (MICROSURFACING) BY E.J. BRENEMAN, INC. (610-678-9691) OR AN APPROVED EQUAL. (10 mm THICK MAX.)



APPROXIMATE QUANTITIES - BRIDGE STRUCTURE, AS DESIGNED

			-		
Mark	Description	Ву	Chk'd	App'd	Date
	REVISIO	ONS			

TYPICAL SECTION & QUANTIES

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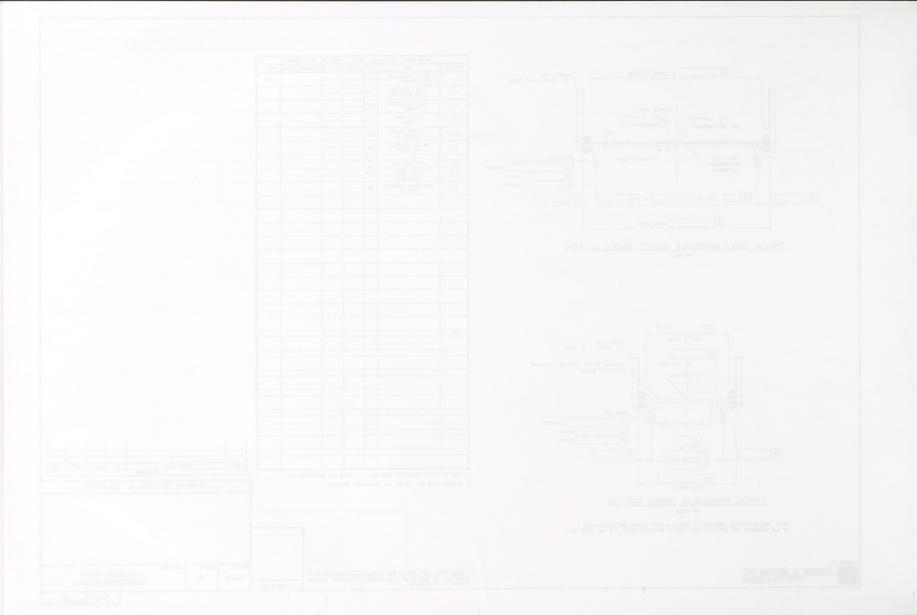
102M ENGINEER'S SEAL

SHEET NO: SERIES TITLE: 4

GLULAM BEAM SUPERSTRUCTURE

SHEET

DEFEASED BY-POWERS & SCHRAM INC. CONSULTING ENGINEERS
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GENERAL NOTES: GENERAL NOTES CONTINUED: DESIGN SPECIFICATIONS STEEL AASHTO LRFD BRIDGE DESIGN SPECIFICATIONS (1994) HOT DIP GALVANIZE ALL TIMBER CONNECTION HARDWARE DESIGN IS IN ACCORDANCE WITH THE LOAD AND RESISTANCE FACTOR DESIGN METHOD. PROVIDE STRUCTURAL STEEL CONFORMING TO AASHTO M270, GRADE 250 (ASTM A709M, GRADE 250) DESIGNATION, EXCEPT WHEN NOTED OTHERWISE PROVIDE BOLTS AND LAG SCREWS CONFORMING TO ASTM A307 DESIGNATION, EXCEPT WHEN NOTED OTHERWISE TYPICAL BIKE/EMERGENCY VEHICLE BRIDGE PROVIDE BOLTS, NUTS, AND WASHERS IN ACCORDANCE WITH AASHTO LRFD BRIDGE DESIGN H DESIGN TRUCK (EMERGENCY VEHICLE) LOAD AT STRENGTH 1 LOAD COMBINATION (17.2KN FRONT AXLE AND 71.2KN REAR AXLE SPACED AT 4.3m TO 9.0m) SPECIFICATION SECTION 6.4.3. PROVIDE MALLEABLE IRON WASHER CONFORMING TO ASTM A47M, GRADE 24118. PEDESTRIAN LOAD AT STRENGTH 1 LOAD COMBINATION (4.1 x 10-3 MPg) PROVIDE LAG SCREWS CONFORMING TO ANSI 818.2.1 - 1981 TYPICAL PEDESTRIAN BRIDGE PROVIDE WOOD SCREWS IN ACCORDANCE WITH ANSI/ASME B18.6.1. WITH A MINIMUM THREADED PORTION PEDESTRIAN LOAD AT STRENGTH 1 LOAD COMBINATION (4.1 x 10-3 MPg) OF TWO-THIRDS THE LENGTH OF THE SHAFT. DEAD LOADS MANUFACTURE SHEAR PLATE CONNECTORS FROM PRESSED STEEL MEETING SOCIETY OF AUTOMOTIVE ENGINEERS SPECIFICATION SAE-1010 OR AN APPROVED EGUAL. TYPICAL BIKE/EMERGENCY VEHICLE BRIDGE BITUMINOUS SURFACE OF 90 kg/m2 COORDINATE THE REQUIREMENTS FOR PROTECTION AND/OR RELOCATION OF UTILITIES WITH THE UTILITY TIMBER BRIDGE COMPONENTS 800 kg/m3 OWNER PRIOR TO STARTING WORK STEEL BRIDGE COMPONENTS 7850 kg/m3 VERIFY AND LOCATE ALL EXISTING UTILITIES PRIOR TO STARTING WORK; CONDUCT OPERATIONS IN A MANNER WHICH ENSURES THAT THE UTILITIES WILL NOT BE DISTURBED OR ENDANGERED, AND ASSUME FULL RESPONSIBILITY FOR ANY DAMAGE TO UTILITIES DURING CONSTRUCTION. THE DEPARTMENT DOES NOT ASSUME RESPONSIBILITY FOR REIMBURSEMENT, PARTICIPATION IN DESIGN AND/OR REVISIONS, OR INCLUDES SURFACE AREA DENSITY OF 150 kg/m2 FOR FUTURE WEARING SURFACE ON THE DECK, LIABILITY FOR ACCURACY OF TYPE SIZE AND LOCATION OF ANY LITHTY SELECT SURFACE TREATMENT OF 22.5 kg/m2 TIMBER USE ONLY QLUE LANIMATED TIMBER FARRICATED WITH EITHER SQUITHERN PINE, RED MAPLE OR 
DOUGLAS FIRE LUMBER GRADED FER NORTHEASTERN LUMBER MAUNTAUTHERS'S ASSOCIATION (ED MAPLE) 
WESTERN WOOD PRODUCTS ASSOCIATION (DOUGLAS FIR) OR SQUITHERN PINE INSPECTION BUREAU 
(SQUITHERN PINE) STANDARDS AND MANUFACTURED FOLLOWING ATC 119, AICT 117 OR CURRENT SPECIFICATIONS. TIMBER BRIDGE COMPONENTS 800 kg/m3 STEEL BRIDGE COMPONENTS 7850 kg/m3 INCLUDES SURFACE AREA DENSITY OF 150 kg/m2 FOR FUTURE WEARING SURFACE ON THE DECK. PROVIDE MINIMUM WET-USE BASE RESISTANCES AND MOE VALUES IN ACCORDANCE WITH SHEET 2 OF 100M. USE GRADE NO. 2 OR BETTER FOR SOLID SAWN LUMBER. PROVIDE MATERIALS AND WORKMANSHIP IN ACCORDANCE WITH AASHTO/AWS/DI.5-88 ALL SAWN LUMBER SHALL BE TREATED IN ACCORDANCE WITH THE REQUIREMENTS OF AWPA STANDARD C14 WITH ONE OF THE FOLLOWING PRESERVATIVES: A. CREOSOTE CONFORMING TO AWPA STANDARD P1 NOTIFY THE REGIONAL HEADQUARTERS OF THE FISH COMMISSION PRIOR TO CONSTRUCTION AND COOPERATE WITH FISH COMMISSION DURING CONSTRUCTION OF BRIDGES OVER FISHABLE STREAMS. B. PENTACHLOROPHENOL CONFORMING TO AWPA STANDARD P8 IN HYDROCARBON SOLVENT, TYPE A, CONFORMING TO AWPA STANDARD P9 C. CCA CONFORMING TO AWPA STANDARD P5 ALL DIMENSIONS SHOWN ARE HORIZONTAL AND IN MILLIMETERS UNLESS OTHERWISE NOTED. GLULAM SHALL BE TREATED TO THE ABOVE REQUIREMENTS WITH CREOSOTE OR PENTACHLOROPHENOL SUPERSTRUCTURE DIMENSIONS SHOWN ARE FOR NORMAL TEMPERATURE OF 20° C. TREATED MATERIAL SHALL BE FREE OF EXCESS PRESERVATIVES ON THE WOODS SURFACE. THE TREATING PROCESS FOR THESE PRESERVATIVES SHALL INCLUDE AN EXPANSION BATH, STEAMING SPREAD FOOTINGS MAY BE ORDERED BY THE ENGINEER TO BE AT ANY ELEVATION OR OF ANY DIMENSIONS NECESSARY TO PROVIDE A PROPER FOUNDATION. AND/OR DRIPPING TO ENSURE THAT THE PRESERVATIVE WILL NOT BLEED. THE SUPERSTRUCTURE MUST BE IN PLACE AND CONNECTED TO SUBSTRUCTURE BEFORE ABUTMENTS ARE TREATED WOOD SHALL BE INSPECTED AND CERTIFIED IN ACCORDANCE WITH AWPA STANDARD M2. BACKFILLED. TREAT ALL ABRASIONS AND CUTS MADE IN THE FIELD WITH THREE BRUSH COATS OF THE FIELD BACK FILL BOTH ABUTMENTS CONCURRENTLY. MAINTAIN SYMMETRICAL LOADING TREATMENT SOLUTION CONCRETE FIELD CUTTING IS NOT PERMITTED UNLESS APPROVED BY THE ENGINEER PROVIDE 50 mm CONCRETE COVER ON REINFORCEMENT BARS EXCEPT AS NOTED WHEN FIELD CUTTING, TREAT WITH BITUMINOUS ASPHALT BASED ROOF CEMENT, COPPER NAPHTHENATE PASTE, OR APPROVED PRESERVATIVE SYSTEM. USE CLASS 20.7MPg CEMENT CONCRETE IN ABUTMENTS BELOW BRIDGE SEAT, WINGWALLS, AND FOOTINGS. PROVIDE PILOT HOLES FOR LAG SCREWS IN RANGE OF (0.60)D TO (0.70)D USE CLASS 24.1MPg CEMENT CONCRETE IN CHEEKWALLS. LEAD HOLES FOR LAG SCREWS WITH D< 12.7mm ARE D+ 0.8mm A HIGHER CLASS CONCRETE MAY BE SUBSTITUTED FOR A LOWER CLASS CONCRETE AT NO ADDITIONAL COST TO THE OWNER. LEAD HOLES FOR LAG SCREWS WITH D> 12.7mm ARE D+ 1.6mm PREPARE BEARING AREAS AS SPECIFIED IN CONTRACT DRAWINGS. ALWAYS COAT LAG SCREW THREADS WITH BITUMINOUS ASPHALT BASED ROOF CEMENT, COPPER NAPHTHENATE PASTE, OR APPROVED PRESERVATIVE SYSTEM BEFORE INSTALLING LAG SCREW. SET ANCHOR BOLTS TO TEMPLATE OR IN PERFORMED HOLES. DO NOT DRILL UNLESS SPECIFICALLY INDICATED ON PLANS. FILL THE PERFORMED HOLES WITH NON-SHRINK GROUT. FILL THE CLEARANCE BETWEEN ANCHOR BOLTS AND HOLES IN MASONRY PLATES WITH APPROVED NONHARDENING CAULKING DO NOT DRIVE LAG SCREW WITH HAMMER. SCREW OR TORQUE LAG SCREWS. PROVIDE SUFFICIENT LAG SCREW LENGTH SO LAG SCREW SHANK WILL PENETRATE RECEIVING MEMBER. PROVIDE CRADE. 400 REINFORCING STEEL BARS THAT MEET THE REQUIREMENTS OF ASTM A 615M, A 156M, A SUBMIT SHOP DRAWINGS SHOWING DETAILS OF ALL GLULAM CONSTRUCTION FOR APPROVAL TO THE ENGINEER PRIOR TO FABRICATION OPERATIONS. ALL TIMBER DIMENSIONS SHOWN ARE ACTUAL UNLESS OTHERWISE NOTED PILES Mark Chk'd App'd REVISIONS EPOXY-COAT SUBSTRUCTURE REINFORCEMENT BARS AS INDICATED. DO NOT PERMIT SPLICES IN PILES GENERAL NOTES RAKE-FINISH ALL HORIZONTAL CONSTRUCTION JOINTS, EXCEPT AS INDICATED. PROVIDE PILES IN ACCORDANCE WITH SHEET 2 OF 100M. REINFORCEMENT BAR SCHEDULE IS FOR INFORMATION ONLY, VERIFY IT PRIOR TO BIDDING AND FARRICATION. PLACE CHEEKWALL CONCRETE AFTER BEAMS ARE SET IN POSITION CHAMFER EXPOSED CONCRETE EDGES 25 mm BY 25 mm, EXCEPT AS NOTED. PROVIDE MINIMUM LAP AND EMBEDMENT LENGTH OF 30 DIAMETERS OR IN ACCORDANCE WITH ASSHTO SECTION A5.11 AND D5.11, WHICHEVER IS GREATER.

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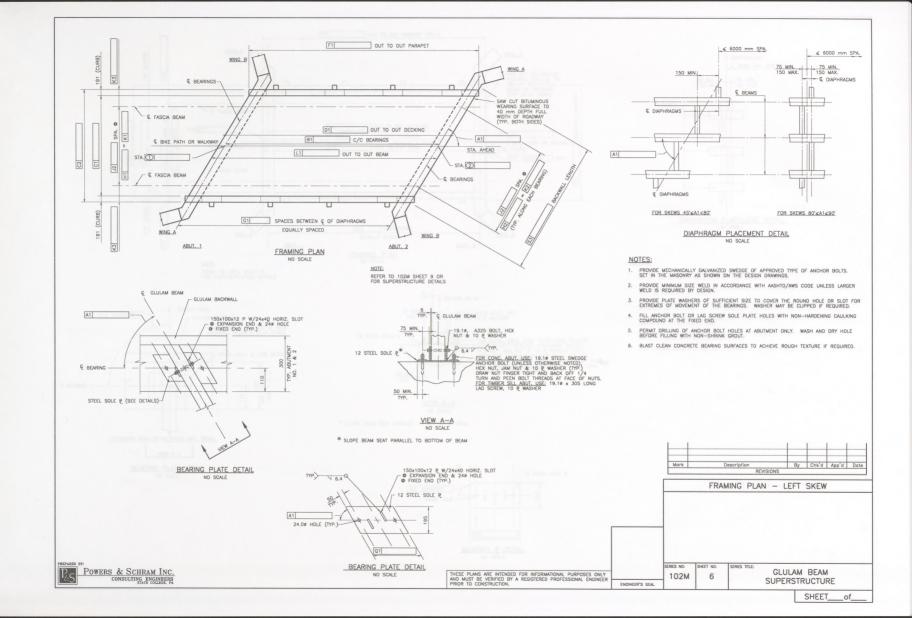
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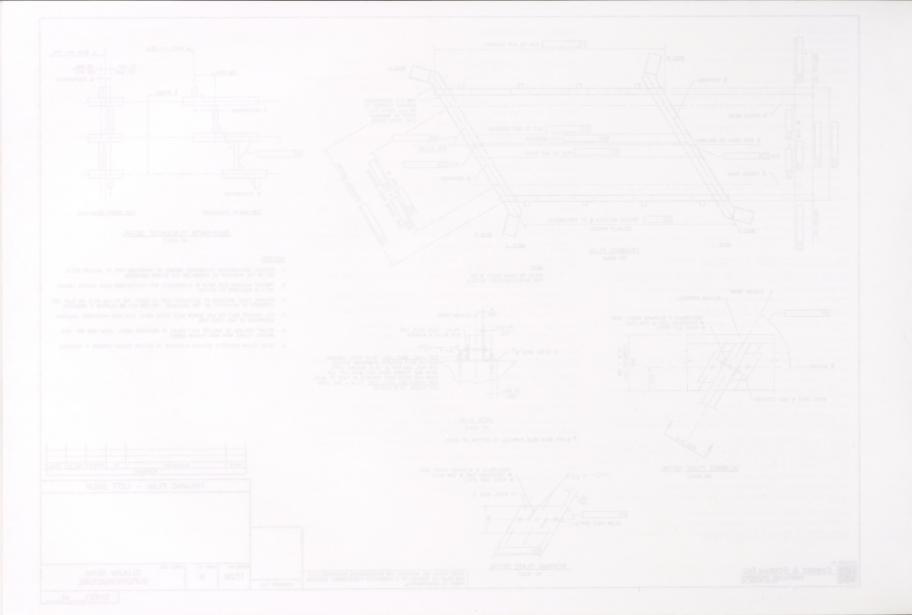
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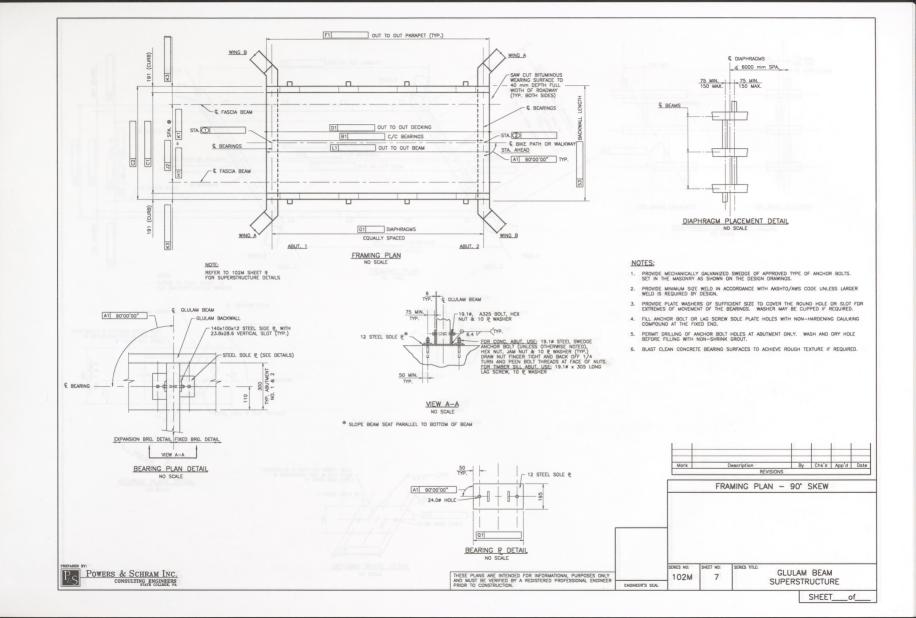
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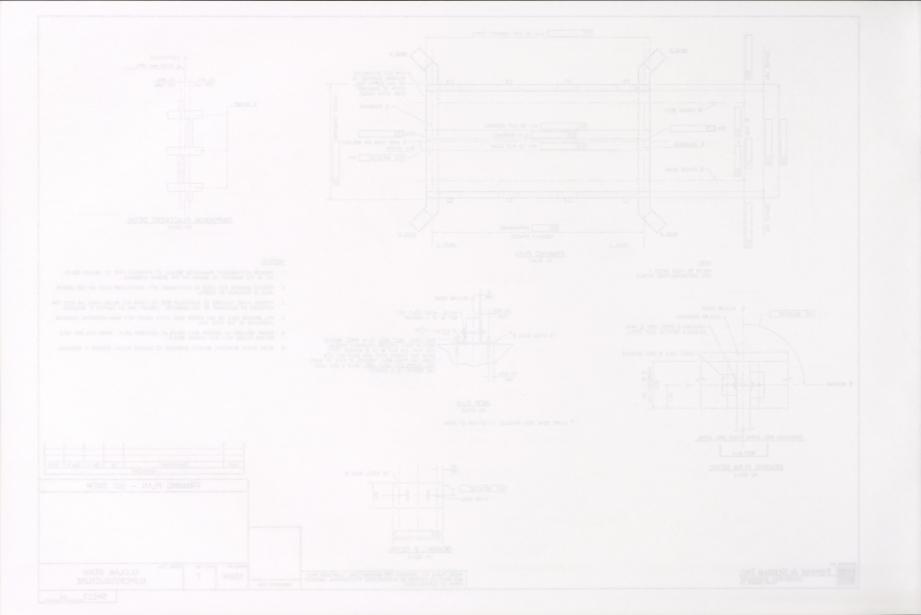
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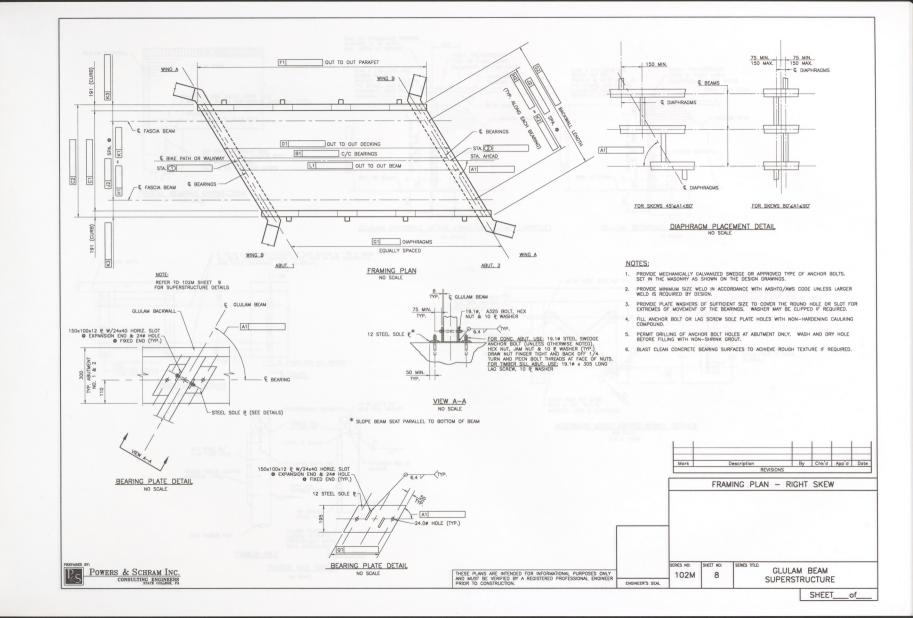
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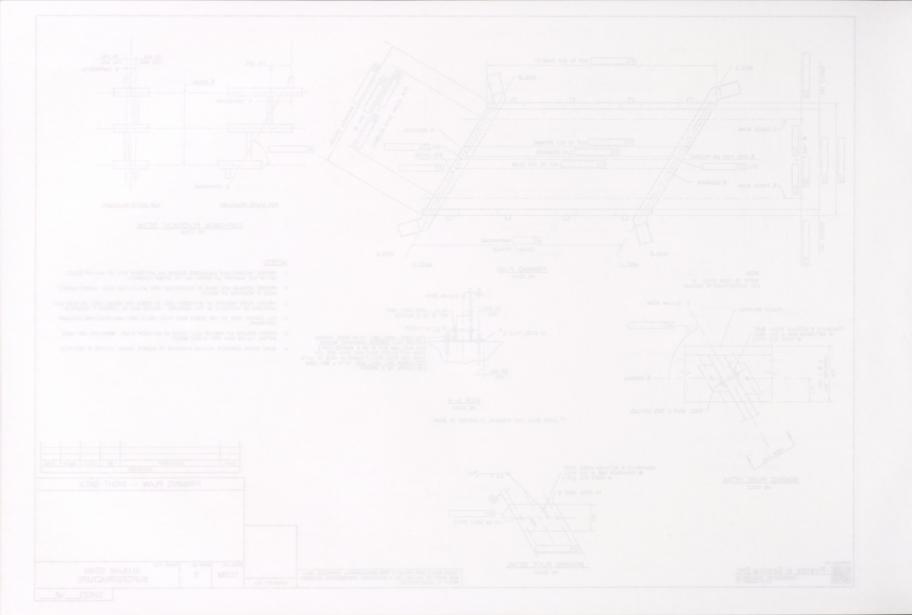


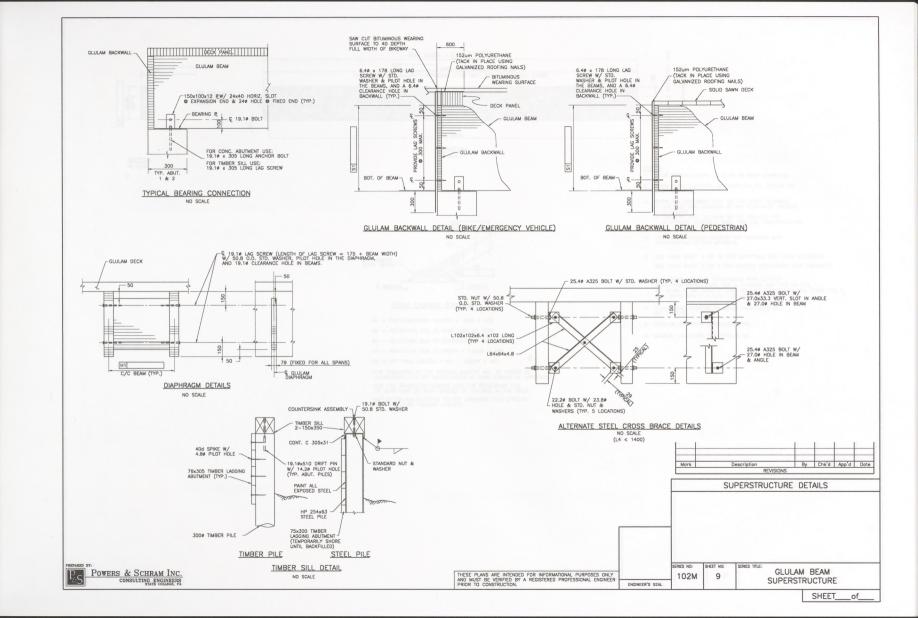


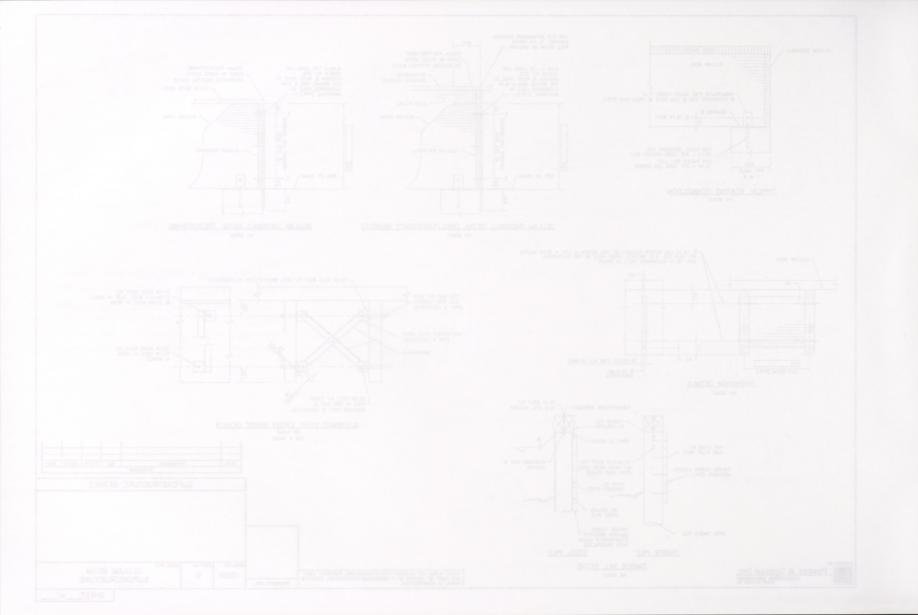


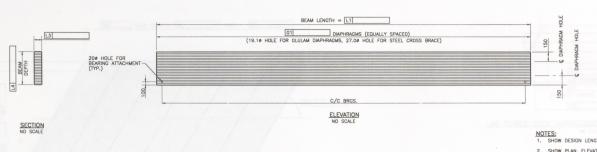


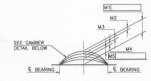












## BEAM CAMBER DIAGRAM

- M1 = PRE-FABRICATED CAMBER = 3(M2 + M3)
- M2 = DEFLECTION DUE TO DEAD LOAD OF BEAM
- M3 = DEFLECTION DUE TO SUPERIMPOSED DEAD LOAD
- M4 = DEFLECTION DUE TO CREEP = 1.5(M2 + M3)
- M5 = NET FINAL CAMBER = M1 2.5(M2 + M3)
- \*THE THICKNESS OF THE WEARING COURSE WILL BE VARIED TO COMPENSATE FOR ANY INACCURACIES IN BEAM CAMBER AS APPLICABLE.
- \*THE PRE-FABRICATED CAMBER LESS THE DEFLECTION DUE TO DEAD LOAD OF BEAM SHOULD BE CHECKED IN THE FIELD.
- \*DEFLECTION CALCULATIONS DO NOT CONSIDER LOAD EFFECTS DUE TO FUTURE WEARING SURFACE.

- 1. SHOW DESIGN LENGTH OF BEAM ON SHOP DRAWINGS.
- SHOW PLAN, ELEVATION, SECTIONS AND ALL DETAILS ON SHOP DRAWINGS.
- SHOW THE FOLLOWING DATA ON THE SHOP DRAWINGS:
   THE SIZE AND LOCATION OF THE TEMPORARY STORAGE
   THE TYPE AND LOCATION OF THE BRAING AND
   TEMPORARY SUPPORTS USED FOR THE TRANSPORTATION
   OF THE BEAMS.
- FABRICATOR CHECKS STABILITY FOR HANDLING AND TRANSPORTING OF THE MEMBERS.
- 5. SEE 102M SHEET 9 OR 10 FOR DIAPHRAGM BOLT HOLE LOCATIONS. SEE 102M SHEET 8 OR 9 FOR BEARING ATTACHMENT HOLE LOCATIONS.
- CONSTRUCT BEAMS IN ACCORDANCE WITH CURRENT INSPECTION MANUAL, AITC 200 & CURRENT AITC 119 OR 117.
   ALL BEAM TO BE MANUFACTURED WITH A MINIMUM 16.5 MPo (2400 PSI) F AND 12410 MPo (1.8x10E6 PSI) MOE (DRY-USE VALUES).
- SPLICE JOINT LOCATION ON OUTER LAMINATIONS IS NOT CRITICAL.
- 8. MAXIMUM LAMINATION THICKNESS IS 50.
- 9. MINIMUM LAMINATION THICKNESS IS 20.

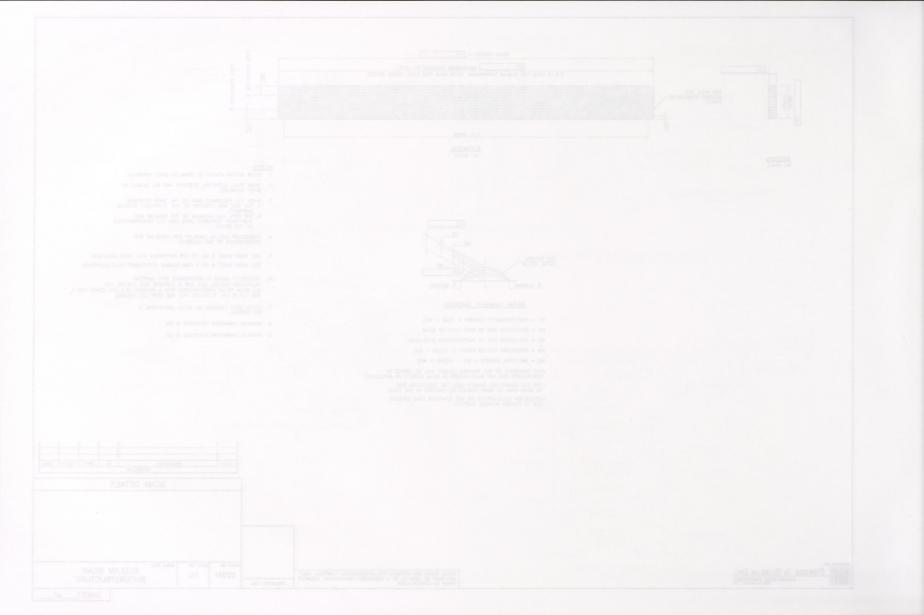
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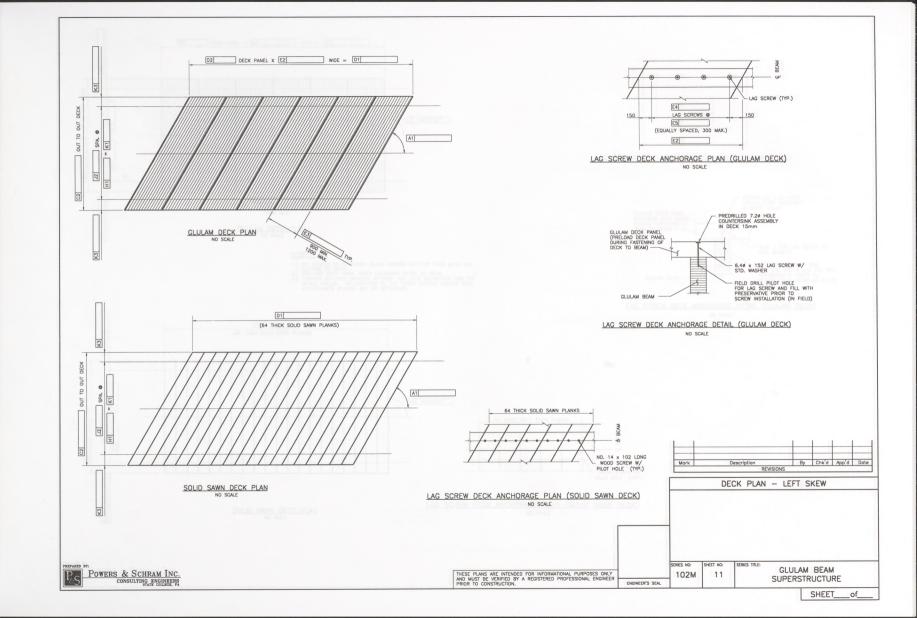


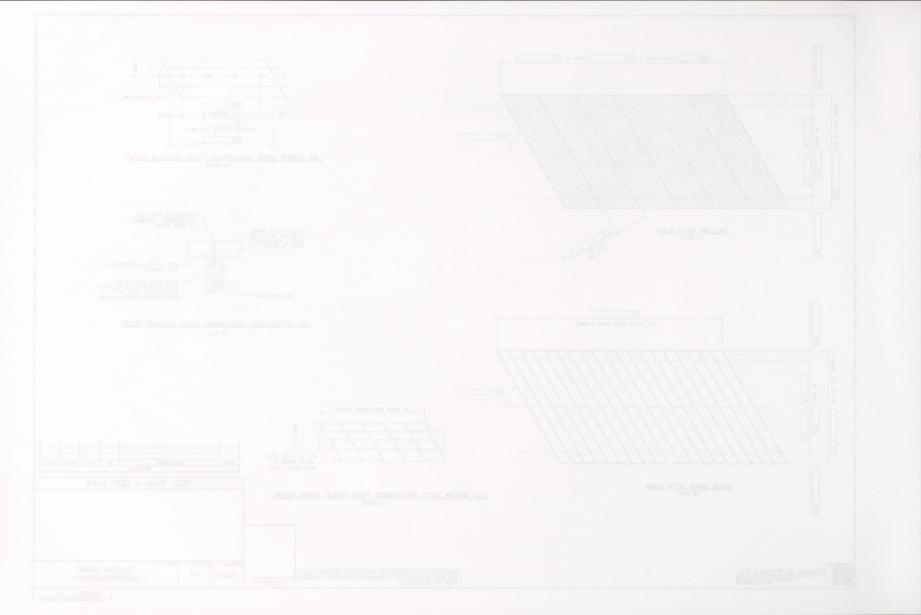
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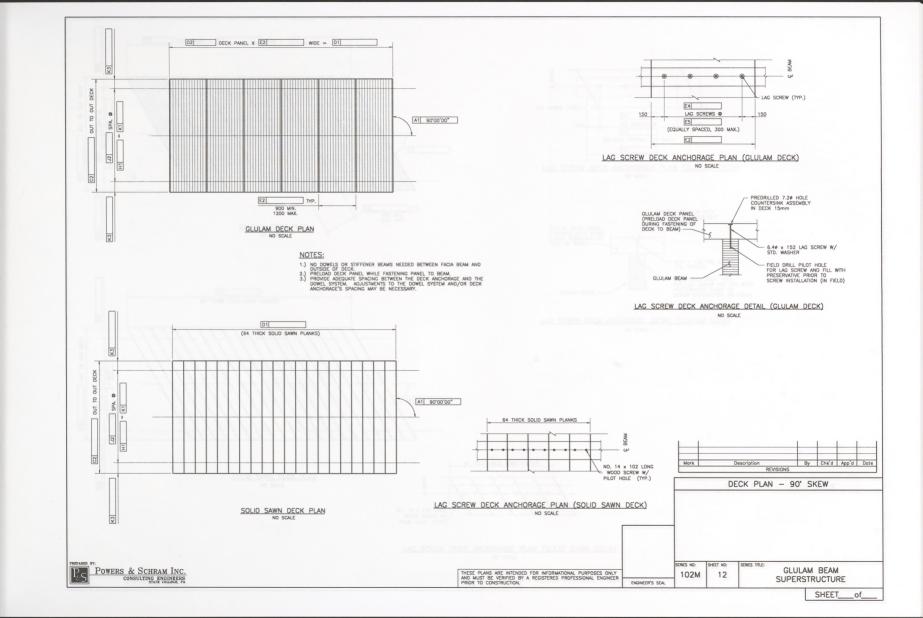
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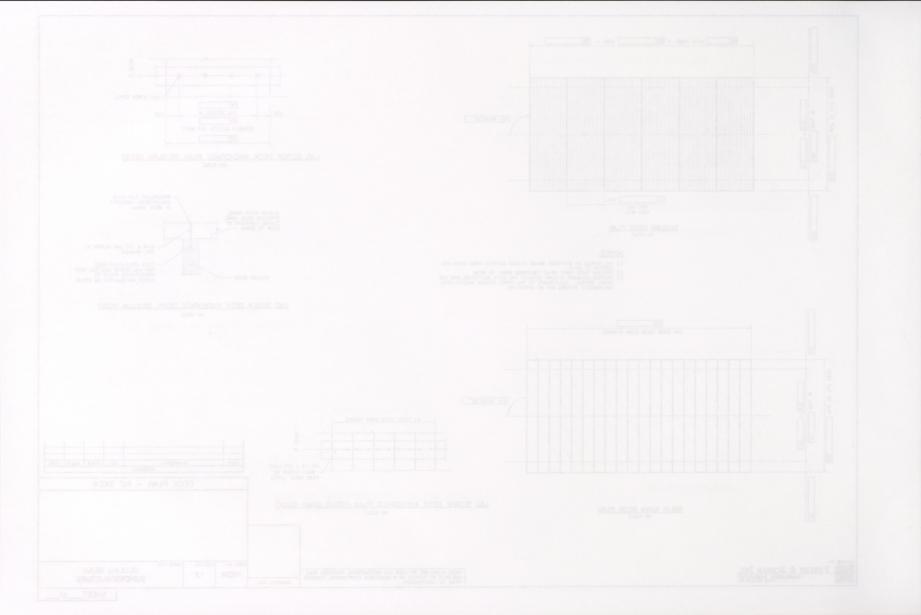
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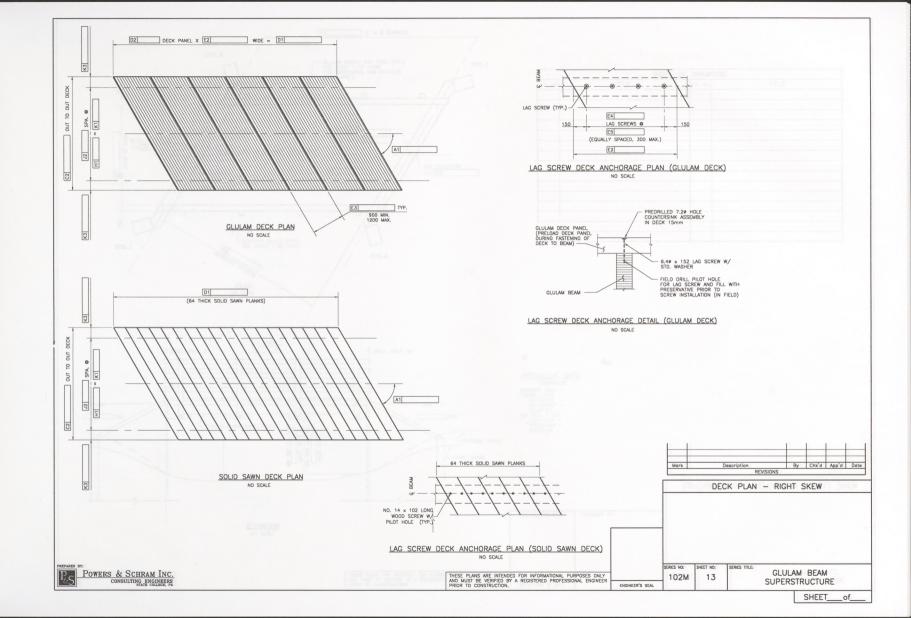


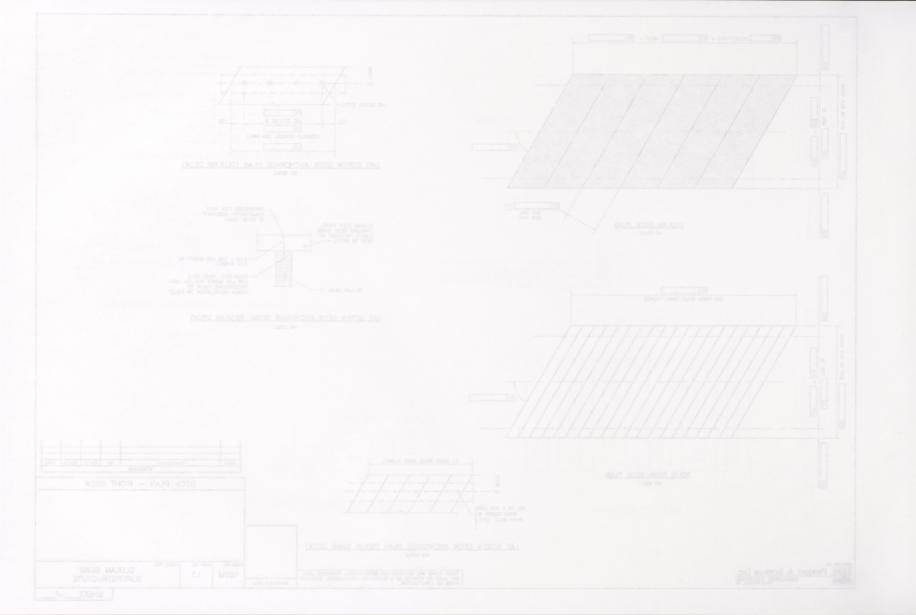


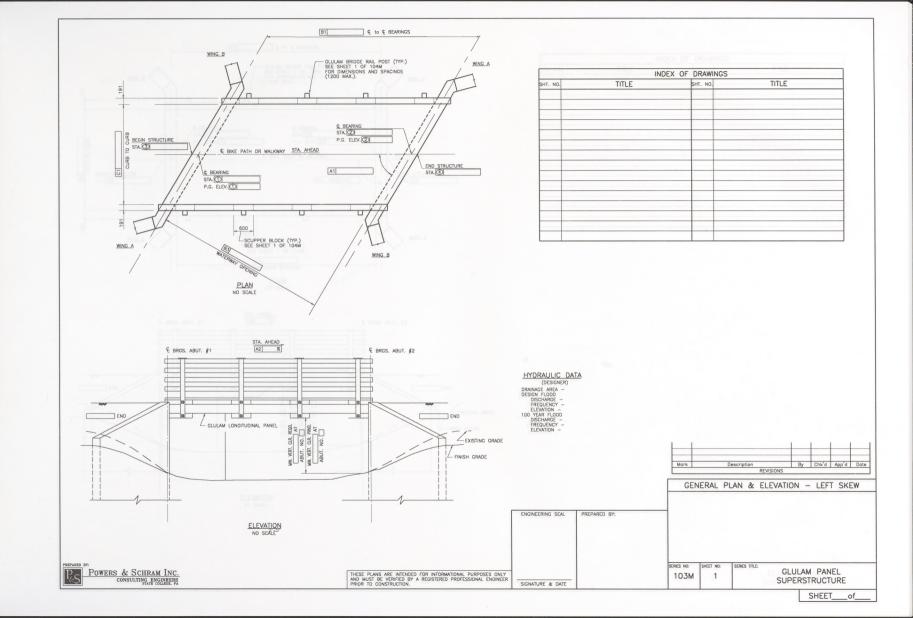


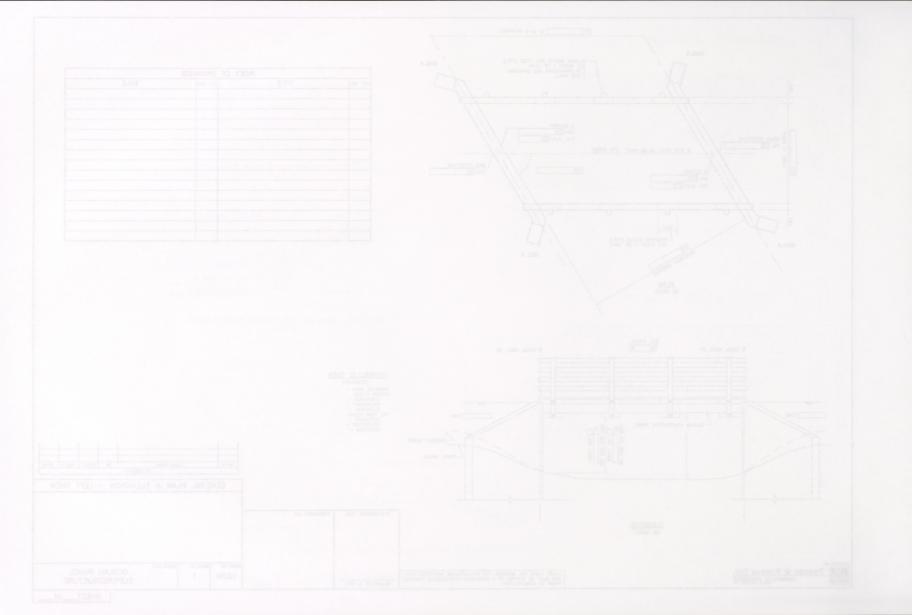


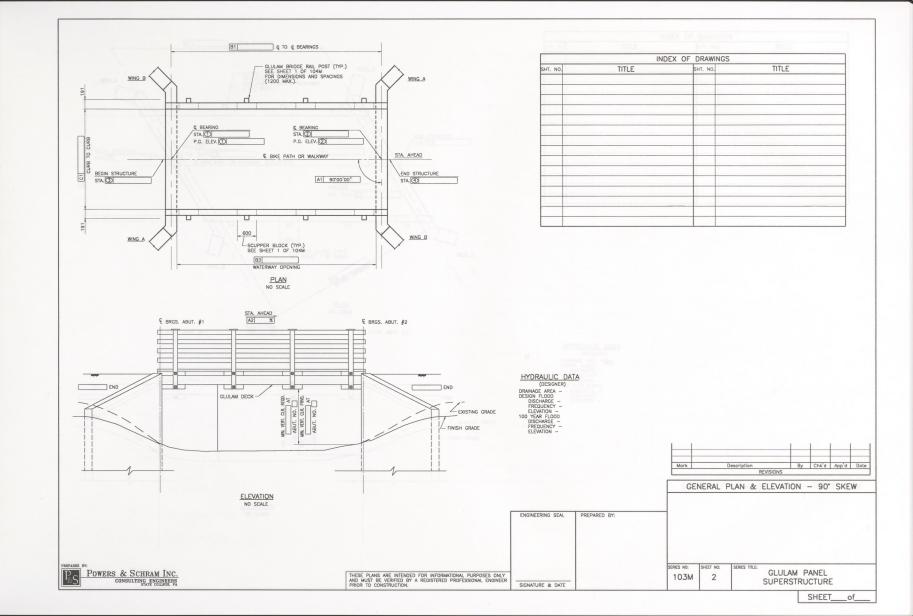


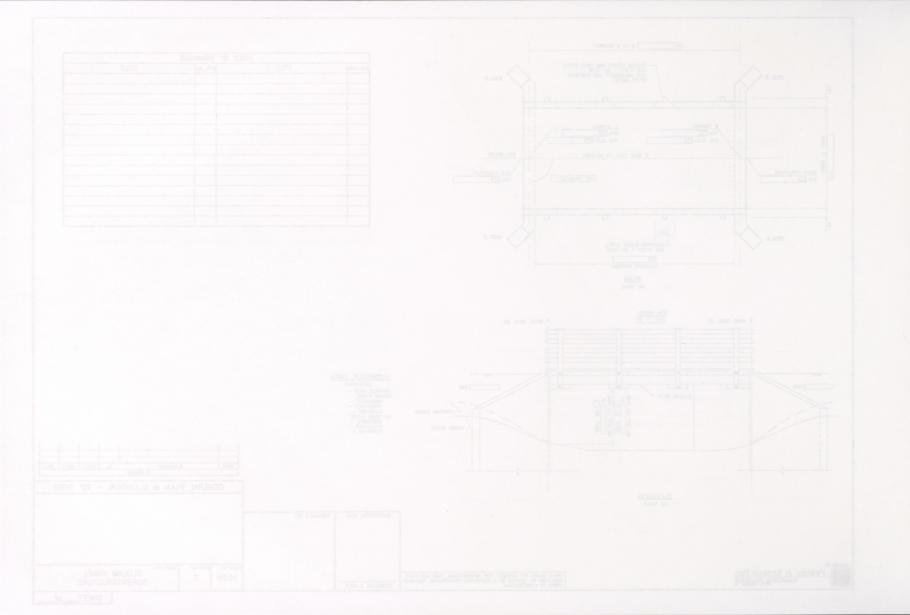


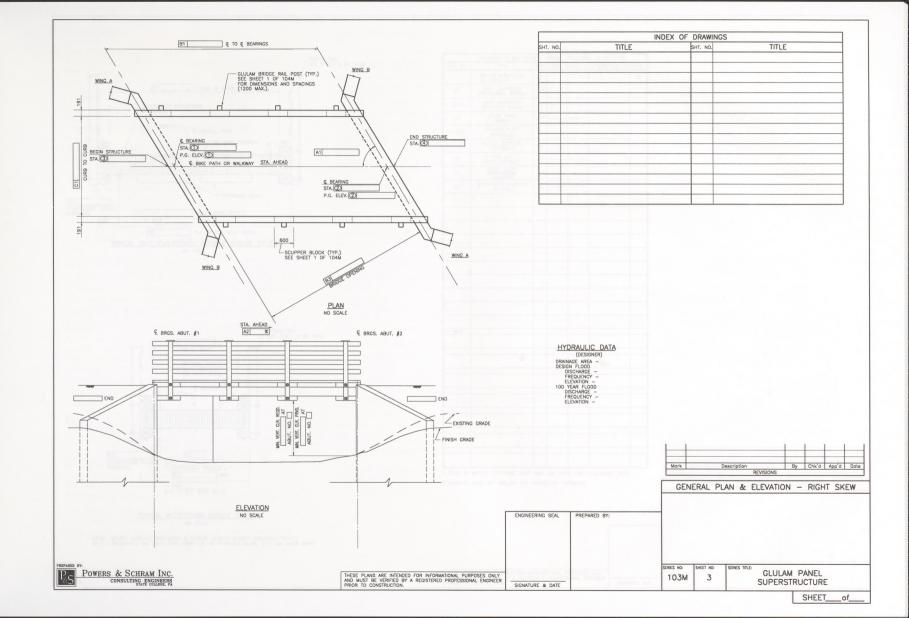


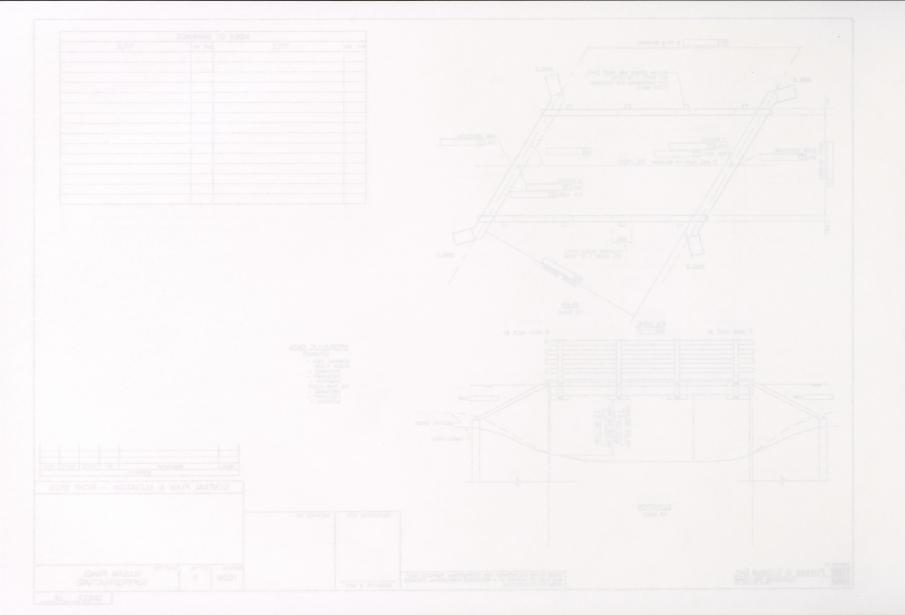


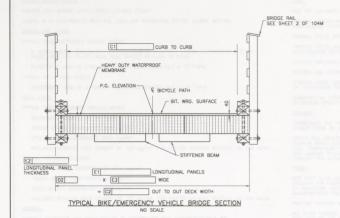


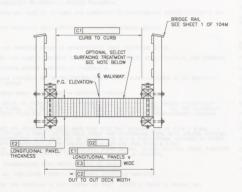












TYPICAL PEDESTRIAN BRIDGE SECTION NO SCALE

NOTE: SELECT SURFACE TREATMENT IS PERCOL ELASTIC CEMENT (MICROSURFACING) BY E.J. BRENEMAN, INC. (610-678-9691) OR AN APPROVED EQUAL. (10 mm THICK MAX.)

PREPARED	BY:
$\mathbf{p}_{-}$	POWERS & SCHRAM INC.
185	CONSULTING ENGINEERS

	APPROXIMATE QUANTITI					
ITEM NO.	BRIDGE STRUCTURE	LS	ABUT, 1	ABUT. 2	SUPERSTRUCTURE	LS
(1)	AS DESIGNED  GLUE LAMINATED	m <sup>3</sup>				-
	LONGITUDINAL PANELS  GLUE LAMINATED					
(1)	STIFFENER BEAMS	m <sup>3</sup>				
(1)	SOLID SAWN TIMBER	m <sup>3</sup>	100000			
(1)(2)	BEARING PLATE ASSEMBLIES	kg				
(1)	SELECT SURFACE TREATMENT	kg				
(1)	152 um POLYURETHANE	m <sup>2</sup>				
(1)	HEAVY DUTY WATERPROOF MEMBRANE	m <sup>2</sup>				
(1)	BITUMINOUS WEARING COURSE	kg				
uncknow	DE ANY URLEY					
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M2 2000	THE RESERVE	-				
A1. 0.0	PER CURSIFICATION TOA			MC UNI	40.0	
040000	MANAGE CONTROL					
ITEMS IN	BRIDGE STRUCTURE LUMP	SUM	ITEM GIVE	N FOR I	NFORMATION ONLY	

					-
Mark	Description	By	Chk'd	App'd	
	REVISIO	ONS			_

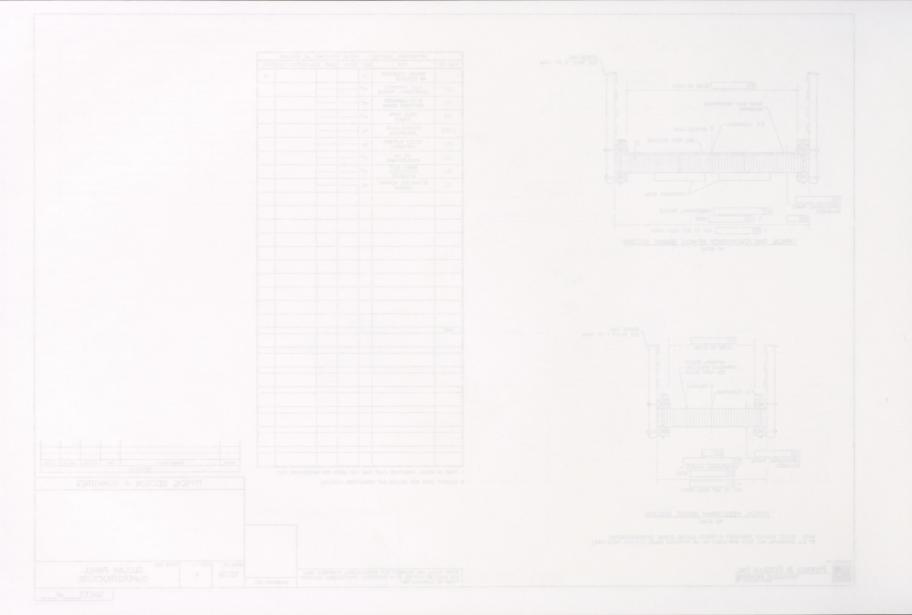
TYPICAL SECTION & QUANTITIES

THESE PLANS ARE INTENDED FOR INFORMATIONAL PURPOSES ONLY AND MUST BE VERIFIED BY A REGISTERED PROFESSIONAL ENGINEER PRIOR TO CONSTRUCTION. ENGINEER'S SEAL

SERIES TITLE: SERIES NO: SHEET NO: 103M 4

GLULAM PANEL SUPERSTRUCTURE

> SHEET of



# GENERAL NOTES: DESIGN SPECIFICATIONS

AASHTO LRFD BRIDGE DESIGN SPECIFICATIONS (1994)

DESIGN IS IN ACCORDANCE WITH THE LOAD AND RESISTANCE FACTOR DESIGN METHOD.

### DESIGN LIVE LOADS

TYPICAL BIKE/EMERGENCY VEHICLE BRIDGE

H DESIGN TRUCK (EMERGENCY VEHICLE) LOAD AT STRENGTH 1 LOAD COMBINATION (17.2KN FRONT AXLE AND 71.2KN REAR AXLE SPACED AT 4.3m TO 9.0m)

PEDESTRIAN LOAD AT STRENGTH 1 LOAD COMBINATION (4.1 x 10-3 MPa)

TYPICAL PEDESTRIAN BRIDGE

PEDESTRIAN LOAD AT STRENGTH 1 LOAD COMBINATION (4.1 x 10-3 MPo)

### DEAD LOADS

TYPICAL BIKE/EMERGENCY VEHICLE BRIDGE

BITUMINOUS SURFACE OF 90 kg/m2

TIMBER BRIDGE COMPONENTS 800 kg/m3

STEEL BRIDGE COMPONENTS 7850 kg/m3

INCLUDES SURFACE AREA DENSITY OF 150 kg/m2 FOR FUTURE WEARING SURFACE ON THE DECK.

TYPICAL PEDESTRIAN BRIDGE

SELECT SURFACE TREATMENT OF 22.5 kg/m2

TIMBER BRIDGE COMPONENTS 800 kg/m3

STEEL BRIDGE COMPONENTS 7850 kg/m3

INCLUDES SURFACE AREA DENSITY OF 150 kg/m2 FOR FUTURE WEARING SURFACE ON THE DECK.

#### GENER

PROVIDE MATERIALS AND WORKMANSHIP IN ACCORDANCE WITH AASHTO/AWS/DI.5-88 BRIDGE WELDING CODE. AND CONTRACT SPECIAL PROVISIONS.

NOTIFY THE REGIONAL HEADQUARTERS OF THE FISH COMMISSION PRIOR TO CONSTRUCTION AND COOPERATE WITH FISH COMMISSION DURING CONSTRUCTION OF BRIDGES OVER FISHABLE STREAMS.

ALL DIMENSIONS SHOWN ARE HORIZONTAL AND IN MILLIMETERS UNLESS OTHERWISE NOTED.

SUPERSTRUCTURE DIMENSIONS SHOWN ARE FOR NORMAL TEMPERATURE OF 20°C.

SPREAD FOOTINGS MAY BE ORDERED BY THE ENGINEER TO BE AT ANY ELEVATION OR OF ANY DIMENSIONS NECESSARY TO PROVIDE A PROPER FOUNDATION.

THE SUPERSTRUCTURE MUST BE IN PLACE AND CONNECTED TO SUBSTRUCTURE BEFORE ABUTMENTS ARE BACKFILLED.

BACK FILL BOTH ABUTMENTS CONCURRENTLY. MAINTAIN SYMMETRICAL LOADING.

# CONCRETE

PROVIDE 50 mm CONCRETE COVER ON REINFORCEMENT BARS, EXCEPT AS NOTED.

USE CLASS 20.7MPo CEMENT CONCRETE IN ABUTMENTS BELOW BRIDGE SEAT, WINGWALLS, AND FOOTINGS.

USE CLASS 24.1MPg CEMENT CONCRETE IN CHEEKWALLS.

A HIGHER CLASS CONCRETE MAY BE SUBSTITUTED FOR A LOWER CLASS CONCRETE AT NO ADDITIONAL COST TO THE OWNER.

PREPARE BEARING AREAS AS SPECIFIED IN CONTRACT DRAWINGS.

SET ANCHOR BOLTS TO TEMPLATE OR IN PERFORMED HOLES. DO NOT DRILL UNLESS SPECIFICALLY INDICATED ON PLANS. FILL THE PERFORMED HOLES WITH NON-SHRINK GROUT. FILL THE CLEARANCE BETWEEN ANCHOR BOLTS AND HOLES IN MASONRY PLATES WITH APPROVED NONHARDEDING CAULKING

PROVIDE GRADE 400 RENFORCING STEEL BARS THAT MEET THE REQUIREMENTS OF ASTW A BISM, A BISM, A BISM, AND AN TEMPORATION OF THE RENFORCING STEEL BARS SURESS SPECIFIED. AS SURESS SPECIFIED. SECTIONAL AREA, IF APPROVED BY THE ENDIFIER DO NOT USE REN. STEEL ASTS AUGUST AS RENFORCEMENT BARS IN BRODE PIERS, ABUTMENTS, SHEAR BLOCKS, BEAMS, FOOTINGS, PILES, PARAPETS AND WHERE BEAMONG OR WELDING OF THE RENFORCEMENT BARS IS INDICATED.

EPOXY-COAT SUBSTRUCTURE REINFORCEMENT BARS AS INDICATED.

RAKE-FINISH ALL HORIZONTAL CONSTRUCTION JOINTS, EXCEPT AS INDICATED.

REINFORCEMENT BAR SCHEDULE IS FOR INFORMATION ONLY. VERIFY IT PRIOR TO BIDDING AND FABRICATION,

PLACE CHEEKWALL CONCRETE AFTER BEAMS ARE SET IN POSITION.

CHAMFER EXPOSED CONCRETE EDGES 25 mm BY 25 mm, EXCEPT AS NOTED.

PROVIDE MINIMUM LAP AND EMBEDMENT LENGTH OF 30 DIAMETERS OR IN ACCORDANCE WITH ASSHTO SECTION A5.11 AND 05.11, WHICHEVER IS GREATER.

# GENERAL NOTES CONTINUED:

STEEL

HOT DIP GALVANIZE ALL TIMBER CONNECTION HARDWARE.

PROVIDE STRUCTURAL STEEL CONFORMING TO AASHTO M270, GRADE 250 (ASTM A709M, GRADE 250) DESIGNATION, EXCEPT WHEN NOTED OTHERWISE.

PROVIDE BOLTS AND LAG SCREWS CONFORMING TO ASTM A307 DESIGNATION. EXCEPT WHEN NOTED OTHERWISE.

PROVIDE BOLTS, NUTS, AND WASHERS IN ACCORDANCE WITH AASHTO LRFD BRIDGE DESIGN SPECIFICATION SECTION 6.4.3.

PROVIDE MALLEABLE IRON WASHER CONFORMING TO ASTM A47M, GRADE 24118.

PROVIDE LAG SCREWS CONFORMING TO ANSI B18.2.1 - 1981

PROVIDE WOOD SCREWS IN ACCORDANCE WITH ANSI/ASME B18.6.1. WITH A MINIMUM THREADED PORTION OF TWO-THIRDS THE LENGTH OF THE SHAFT.

MANUFACTURE SHEAR PLATE CONNECTORS FROM PRESSED STEEL MEETING SOCIETY OF AUTOMOTIVE ENGINEERS SPECIFICATION SAE-1010 OR AN APPROVED EGUAL.

#### UTILITIES

COORDINATE THE REQUIREMENTS FOR PROTECTION AND/OR RELOCATION OF UTILITIES WITH THE UTILITY OWNER PRIOR TO STARTING WORK.

VERIFY AND LOCATE ALL EXISTING UTILITIES PRIOR TO STARTING WORK; CONDUCT OPERATIONS IN A MANKER WHICH ENSURES THAT THE UTILITIES WILL NOT BE DISTURBED OR ENDANGERD, AND ASSUME RESULT POR ANY DAMAGE TO UTILITIES DURING CONSTRUCTION. THE DEPARTMENT DOES NOT ASSUME RESPONSIBILITY FOR REIMBURSEMENT, PARTICIPATION IN DESIGN AND/OR REVISIONS, OR LABILITY FOR ACCUPACY OF TYPE, SZE, AND LOCATION OF ANY UTILITY.

### TIMBER

USE ONLY GLUE LAMANTED THISER FARRICHED WITH EITHER SOUTHERN PINE, RED MAPLE OR DOUGLAS FIR LUMBER GRADED PER NORTH-METERN LUMBER MANUFACTURER'S ASSOCIATION (RED MAPLE) OR NORTHERN SOFTWOOD LUMBER BUREAU (DOUGLAS FIR AND SOUTHERN PINE) STANDARDS AND MANUFACTURER'D FOLLOWING ART C1 19, AITC 117 OR CURRENT PSECIFICATIONS.

PROVIDE MINIMUM WET-USE BASE RESISTANCES AND MOE VALUES IN ACCORDANCE WITH SHEET 2 OF 100M.

ALL SAWN LUMBER SHALL BE TREATED IN ACCORDANCE WITH THE REQUIREMENTS OF AWPA STANDARD C14 WITH ONE OF THE FOLLOWING PRESERVATIVES:

A. CRESCRIE CORPORATION OF AWRA STANDARD P1

CONFORMING TO AWPA STANDARD P3

AWPA STANDARD P8 IN HYDROCARBON SOLVENT, TYPE A, ED. CONFORMING TO AWPA STANDARD P8

C. CCA CONFORMING TO AWPA STANDARD P5

GLULAM SHALL BE TREATED TO THE ABOVE REQUIREMENTS WITH CREOSOTE OR PENTACHLOROPHENOL.

TREATED MATERIAL SHALL BE FREE OF EXCESS PRESERVATIVES ON THE WOODS SURFACE. THE TREATING PROCESS FOR THESE PRESERVATIVES SHALL INCLUDE AN EXPANSION BATH, STEAMING AND/OR DRIPPING TO ENSURE THAT THE PRESERVATIVE WILL NOT BLEED.

TREATED WOOD SHALL BE INSPECTED AND CERTIFIED IN ACCORDANCE WITH AWPA STANDARD M2.

TREAT ALL ABRASIONS AND CUTS MADE IN THE FIELD WITH THREE BRUSH COATS OF THE FIELD TREATMENT SOLUTION.

FIELD CUTTING IS NOT PERMITTED UNLESS APPROVED BY THE ENGINEER.

WHEN FIELD CUTTING, TREAT WITH BITUMINOUS ASPHALT BASED ROOF CEMENT, COPPER NAPHTHENATE PASTE, OR APPROVED PRESERVATIVE SYSTEM.

PROVIDE PILOT HOLES FOR LAG SCREWS IN RANGE OF (0.06)D TO (0.85)D

LEAD HOLES FOR LAG SCREWS WITH D< 12.7mm ARE D+ 0.8mm

LEAD HOLES FOR LAG SCREWS WITH D> 12.7mm ARE D+ 1.6mm

ALWAYS COAT LAG SCREW THREADS WITH BITUMINOUS ASPHALT BASED ROOF CEMENT, COPPER NAPHTHENATE PASTE, OR APPROVED PRESERVATIVE SYSTEM BEFORE INSTALLING LAG SCREW.

DO NOT DRIVE LAG SCREW WITH HAMMER. SCREW OR TOROUG LAG SCREWS.

PROVIDE SUFFICIENT LAG SCREW LENGTH SO LAG SCREW SHANK WILL PENETRATE RECEIVING MEMBER.

SUBMIT SHOP DRAWINGS SHOWING DETAILS OF ALL GLULAM CONSTRUCTION FOR APPROVAL TO THE ENGINEER PRIOR TO FABRICATION OPERATIONS.

ALL TIMBER DIMENSIONS SHOWN ARE ACTUAL UNLESS OTHERWISE NOTED.

# PILES

DO NOT PERMIT SPLICES IN PILES.

PROVIDE PILES IN ACCORDANCE WITH SHEET 2 OF 100M

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Mark	Description	By	Chk'd	App'd	Date

GENERAL NOTES

ERIES NO: SHEET NO: SERVE

103M

FNGINEER'S SEAL

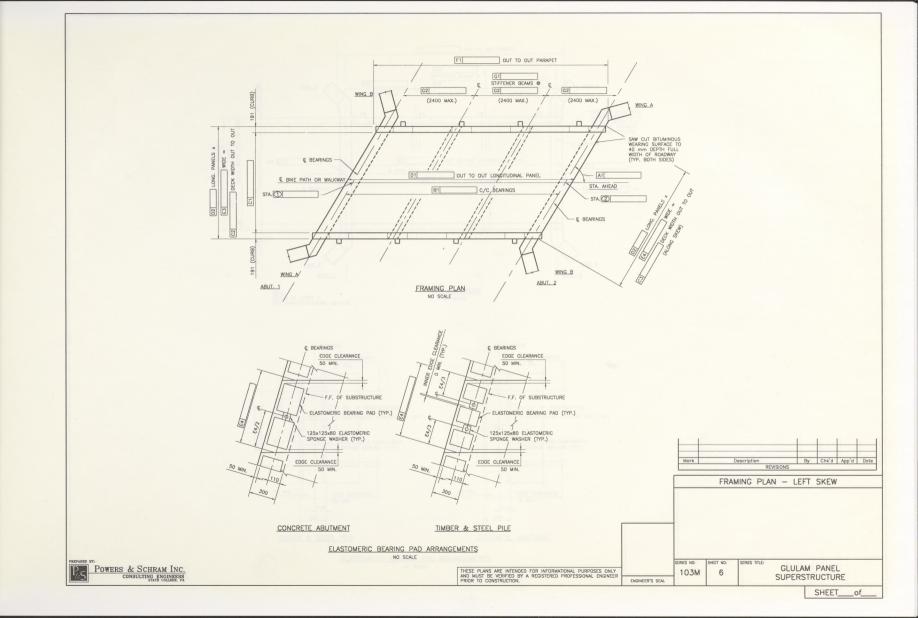
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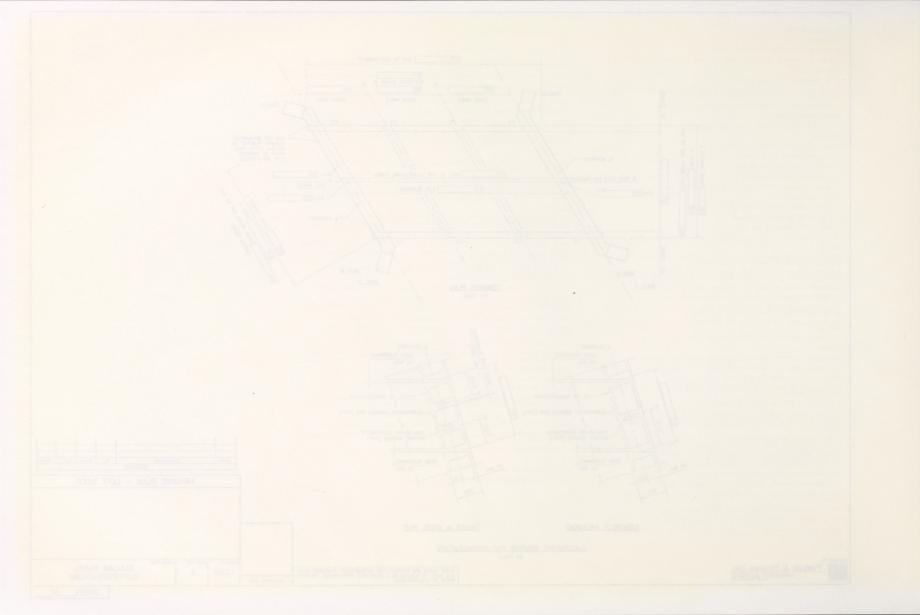
GLULAM PANEL SUPERSTRUCTURE

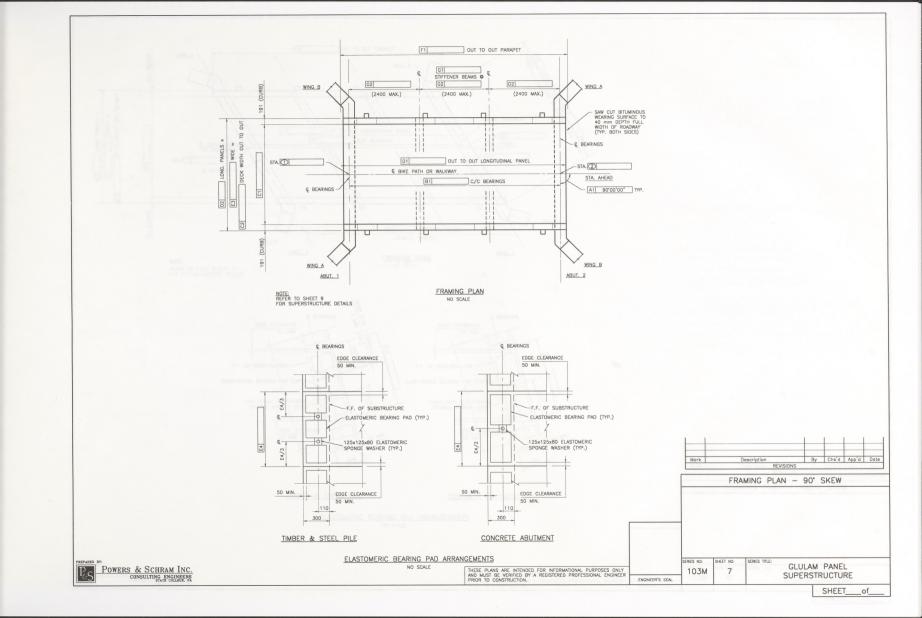
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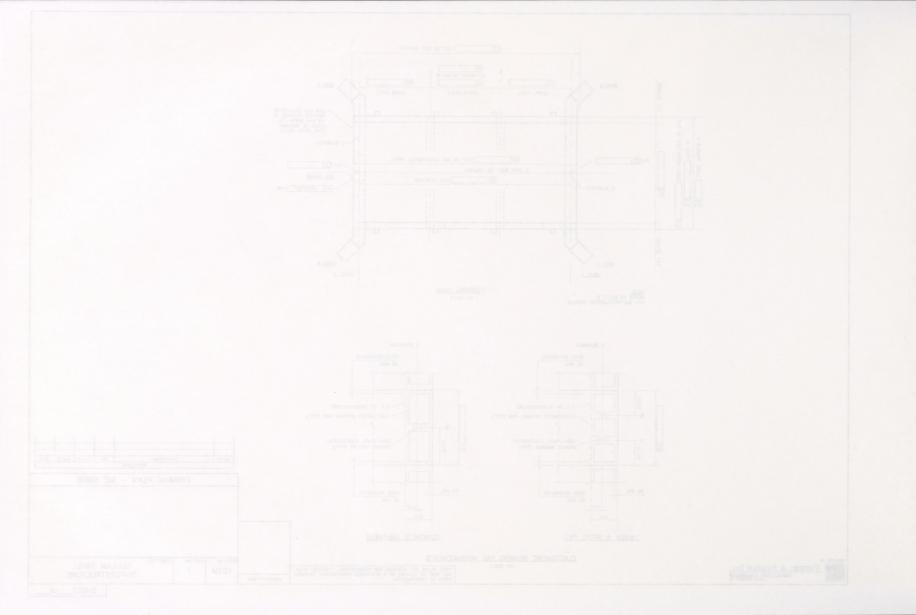
Powers & Schram Inc.

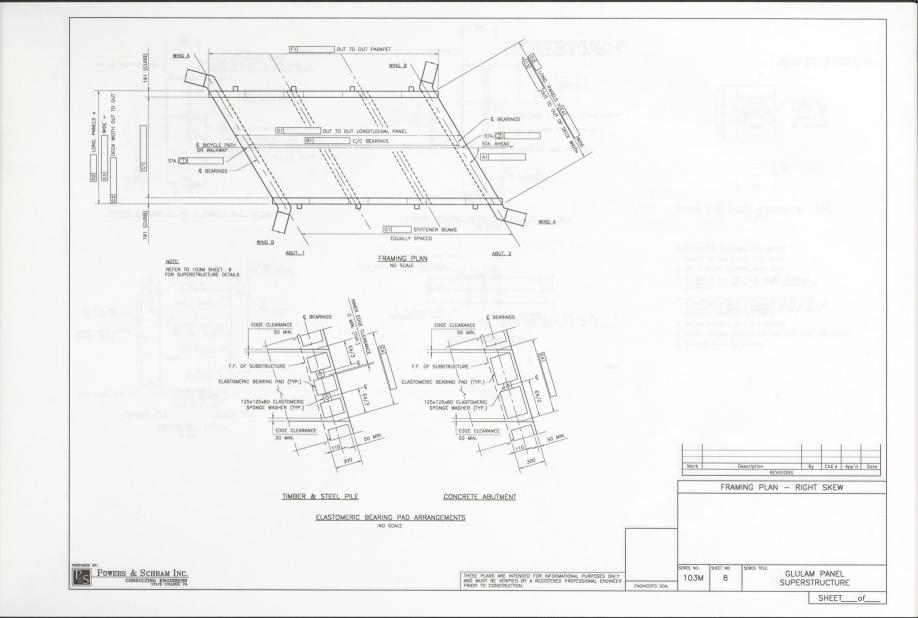
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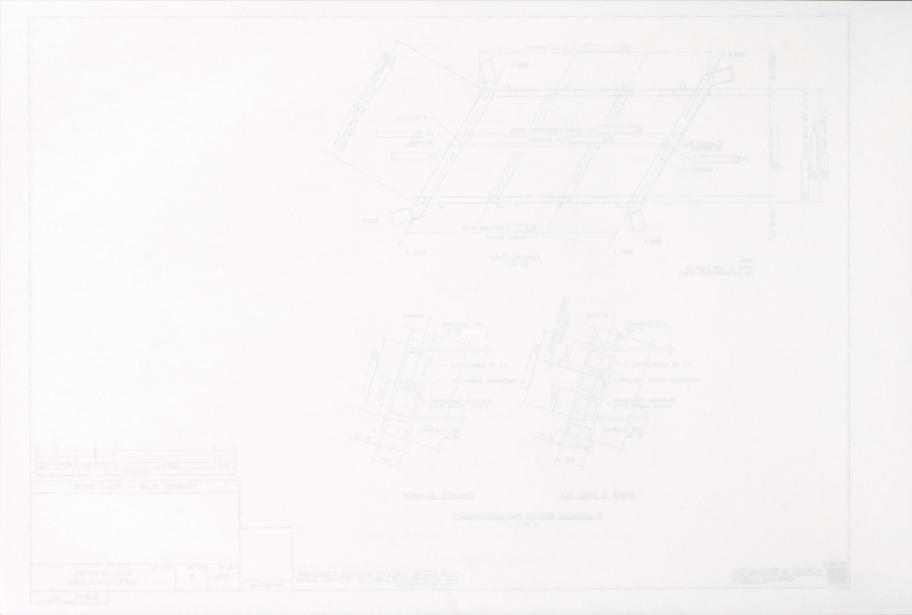


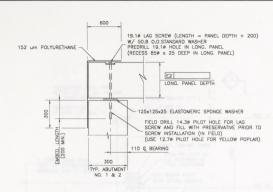




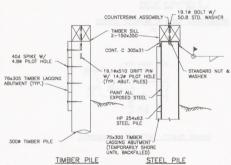




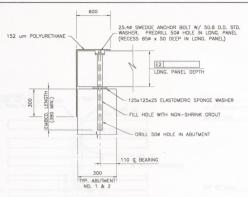




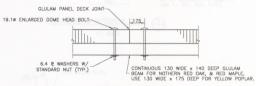
TYPICAL BEARING DETAIL - TIMBER SILL ABUTMENT
NO SCALE



TIMBER SILL DETAIL

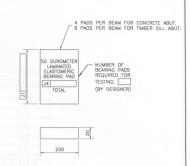


TYPICAL BEARING DETAIL - CONCRETE ABUTMENT
NO SCALE



STIFFENER BEAM DETAIL

NO SCALE



TYPICAL ELASTOMERIC BEARING PAD DETAIL
NO SCALE

# ELASTOMERIC BEARING PAD NOTES:

- 1. SMOOTH CUT AND DEBURR METAL SHIMS
- 2. GRIT BLAST AND DEGREASE METAL SHIMS.
- ALL BEARING PADS ARE TO BE MOLDED TO DESIGN DIMENSIONS. CUTTING TO SIZE AFTER FABRICATION IS PROHIBITED.
- MEET THE MATERIAL SPECIFICATION FOR ELASTOMERIC BEARING REQUIREMENTS OF CURRENT AASHTO (M-251-92 STANDARD SPECIFICATIONS BEARINGS) AS LISTED UNDER SUBSECTION "MATERIALS AND TESTING."
- 5. PROVIDE NEOPRENE 50 ± 5 DUROMETER.
- 6. PROVIDE INTERNAL SHIMS AS PER ASTM A570 GRADE 248 (36 KSI)
- 7. VULCANIZE PATCH PIN GROOVES.



SUPERSTRUCTURE DETAILS

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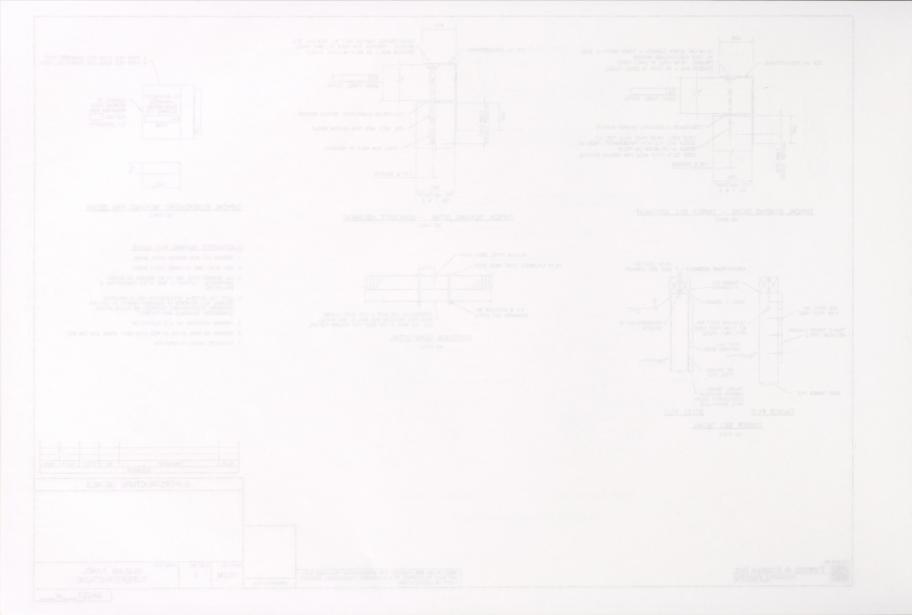
GLULAM PANEL SUPERSTRUCTURE

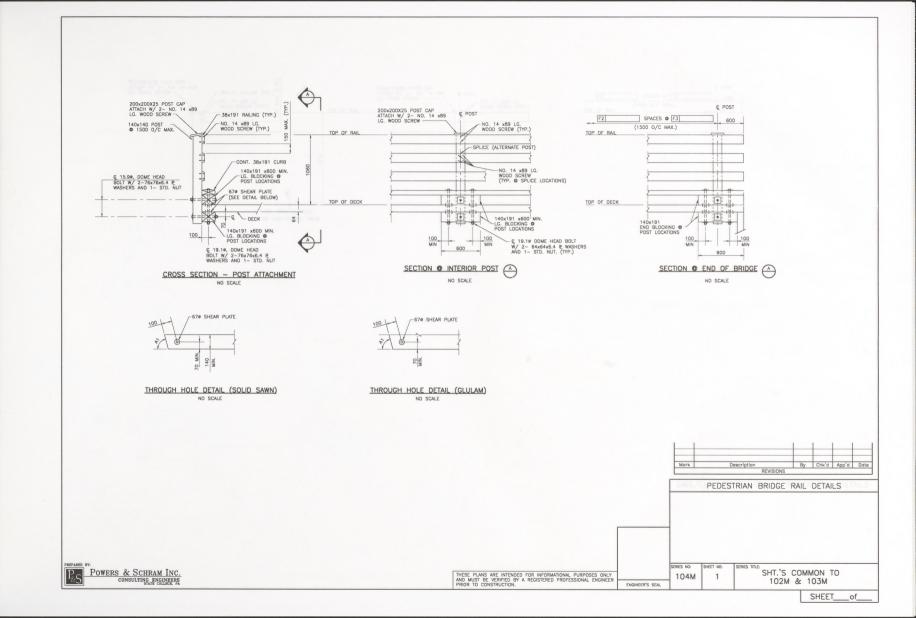
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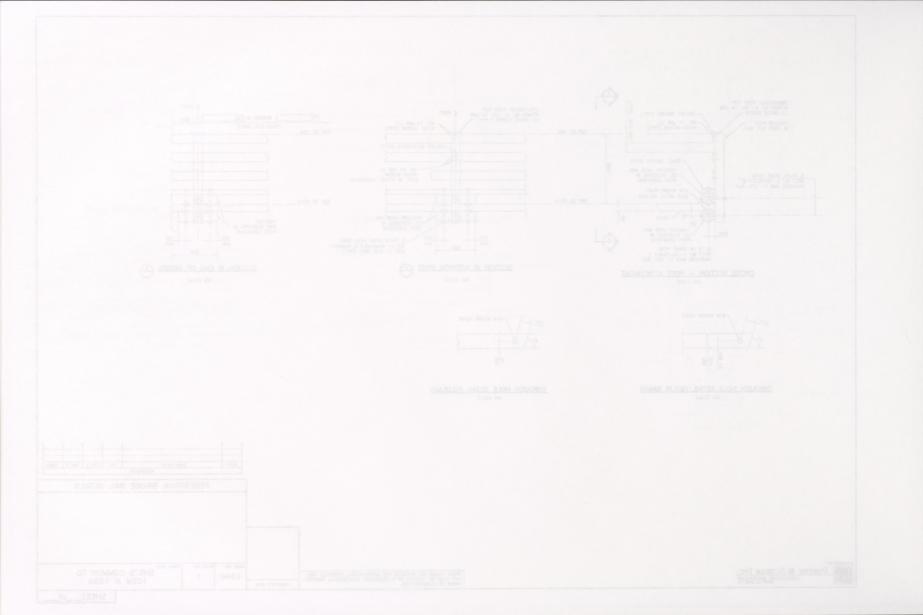
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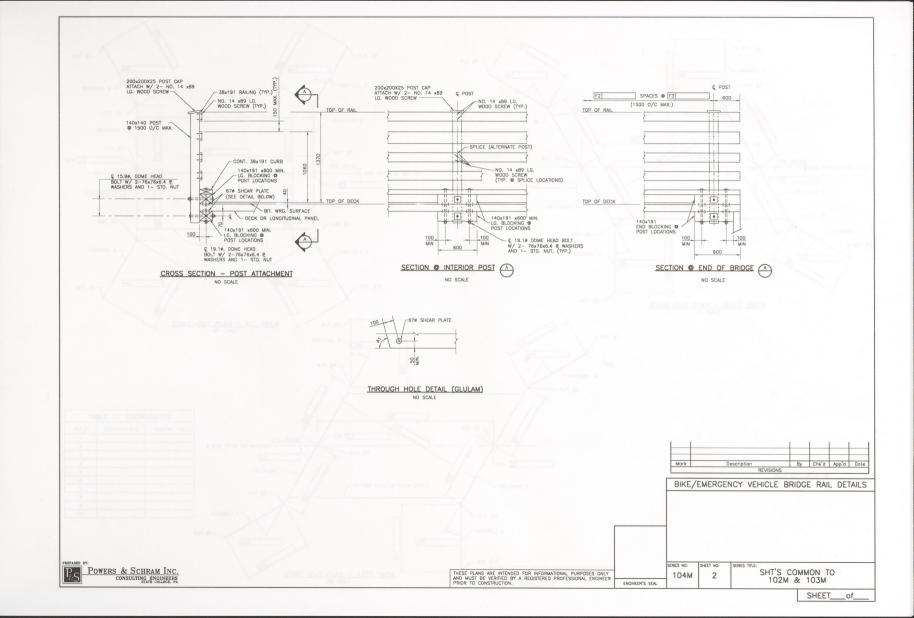
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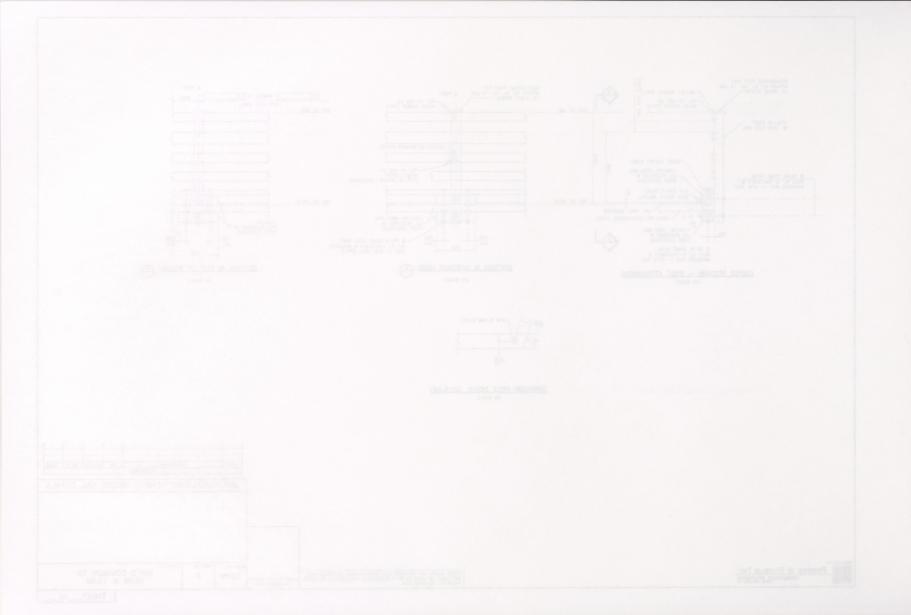
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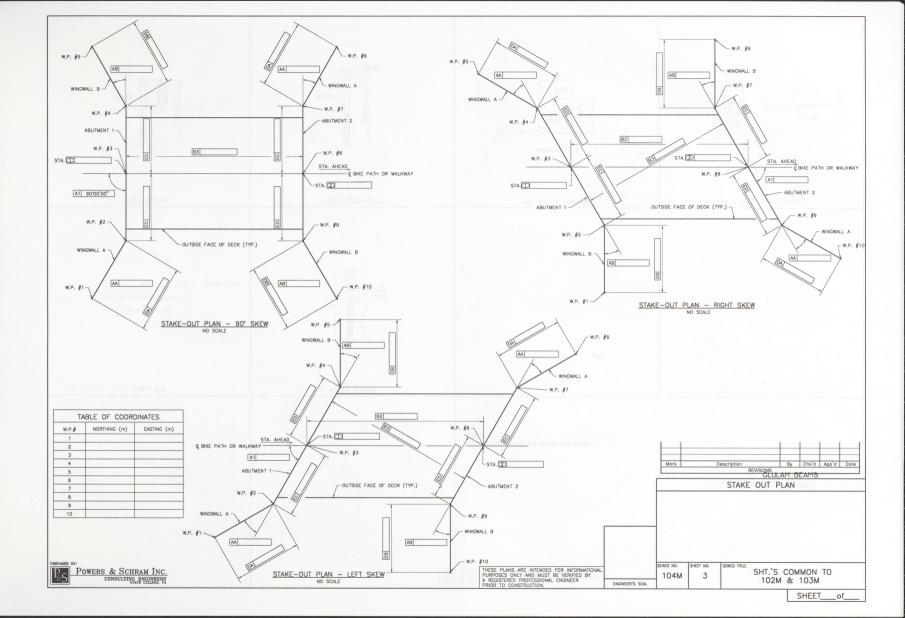


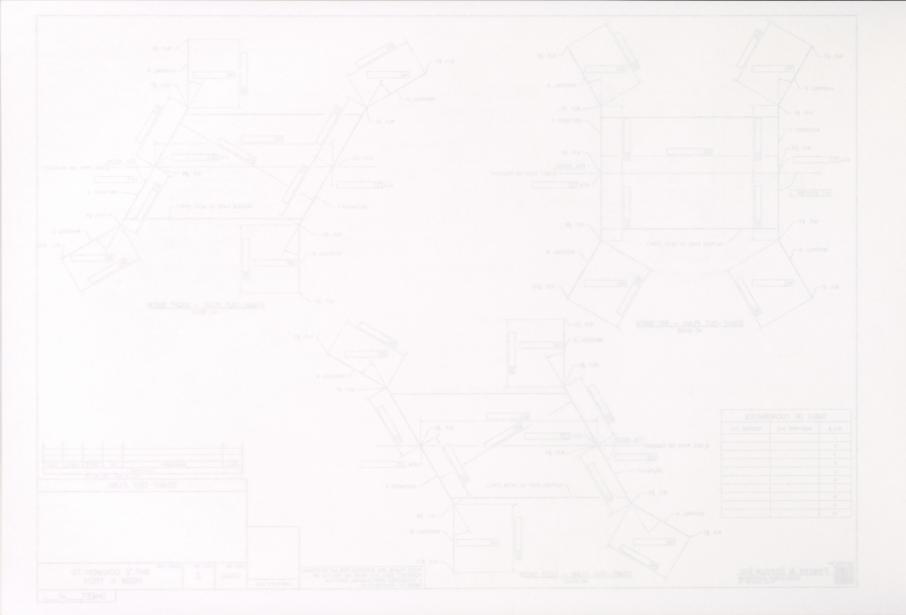


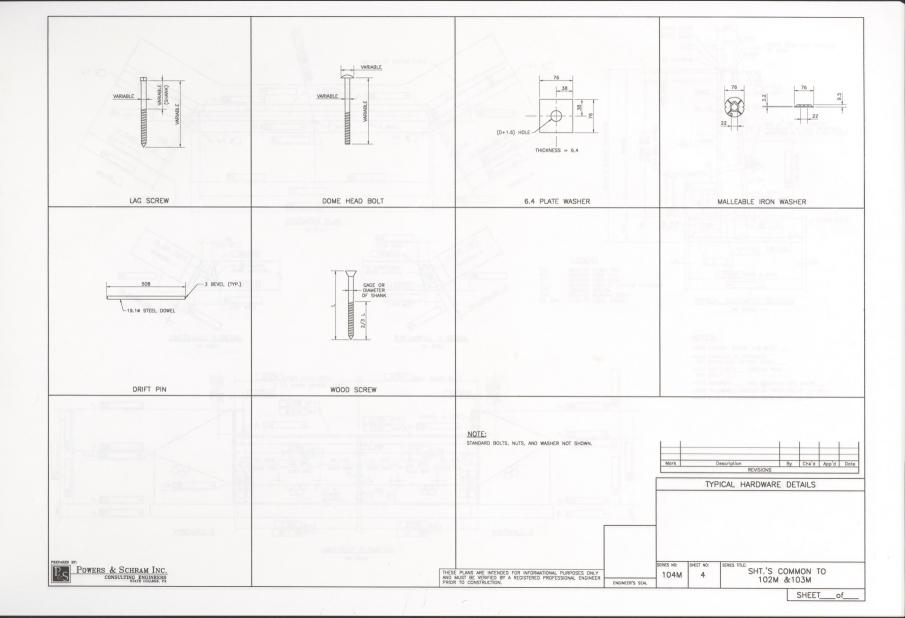


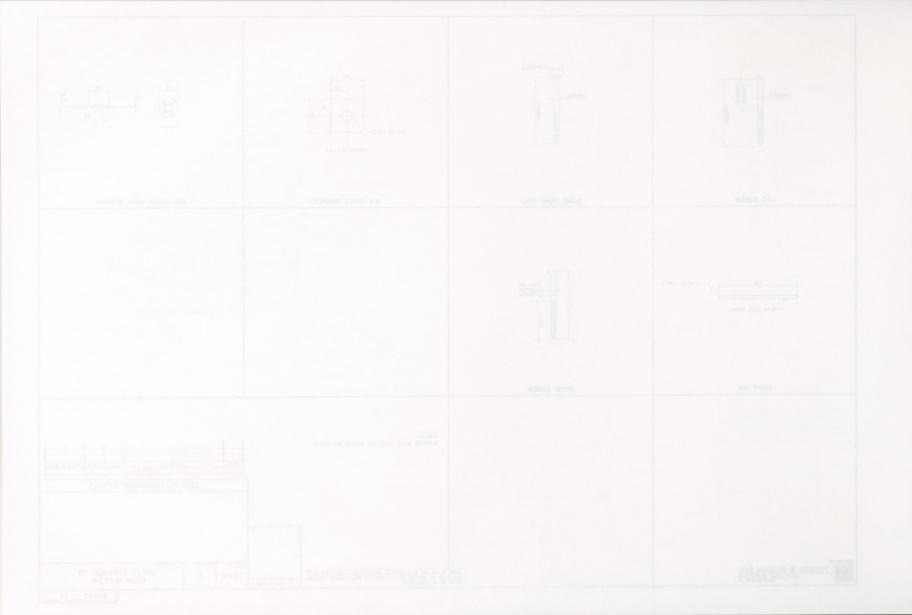


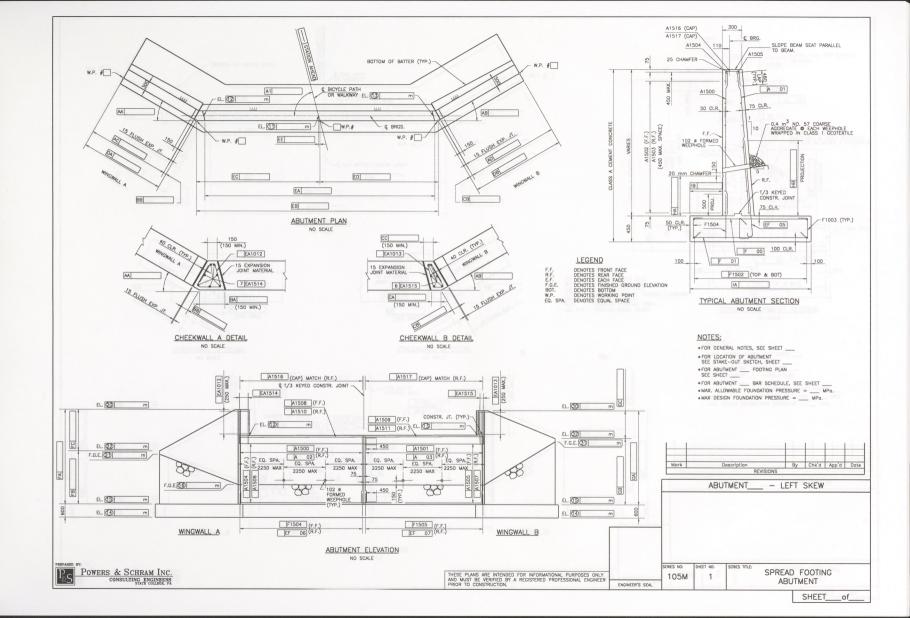


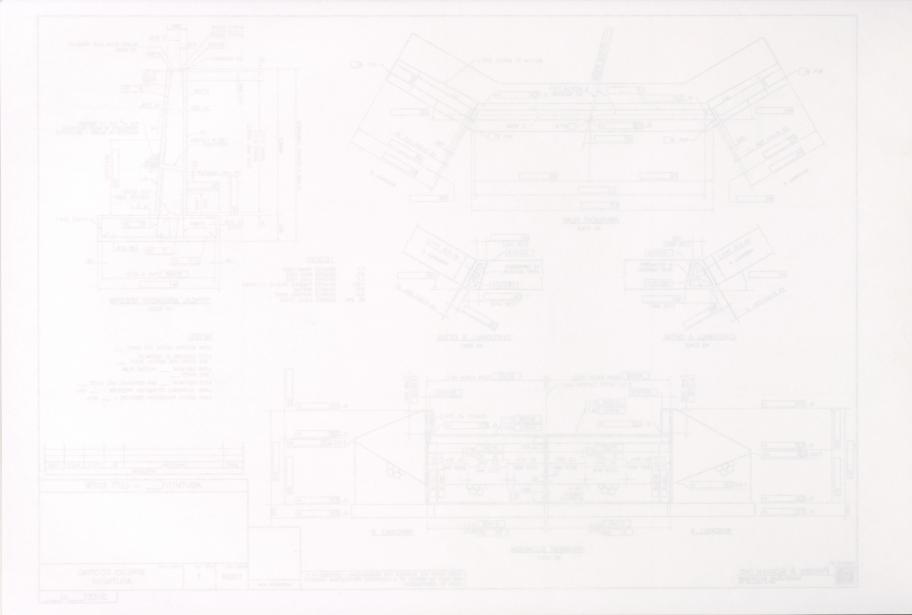


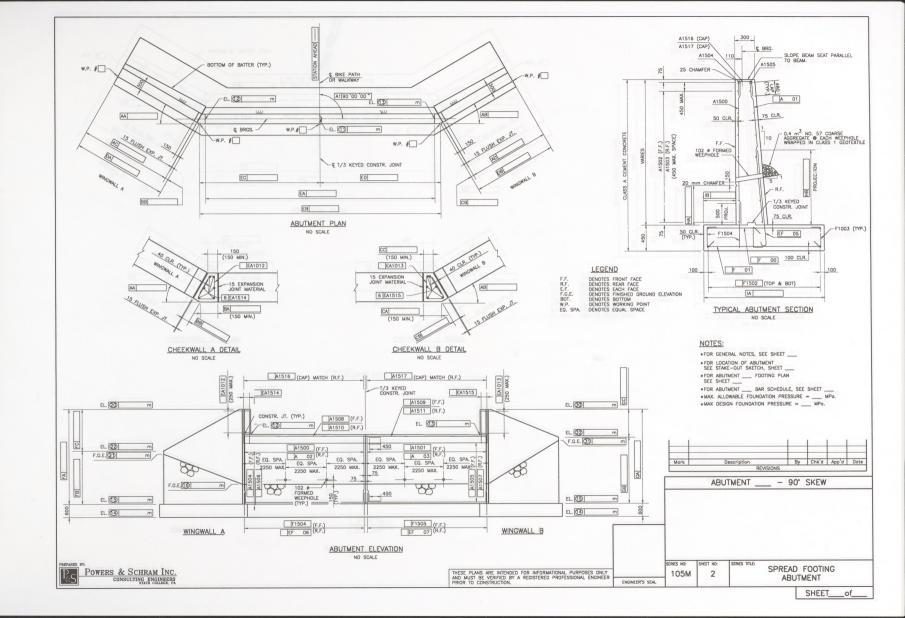


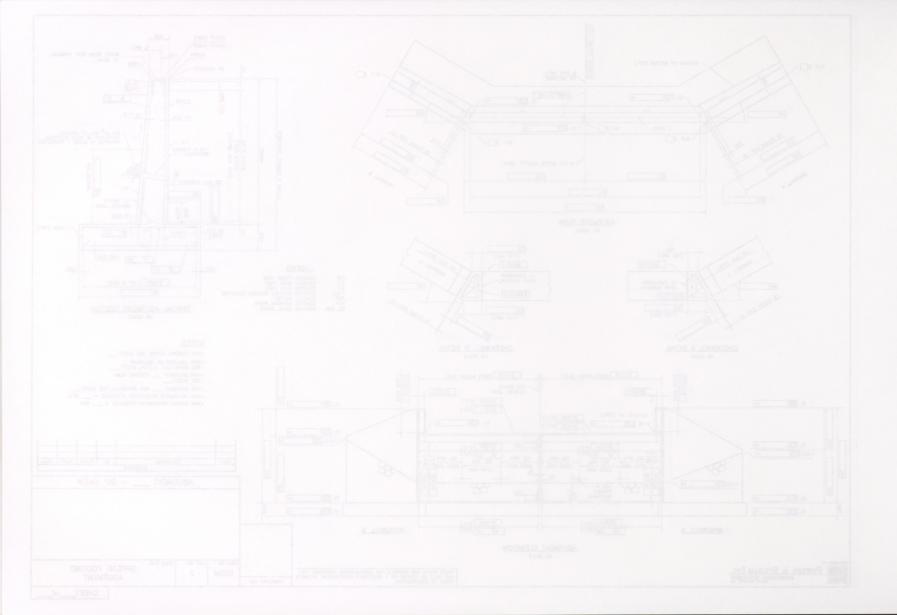


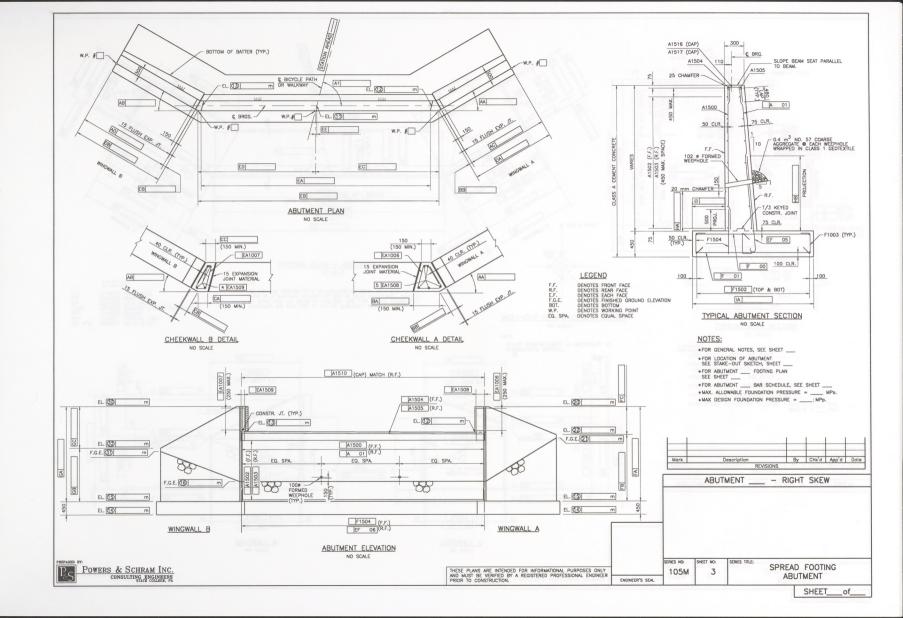


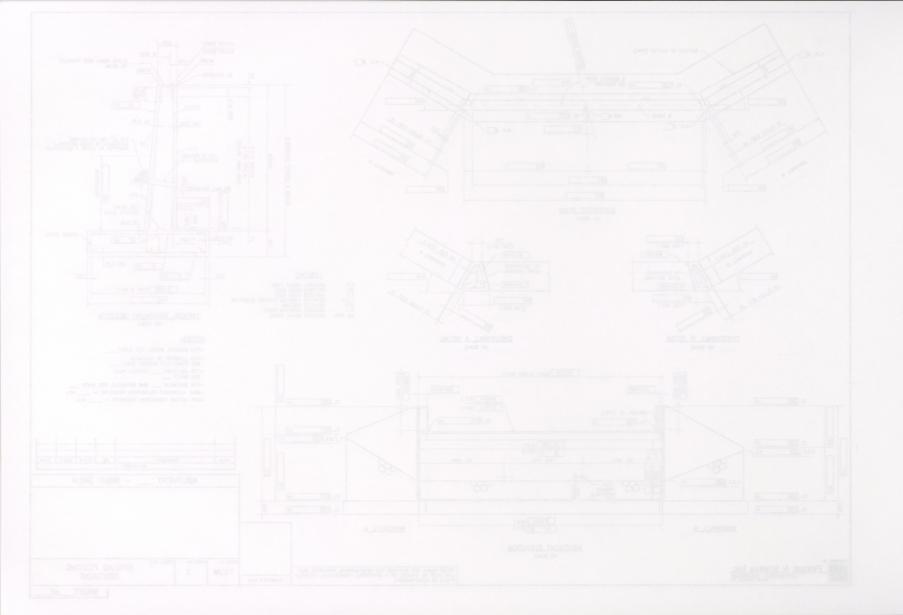


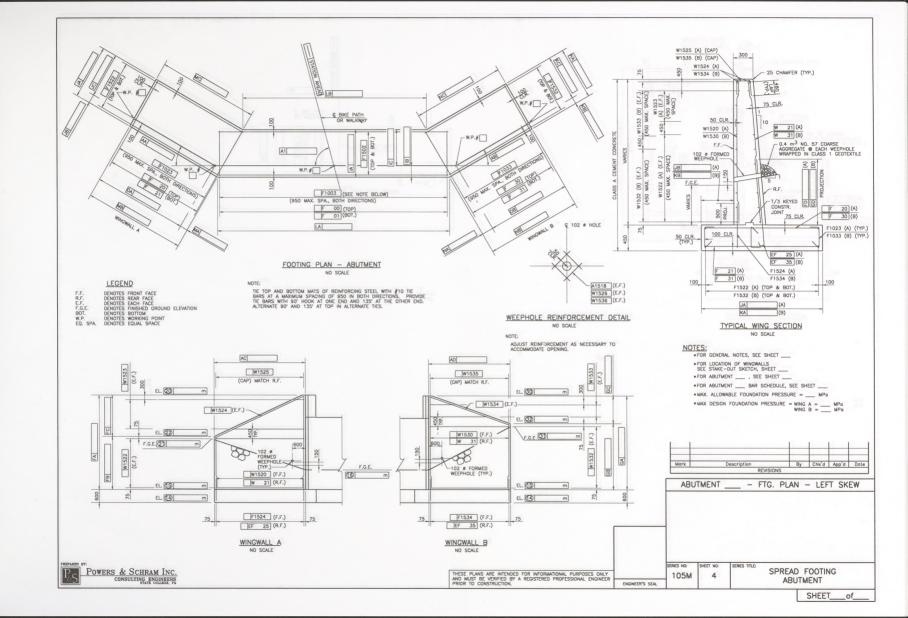


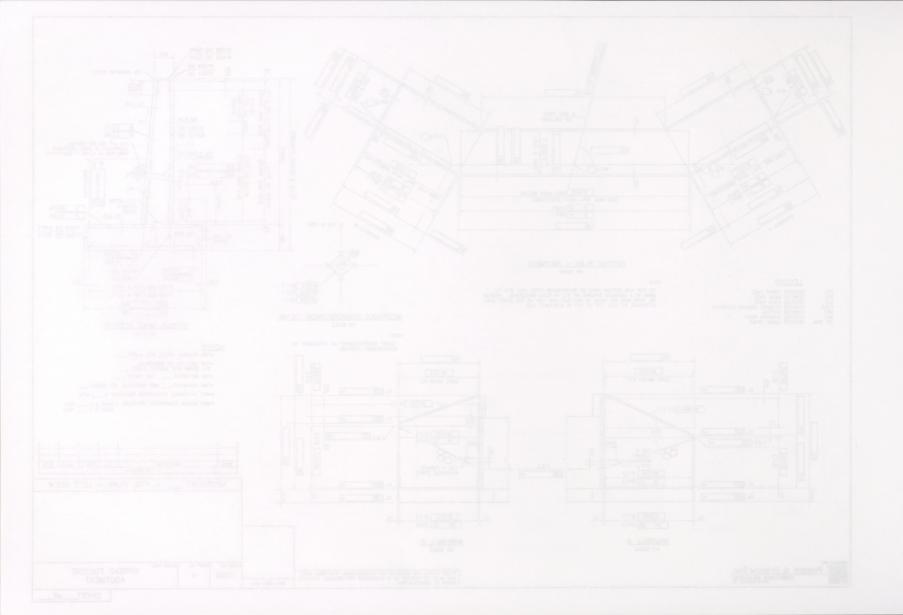


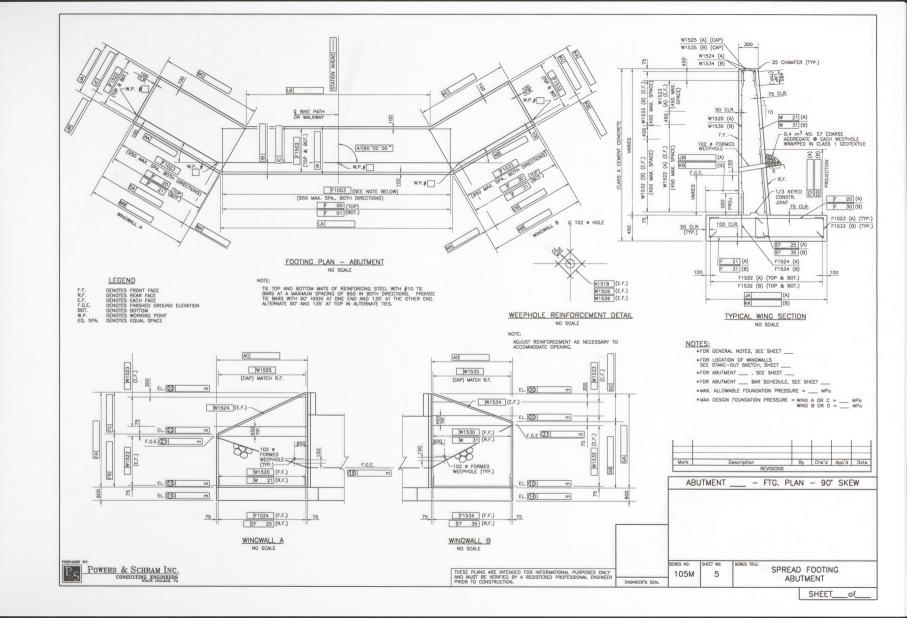


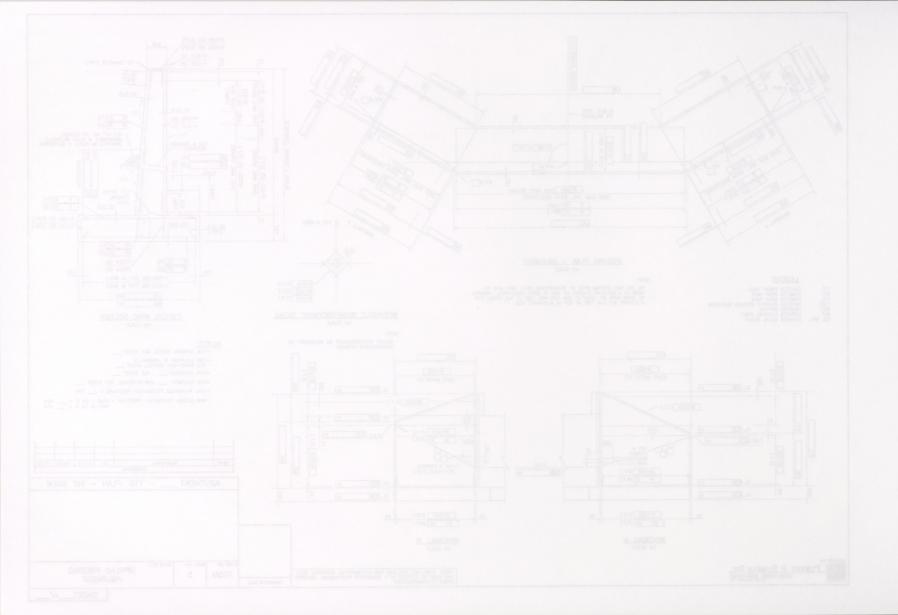


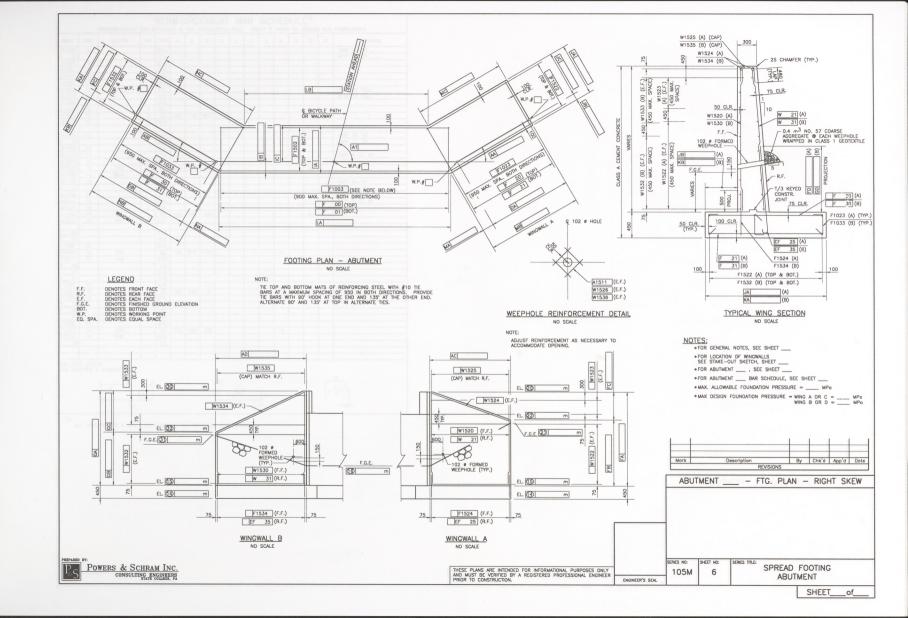


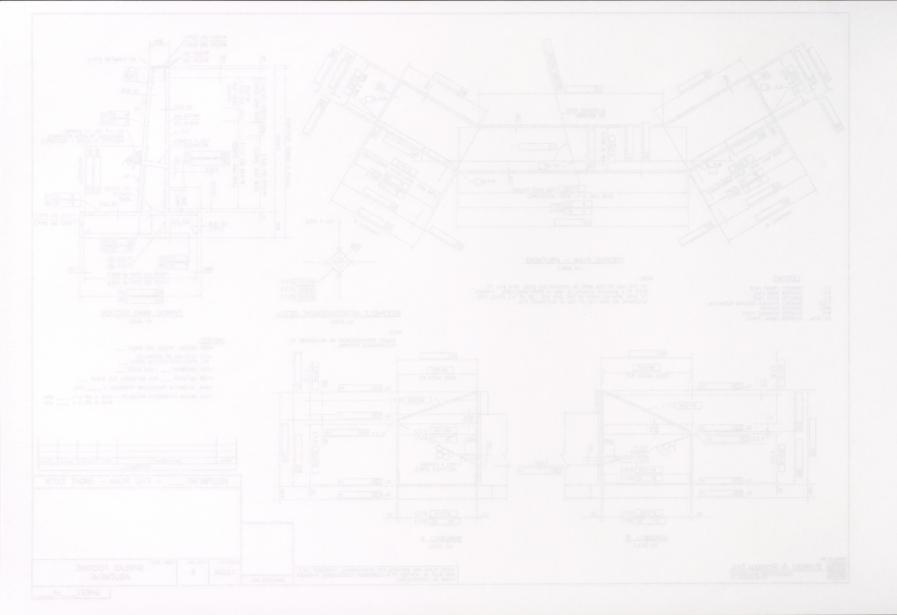












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		-		125	450	125					75				
15	900	-		-								-			
		+		_		_						-			
		+				-			-			-	-		
15		+		-					-	-		-	-	_	
	700	-		125	450	125		-	-	-	75	-			
15	900	+	STR.	123	730	123					/3				
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<sup>\*</sup> USE 101M SHEETS 7 AND 8 TO COMPLETE BAR SCHEDULE INFORMATION.

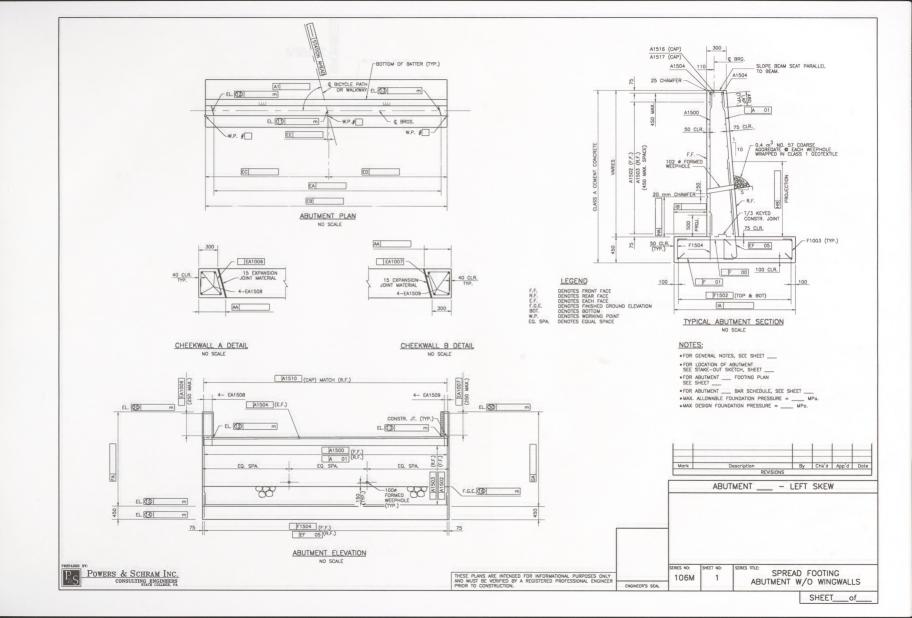
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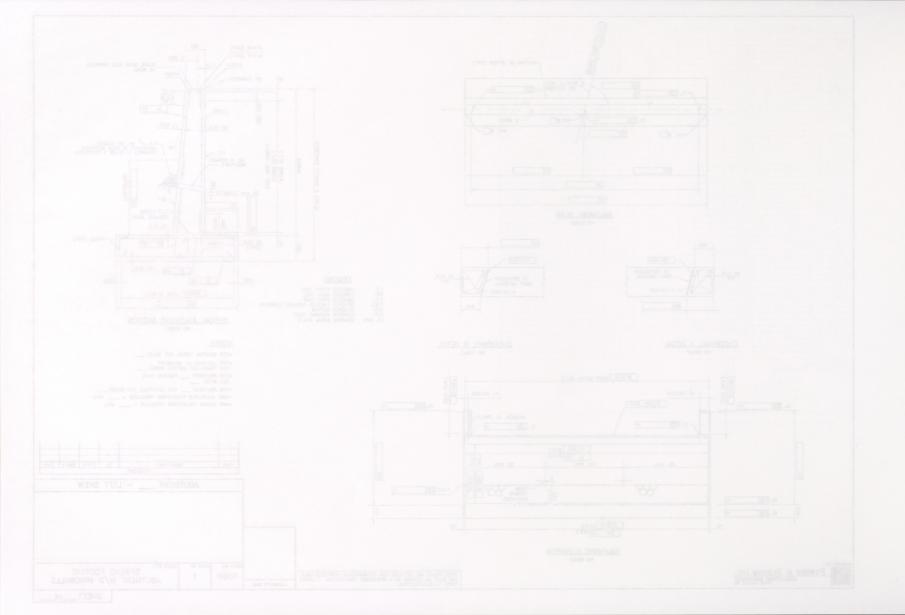
SERES NO: SERES NO: SERES ITLE: SPREAD FOOTING ABUTMENT

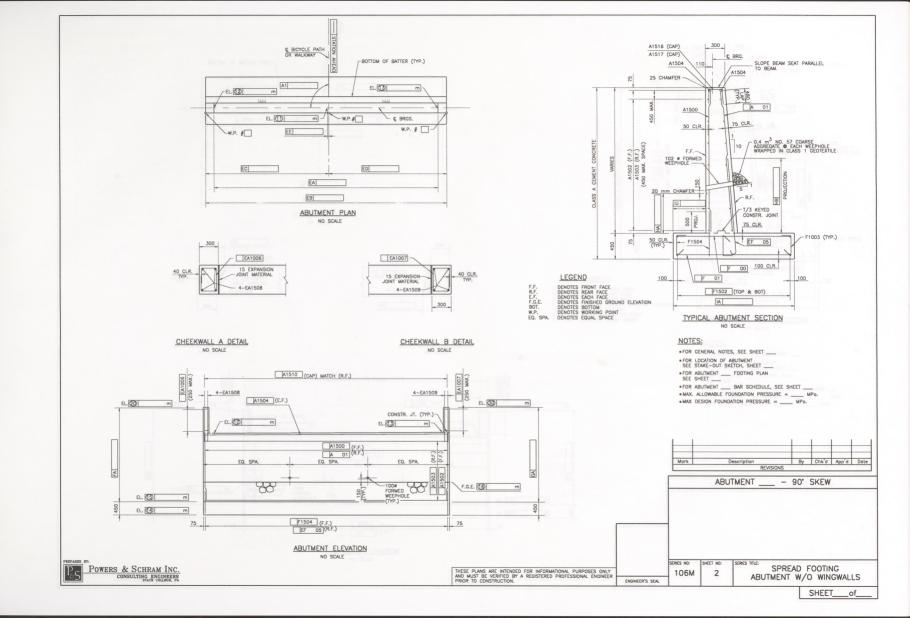
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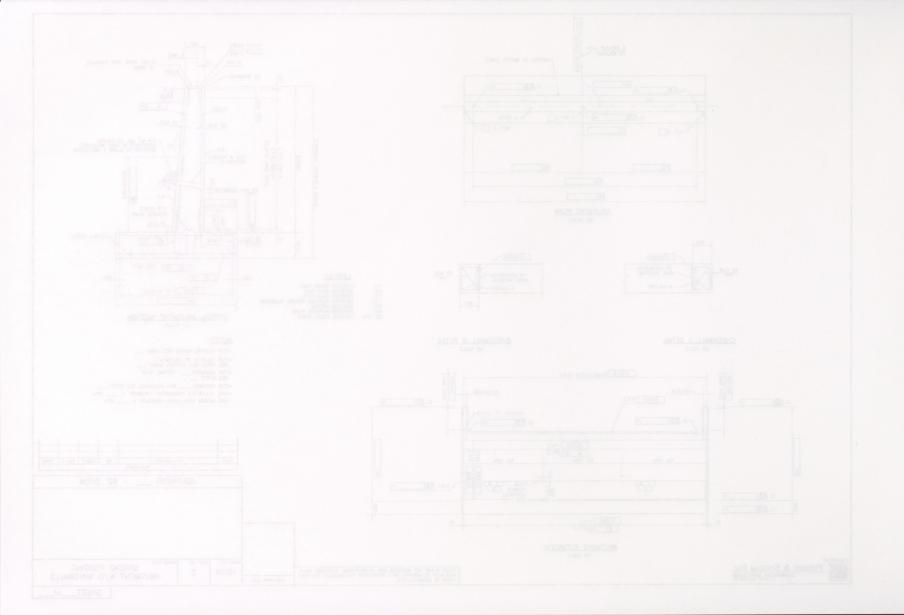
POWERS & SCHRAM INC.

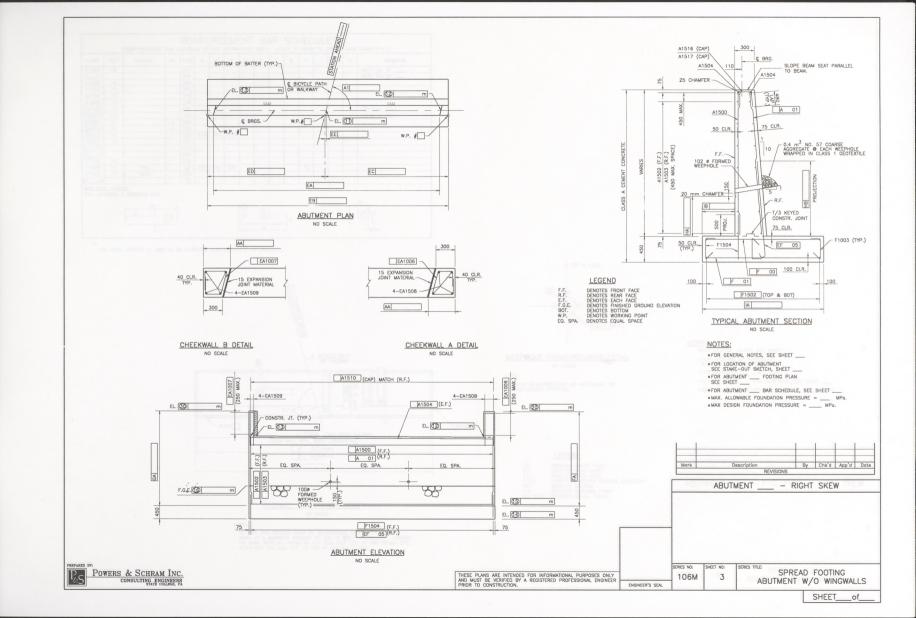
CONSULTING ENGINEERS
STATE COLLEGE, PA

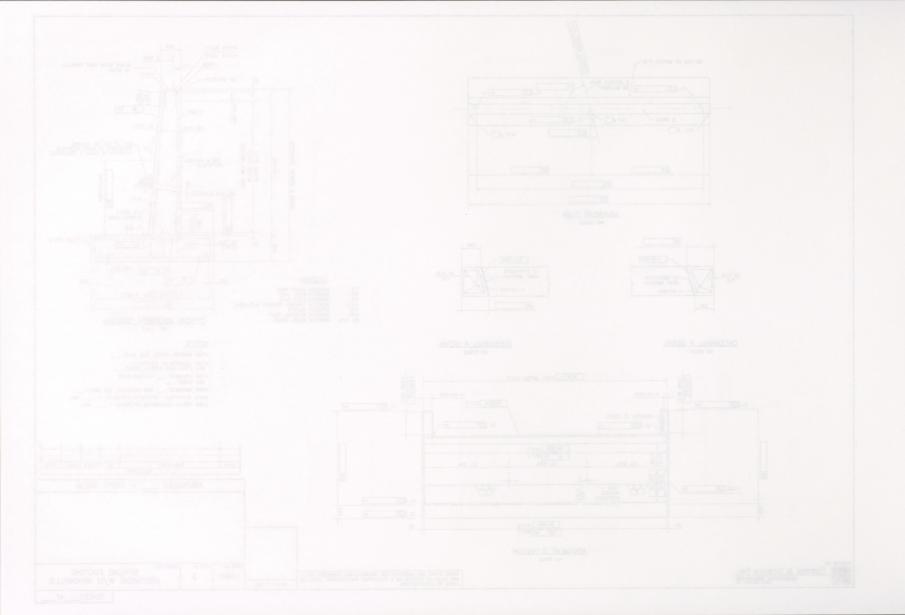






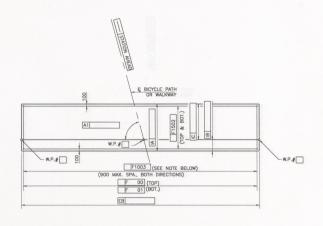






A1504 15 STR. A1504 15 STR. A1506 15 STR. A1606 10 STR. EA1006 10 STR. EA1007 10 STR. EA1508 15 4 STR. EA1509 15 4 STR.	VARY EA. BY
A1502 15 STR.  A1502 15 STR.  15 STR.  A1504 15 STR.  EA1006 10 STR.  STR.  EA1007 10 STR.  EA1007 10 STR.  EA1508 15 4 STR.  EA1509 15 4 STR.	VARY EA. BY
A1503 15 STR. A1504 15 STR. A1505 15 STR. EA1006 10 STR. EA1007 10 STR. EA1007 10 STR. EA1509 15 4 STR. EA1509 15 4 STR. EA1509 15 4 STR.	
A1504 15 STR. A1505 15 STR. EA1006 10 STR. EA1006 10 STR. EA1007 10 STR. EA1509 15 4 STR. EA1509 15 4 STR.	
A1505 15 STR.  EA1006 10 STR.  EA1007 10 STR.  EA1509 15 4 STR.  EA1509 15 4 STR.	
EA1006 10 STR. EA1007 10 STR. EA1007 10 STR. EA1508 15 4 STR. EA1509 15 4 STR.	
EA1007 10 STR. EA1508 15 4 STR. EA1509 15 4 STR.	
EA1508 15 4 STR. EA1509 15 4 STR.	BEND IN FIELD
EA1509 15 4 STR.	
A1510 15 3 400 325 400 40	
A1511 15 STR.	
F00 STR.	
F01 STR.	
F1502 15 STR.	
F1003 10 700 ② 125 450 125 75	
F1504 15 1050 STR.	
EF 06	

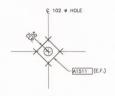
USE 101M SHEETS 11 AND 12 TO COMPLETE BAR SCHEDULE INFORMATION.



FOOTING PLAN - ABUTMENT NO SCALE

NOTE:

TIE TOP AND BOTTOM MATS OF REINFORCING STEEL WITH \$10 TIE BARS AT A MAXIMUM SPACING OF 950 IN BOTH DIRECTIONS. PROVIDE TIE BARS WITH 90" HOOK AT ONE END AND 135" AT THE OTHER END. ALTERNATE 90" AND 135" AT TOP IN ALTERNATE TIES.



## WEEPHOLE REINFORCEMENT DETAIL

NO SCALE

ADJUST REINFORCEMENT AS NECESSARY TO ACCOMMODATE OPENING.

# NOTES:

- . FOR GENERAL NOTES, SEE SHEET \_\_\_\_
- •FOR LOCATION OF WINGWALLS SEE STAKE-OUT SKETCH, SHEET \_\_\_\_
- FOR ABUTMENT \_\_\_ , SEE SHEET \_\_\_
- FOR ABUTMENT \_\_\_ BAR SCHEDULE, SEE SHEET \_\_\_
- MAX. ALLOWABLE FOUNDATION PRESSURE = \_\_\_\_ MPa

LEGEND

F.F. DENOTES FRONT FACE
R.F. DENOTES REAR FACE
ENOTES EACH FACE
F.G.E. DENOTES SENT FACE
BOT. DENOTES SHORT
W.P. DENOTES BOTTOM
M.P. DENOTES BOTTOM
DENOTES BOTTOM
DENOTES BOTTOM
DENOTES BOTTOM
DENOTES BOTTOM
DENOTES COLUM

Mark By Chk'd App'd Date

ABUTMENT \_\_\_ - FTG. PLAN - LEFT SKEW

SERIES NO: SHEET NO: 106M

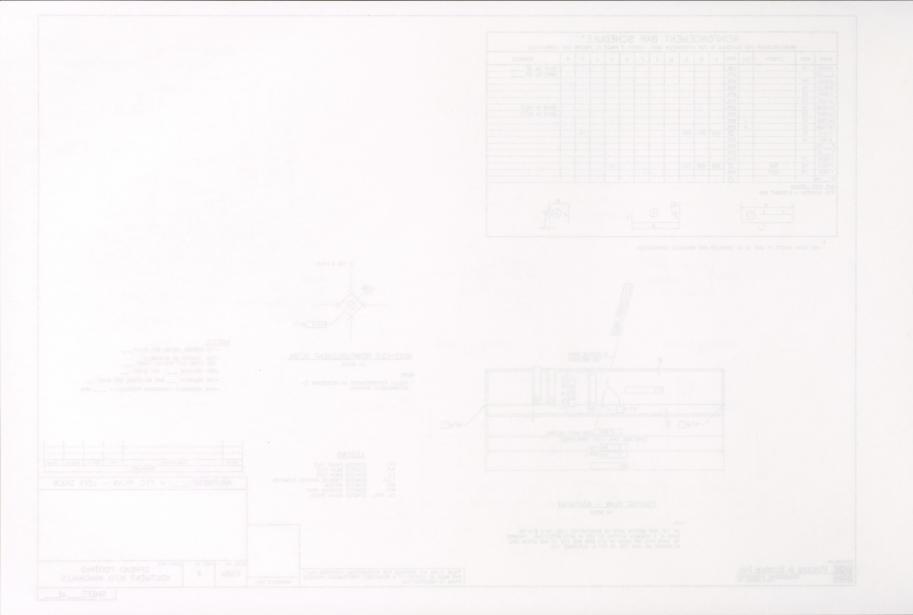
ENGINEER'S SEAL

SPREAD FOOTING
ABUTMENT W/O WINGWALLS

SHEET \_of\_

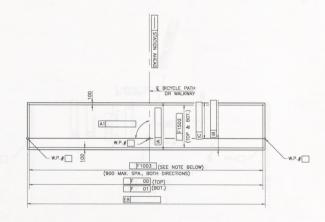


THESE PLANS ARE INTENDED FOR INFORMATIONAL PURPOSES ONLY AND MUST BE VERIFIED BY A REGISTERED PROFESSIONAL ENGINEER PRIOR TO CONSTRUCTION.



	SIZE	LENGTH	NO.	TYPE	Α	В	С	D .	E	F	G	н	J	К	R	REMARKS
A1500	15			STR.												VARY EAL BY
A01				STR.												VARY EA. BY
A1502	15			STR.												
A1503	15			STR.												
A1504	15			STR.												
A1505	15			STR.												
EA1006	10			STR.												BEND IN FIELD
EA1007	10			STR.												BEND IN FIELD
EA1508	15		4	STR.												
EA1509	15		4	STR.					1							
A1510	15			3	400	325	400							40		
A1511	15			STR.												
F00				STR.												
F01				STR.												
F1502	15			STR.												
F1003	10	700		2	125	450	125					75				
F1504	15	1050		STR.												
F 06				0												

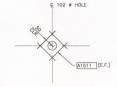
USE 101M SHEETS 11 AND 12 TO COMPLETE BAR SCHEDULE INFORMATION.



FOOTING PLAN - ABUTMENT
NO SCALE

NOTE:

TIE TOP AND BOTTOM MATS OF REINFORCING STEEL WITH ∯10 TIE BARS AT A MAXIMUM SPACING OF 950 IN BOTH DIRECTIONS. PROVIDE TIE BARS WITH 90" HOOK AT ONE END AND 135" AT THE OTHER END. ALTERNATE 90" AND 135" AT TOP IN ALTERNATE TIES.



WEEPHOLE REINFORCEMENT DETAIL

NO SCALE

TF.

ADJUST REINFORCEMENT AS NECESSARY TO ACCOMMODATE OPENING.

### NOTES:

FOR GENERAL NOTES, SEE SHEET \_\_\_\_

•FOR LOCATION OF WINGWALLS SEE STAKE-OUT SKETCH, SHEET

FOR ABUTMENT \_\_\_\_ , SEE SHEET \_\_\_\_

FOR ABUTMENT \_\_\_ BAR SCHEDULE, SEE SHEET \_\_\_

• MAX. ALLOWABLE FOUNDATION PRESSURE = \_\_\_\_ MPa

### LEGEND

F.F. DENOTES FRONT FACE
R.F. DENOTES REAR FACE
E.F. DENOTES REAH FACE
F.G.E. DENOTES SHOWNED
BOT: DENOTES SHISHED GROUND ELEVATION
BOT: DENOTES BOTTOM
W.P. DENOTES BOTTOM
DENOTES WORKING POINT
EG. SPA. DENOTES EQUAL SPACE

Mork Description By Child App'd Date
REVISIONS

ABUTMENT \_\_\_ - FTG. PLAN - 90° SKEW

ABOTMENT \_\_\_ - FIG. PLAN - 90 SKEW

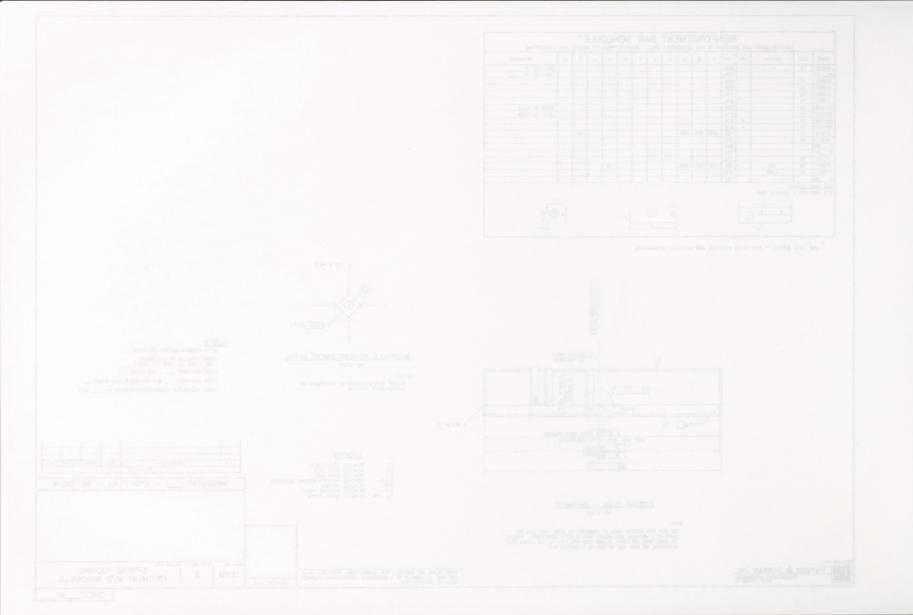
THESE PLANS ARE INTENDED FOR INFORMATIONAL PURPOSES ONLY AND MUST BE VERIFIED BY A REGISTERED PROFESSIONAL ENGINEER PRIOR TO CONSTRUCTION.

SERIES NO: SHEET NO: 5

SPREAD FOOTING
ABUTMENT W/O WINGWALLS

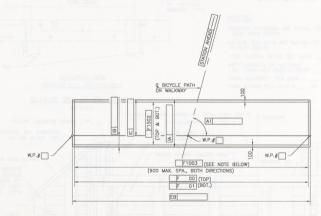
SHEET\_\_\_of\_\_

POWERS & SCHRAM INC.
CONSULTING ENGINEERS
STATE COLLEGE, PA



MARK	SIZE	LENGTH	NO.	TYPE	Α	В	C	D	E	F	G	Н	J	K	R	REMARKS
A1500	15			STR.				100	.89.							VARY EA. BY
A01				STR.	1											VARY EA. BY
A1502	15			STR.						-						
A1503	15			STR.					100							
A1504	15			STR.		/		W	3							
A1505	15			STR.				0.37			300					
FA1006	10			STR.	TA				139	1					0	BEND IN FIELD
EA1007	10			STR.		1				-			7.	. 2		BEND IN FIELD
EA1508	15		4	STR.		110	1		-			1				
EA1509	15		4	STR.				444								
A1510	15			(3)	400	325	400							40		
A1511	15			STR.				1								The second secon
F 00				STR.	77		1	100					1767			
F01				STR.	100	100										
F1502	15			STR.		100				7						
F1003	10	700			125	450	125					75				
F1504	15	1050		STR.	-	-										
F 06			1	(1)												
		STRAIGHT BAR	0					4	2		Jc				-	3 6

USE 101M SHEETS 11 AND 12 TO COMPLETE BAR SCHEDULE INFORMATION.



FOOTING PLAN - ABUTMENT

NO SCALE

TIE TOP AND BOTTOM MATS OF REINFORGING STEEL WITH #10 TIE BARS AT A MAXIMUM SPACING OF 950 IN BOTH DIRECTIONS. PROVIDE TIE BARS WITH 90' HOOK AT ONE BND AND 135' AT THE OTHER END. ALTERNATE 90' AND 135' AT TOP IN ALTERNATE TIES. DECK WING CITATO

€ 102 # HOLE

WEEPHOLE REINFORCEMENT DETAIL

NO SCALE

re.

ADJUST REINFORCEMENT AS NECESSARY TO ACCOMMODATE OPENING. NOTES:

FOR GENERAL NOTES, SEE SHEET

• FOR LOCATION OF WINGWALLS SEE STAKE-OUT SKETCH, SHEET

• FOR ABUTMENT \_\_\_\_ , SEE SHEET \_\_\_\_

•FOR ABUTMENT \_\_\_ BAR SCHEDULE, SEE SHEET \_\_\_

• MAX. ALLOWABLE FOUNDATION PRESSURE = \_\_\_\_ MPa

ENGINEER'S SEAL

F.F. DENOTES FRONT FACE
R.F. DENOTES REAR FACE
E.F. DENOTES MATERIAL FACE
F.G.E. DENOTES SHORT FACE
F.G.E. DENOTES SHORT FACE
OF DENOTES SHORT FACE
W.P. DENOTES WORKING POINT
E.G. SPA. DENOTES WORKING SPACE

Mark Description By Chi'd App'd Date REVISIONS

ABUTMENT \_\_\_ - FTG. PLAN - RIGHT SKEW

ADDIWENT \_\_\_\_ TO. TEAN - RIGHT SKEW

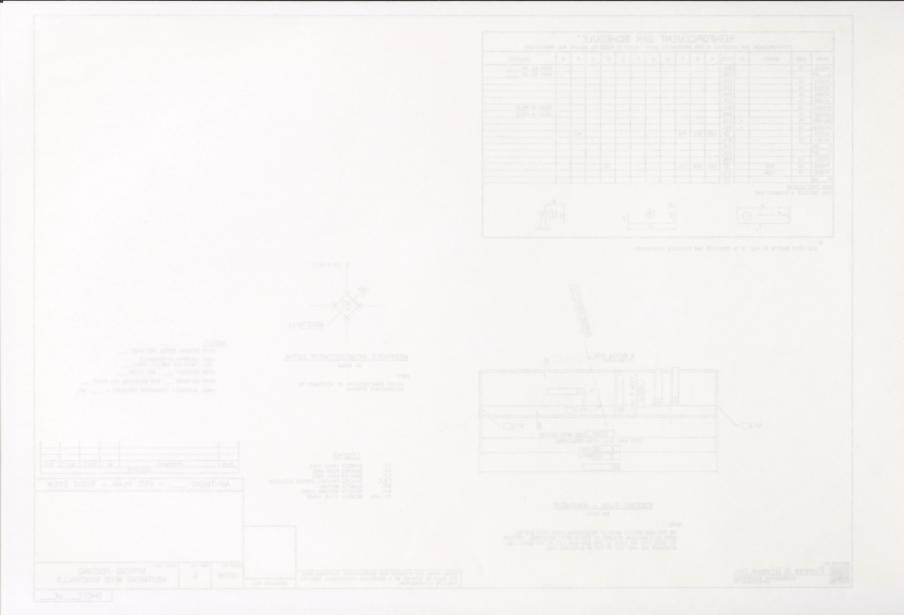
ERIES NO: SHEET NO:

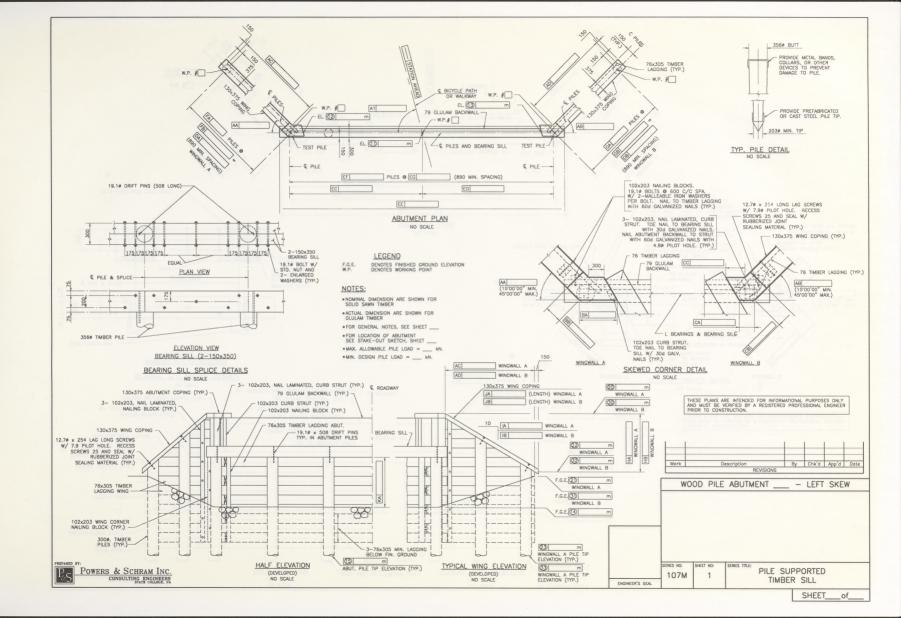
SPREAD FOOTING
ABUTMENT W/O WINGWALLS

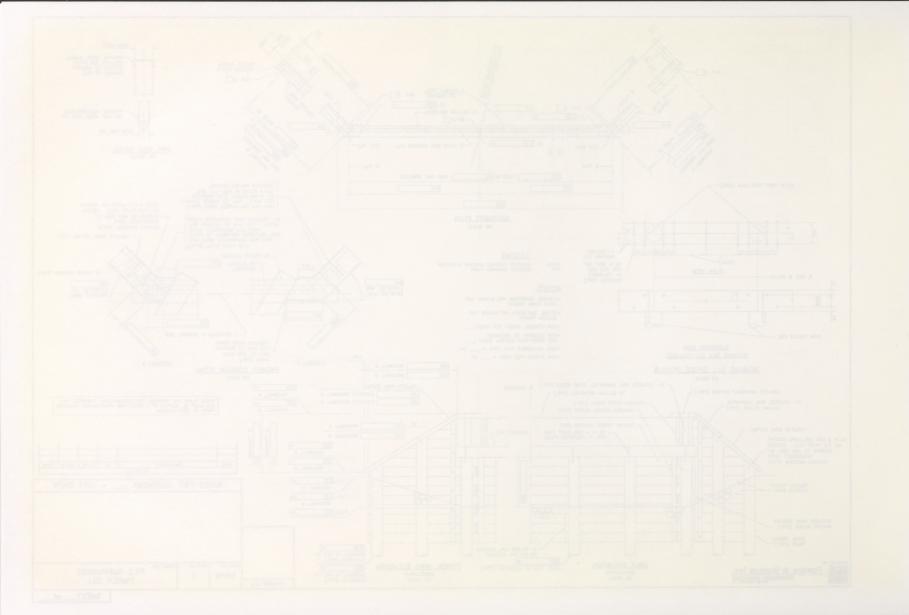
SHEET\_\_\_of\_\_

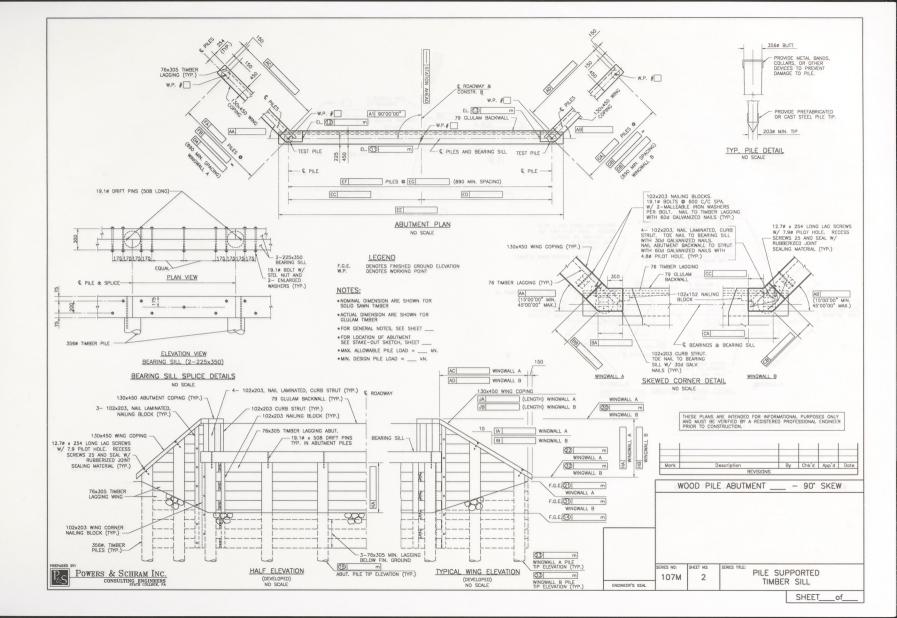


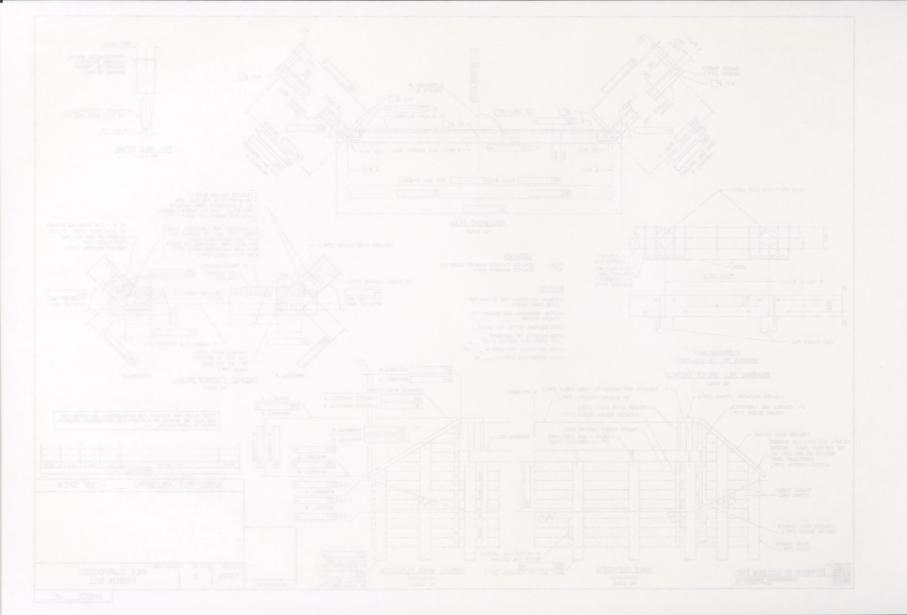
THESE PLANS ARE INTENDED FOR INFORMATIONAL PURPOSES ONLY AND MUST BE VERIFIED BY A REGISTERED PROFESSIONAL ENGINEER PRIOR TO CONSTRUCTION.

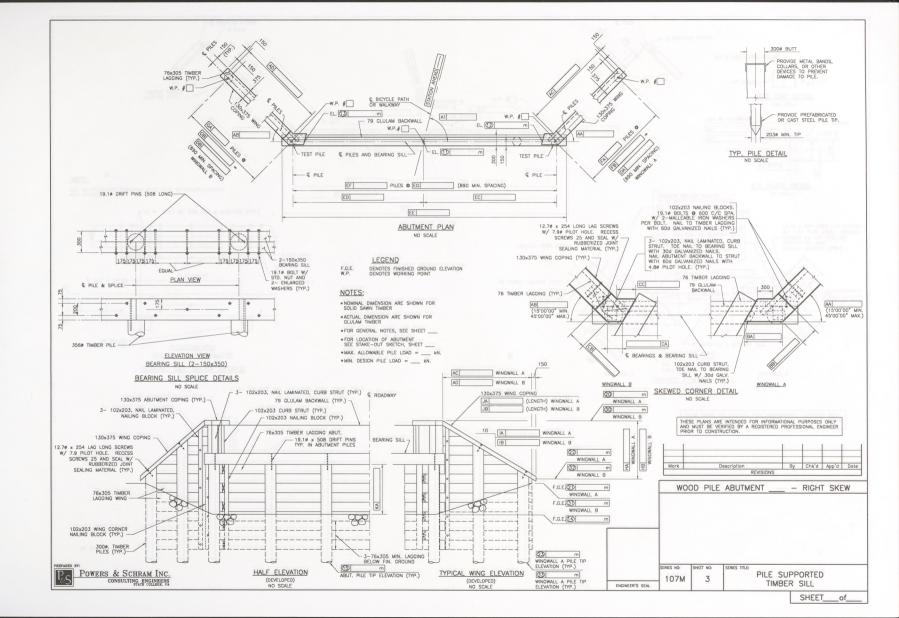


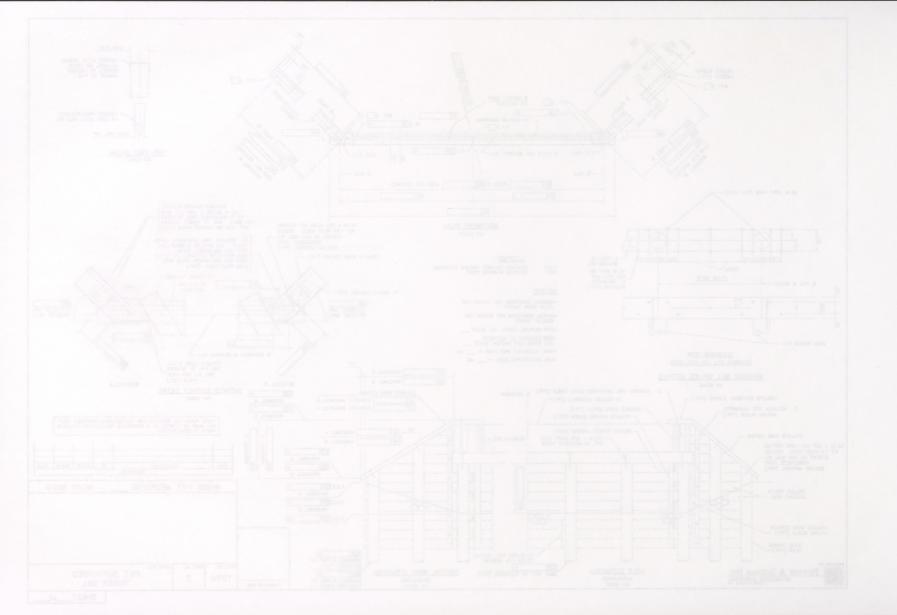


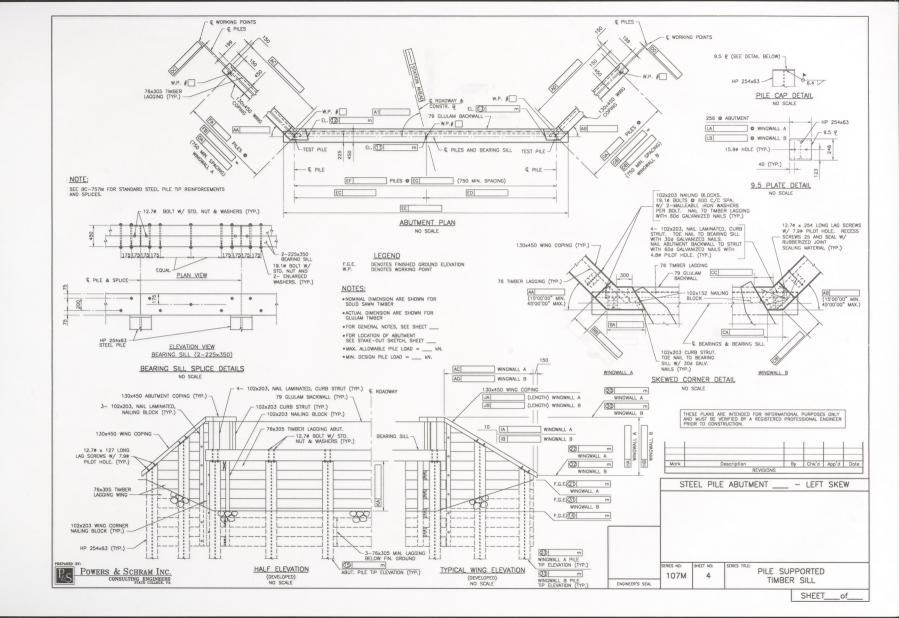


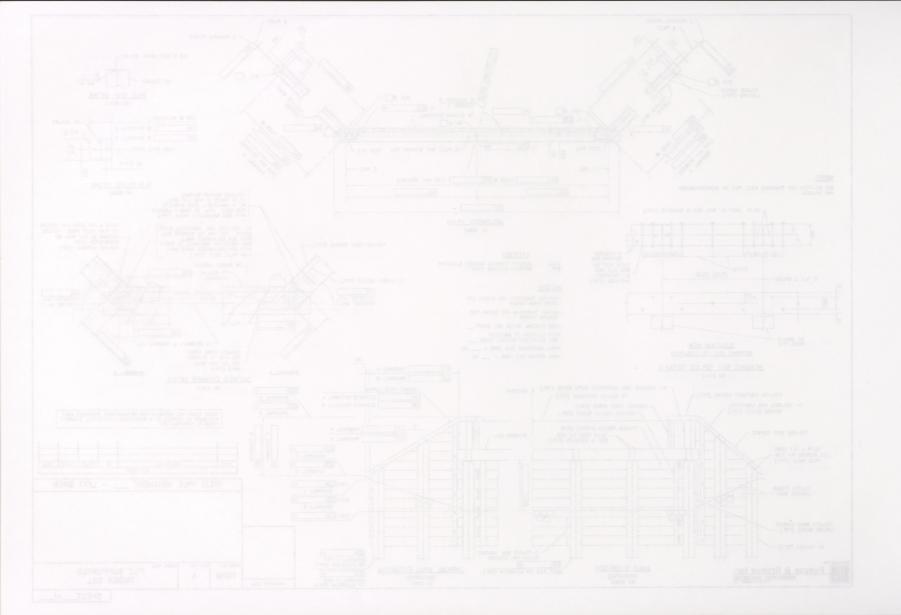


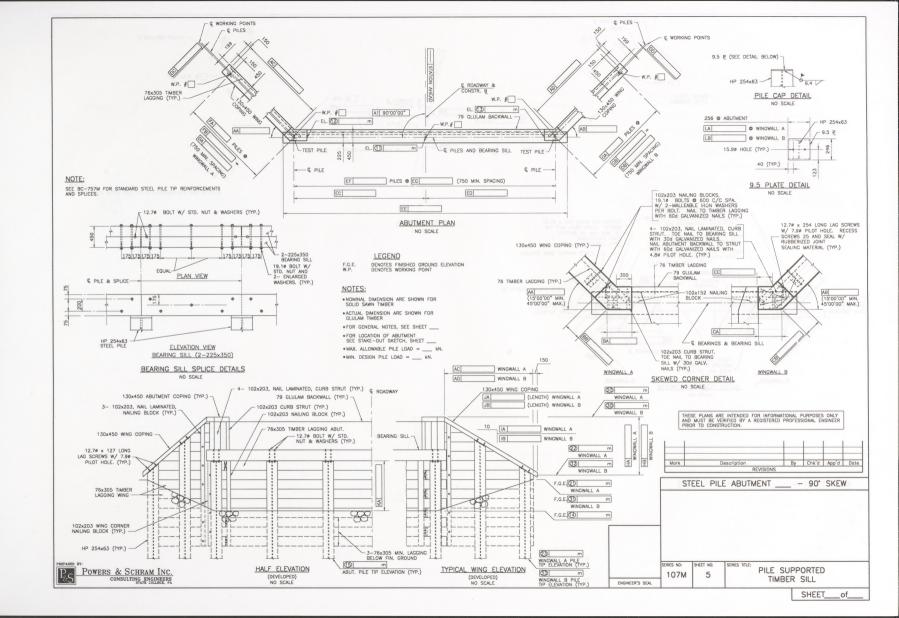


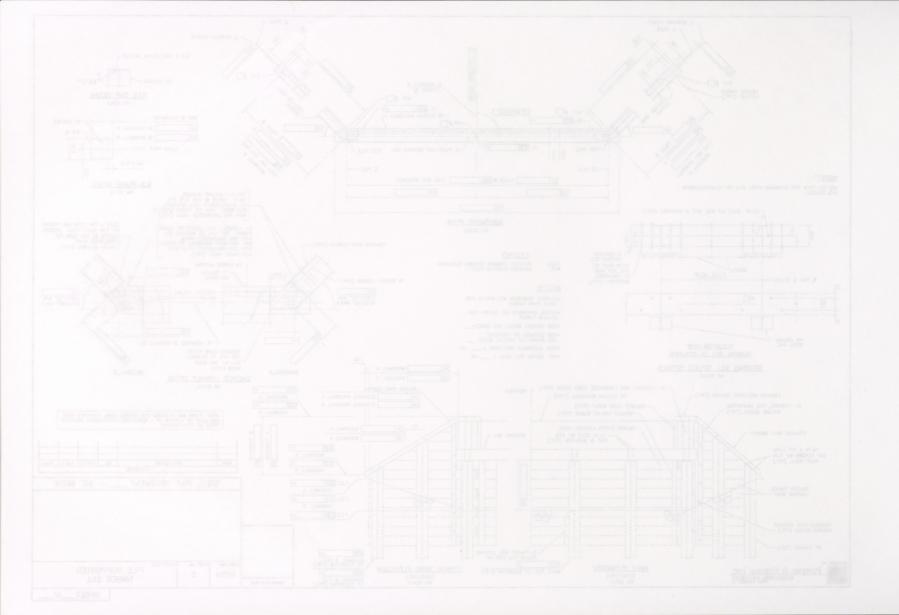


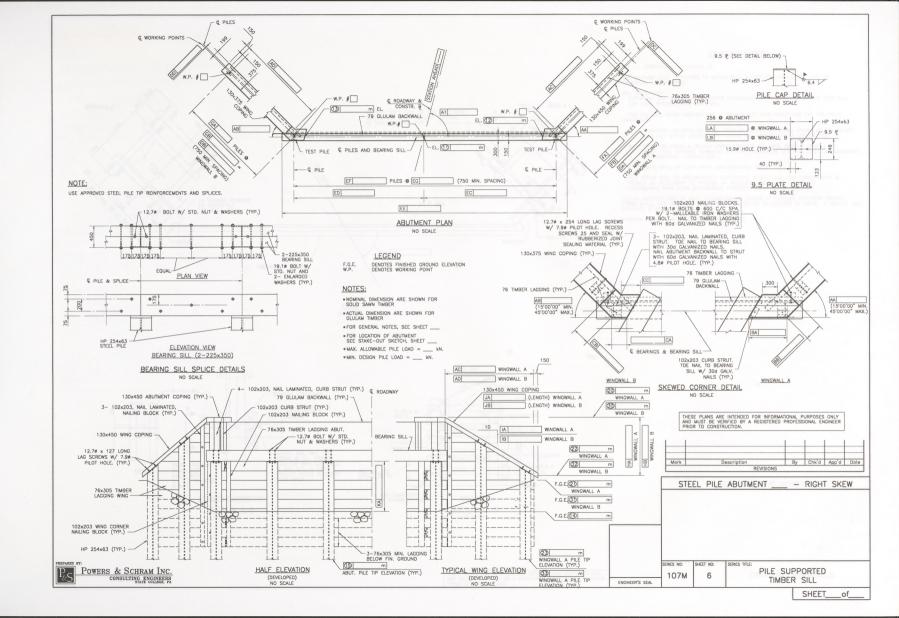


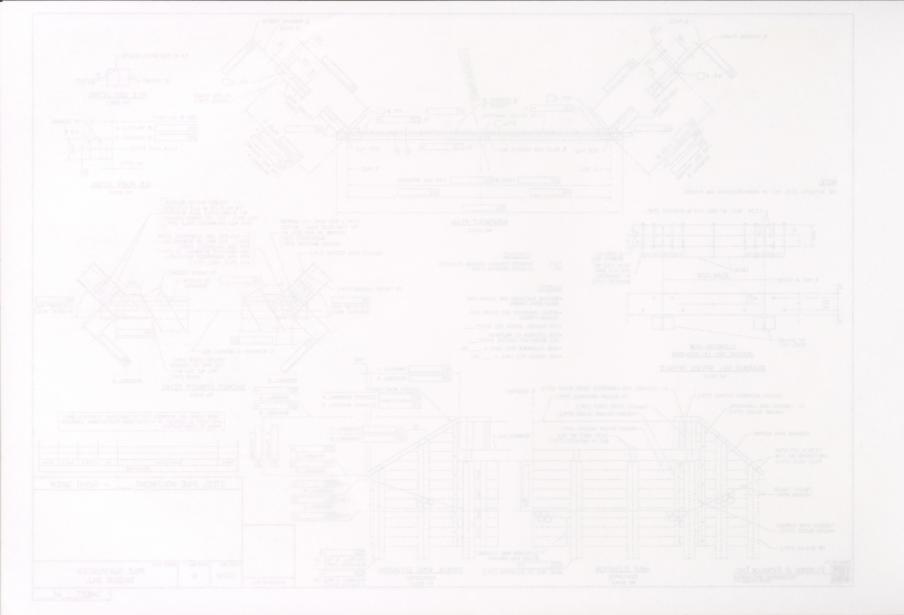


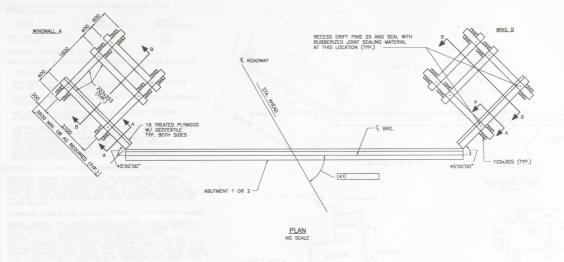


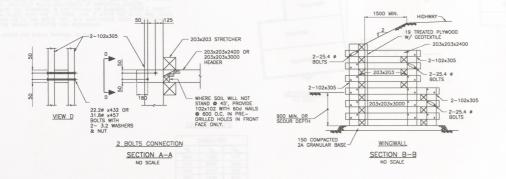












#### CRIBBING NOTES

LAY ALL STRETCHERS HORIZONTALLY.

USE MACHINE BOLT FASTENERS TO MATCH ASTM A-307 SPECIFICATIONS. HOT-DIP GALVANIZE ALL HARDWARE.

SOIL CONDITIONS:
DETERMINE THE SOIL & GROUNDWATER CONDITIONS & THE STABILITY OF THE CRIB WALL FOR EACH SPECIFIC CRIB WALL SITE.

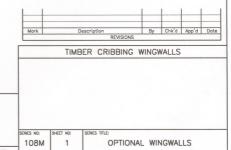
THE SECTIONS SHOW PROPORTIONS & DETAILS FOR CRIB WALLS FOR THE FOLLOWING CONDITIONS:

- A. FOUNDATION CONSISTS OF SAND, SAND & GRAVEL, OR OTHER GRANULAR SOIL WHICH DOES NOT SETTLE SIGNIFICANTLY UNDER THE WEIGHT OF THE CRIB & FILL.
- B. FILL WITHIN CRIBS & BEHIND CRIBS CONSISTS OF SAND, SAND & GRAVEL, OR OTHER FREE DRAINING GRANULAR MATERIAL PLACED IN 150 mm LAYERS & COMPACTED WITH VIBRATORY COMPACTORS.
- C. LOCATE BASE OF CRIB ABOVE GROUNDWATER TABLE.

FOR OTHER SOIL OR GROUNDWATER CONDITIONS, ADJUST THE CRIB PROPORTIONS & DETAILS AS NECESSARY TO PROVIDE AN ADEQUATE FACTOR-OF-SAFETY IN ACCORDANCE WITH GOOD ENGINEERING PRACTICE.

DESIGN ASSUMES END OF WALL TERMINATION TO OCCUR AT EXPOSED ABUTMENT HEIGHT (3000 MAX.), USE 4900 mm STRETCHERS TOE NAILED TO HEADERS AT ENDS. A HIGHER WALL REQUIRES A SPECIAL DESIGN.

MAXIMUM HEIGHT FOR TIMBER CRIB WALL IS 3000.



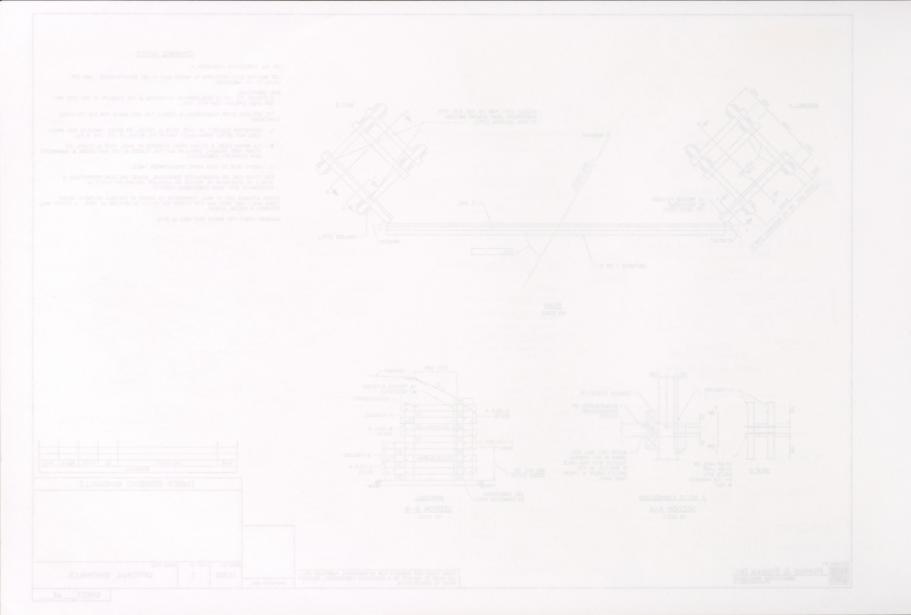
PREPARED BY:

POWERS & SCHRAM INC.

CONSULTING ENGINEERS, PARED STATE COLLEGE, PA

THESE PLANS ARE INTENDED FOR INFORMATIONAL PURPOSES ONLY AND MUST BE VERIFIED BY A REGISTERED PROFESSIONAL ENGINEER PRIOR TO CONSTRUCTION.

SHEET\_\_\_of\_\_



GABION NOTES

ASSURE THAT MATERIALS AND CONSTRUCTION MEET THE REQUIREMENTS OF:

MATERIAL

AGGREGATE:

PHYSICAL REQUIREMENTS, USE ACCEPTABLE QUALITY AGGREGATE, SOUND, FREE FROM STRUCTURAL DEFECTS AND FOREIGN SUBSTANCES.

SIZE, USE AGGREGATE IN THE FOLLOWING SIZES, MEASURED IN THE GREATEST DIMENSION:

GABION	MINIMUM	MAXIMUM			
HEIGHT	AGGREGATE SIZE	AGGREGATE SIZE			
ESS THAN 300	75	125			
300 OR OVER	100	200			

CENTEXTILES CLASS 2 TYPE B

GABION BASKETS- AS SHOWN ON THE STANDARD DRAWINGS AND AS FOLLOWS:

GALVANIZED STEEL WIRE, MINIMUM NO. 11 GAGE FOR HEIGHTS 300 AND OVER, NO. 13 GAGE FOR THE 225 HEIGHT.

TENSILE STRENGHT FROM 414MPa TO 586MPa, DETERMINED IN ACCORDANCE WITH ASTM-A3 92.

ZINC COATED WITH A MINIMUM COATING OF 0.24 kg/m2 DETERMINED IN ACCORDANCE WITH ASTM-A90.

MAXIMUM LINEAR DIMENSION OF THE MESH OPENING NOT EXCEEDING 113 AND MESH OPENING AREA NOT EXCEEDING 200 FOR BASKETS
300 IN HEIGHT AND OVER; MAXIMUM LINEAR DIMENSION NOT 300 IN HEIGHT AND OVER; MAXIMUM LINEAR DIMENSION NOT EXCEEDING 81 INCHES AND MESH OPENING AREA NOT EXCEEDING 3750 mm² FOR BASKETS 225 IN HEIGHT. DIMENSIONS MAY VARY, SUBJECT TO A TOLERANCE LIMIT OF 3% OF THE MANUFACTURER'S STATED SIZES.

CONSTRUCTION- AS SHOWN ON THE STANDARD DRAWINGS AND AS FOLLOWS:

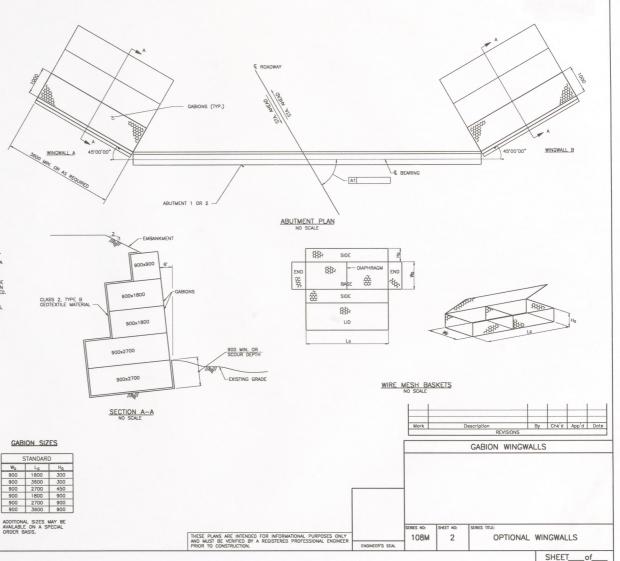
EXCAVATION, EXCAVATE AS REQUIRED TO PLACE THE BASKETS. REMOVE UNSUITABLE MATERIAL BELOW THE BOTTOM OF BASKETS AND REPLACE WITH ACCEPTABLE MATERIAL. THOROUGHLY COMPACT THE ENTIRE FOUNDATION AND FINISH TO A PIRM, EVEN SURFACE, ONE FREE OF VEGETATION, LARGE STONES, AND OTHER DEBRIS, WITH DEPRESSIONS FILLED. DISPOSE OF UNSUITABLE OR EXCESS MATERIAL.

GEOTEXTILES, CLASS 2, TYPE B, PLACE AS SHOWN ON THE STANDARD DRAWINGS.

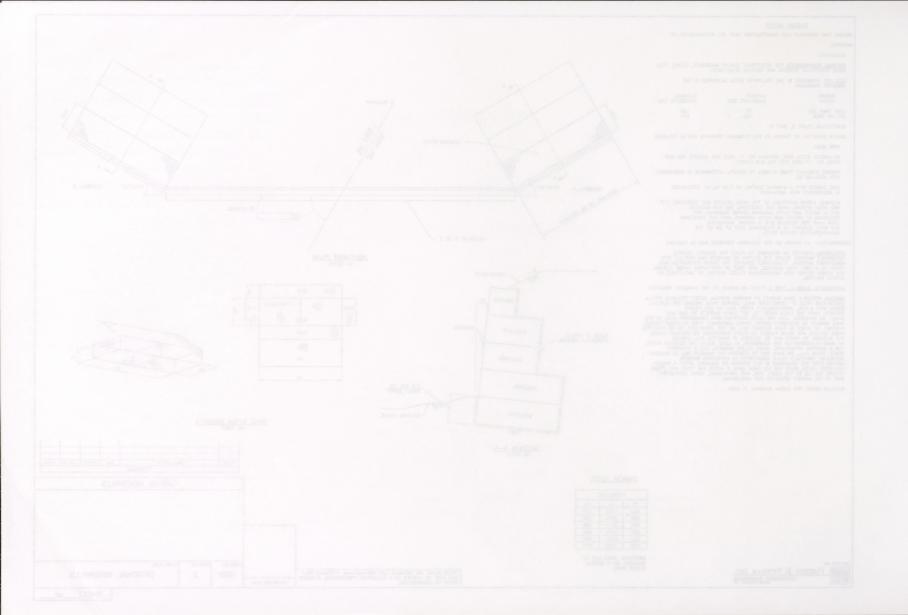
GEDITATILES, CLASS Z. LYPE B, PLACE AS SHOWN ON IN HE STANDARD DIAWNINS.

ABBIONS, ASSEMBLE EACH ASKETT BY BINDING VERTICAL EDGES TOGETHER WITH A
CONTINUOUS PIECE OF CONNECTING WIRE, LOOPED TWICE AROUND THE VERTICAL
EDGES WITH A COLL APPROXIMATELY VERYEY 200 NO 225 HEIGHT
BASKETS, LOOP THE COILS EVERY 75. SET EMPTY BASKETS TO LINE AND
ORDER, AS BROOKEDS, JOAN THE OWNS TOGETHER WITH AND HERE AND
ORDER, AS BROOKEDS, JOAN THE OWNS TOGETHER WITH, THEN SECURITY ATSETS
INTERNAL THE WIRES IN EACH OUTSIDE CELL OF THE STRUCTURE, OR AS DIRECTED,
WHEN GABIONS ARE BEINEY PLACED AS SLOPE PROTECTION OR CHANNEL LINING,
THE INTERNAL THE WIRES MAY BE DELETED, IF DIRECTED, THE ORDINAL LINING,
THE NITERNAL THE WIRES MAY BE DELETED, IF DIRECTED, THE ORDINAL LINING,
THE NITERNAL THE WIRES MAY BE DELETED, IF DIRECTED, THE ORDINGON'S
PLAND PLACEMENT OF THE ADDRESSALE, ALONG THE CAPORD
FACES, CHAIN TALL, OR IRON ROO TO STRETCH THE BASKETS AND TO MAINTAIN
ALIONMENT, CARPETLLY! PLACE AGREGATES IN CORROSION BASKETS
MAKING SURE THE SHEATHING IS NOT BROKEN OR DAMAGED. AFTER A BASKET
WAS BEEN PLACED, BROM THE LO OVER UNITLE. HERETS THE SIDES AND EDGES.
SWITCH IN THE MANNER SPECIFIED FOR ASSEMBLING.

MAXIMUM HEIGHT FOR GABON WINGWALL IS 2400











WIT-02-0049